# Modelling the Properties of Packed Bed Structures Formed During Filtration 

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Signed: William Eales

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## COVID-19 Statement

This project was affected by the COVID-19 pandemic, however due to its nature as a computational project, it was still able to progress during lockdown, even if at a slightly slower pace. The main effect the pandemic had on this project was the decreased accessibility to my supervisors and others in my department, as whilst email contact was maintained, there was a natural delay compared to being able to discuss issues or ideas in person.


#### Abstract

Agglomeration is an issue that causes many problems during secondary processing for pharmaceutical companies, causing material to need further processing, and costing additional time and resources to ensure a satisfactory outcome. A potential source of agglomeration arises from the particle contacts established during filtration that lead to robust agglomerates forming during drying, so that a necessary first step towards understanding agglomeration is to study the packing properties of filtration beds. Here I present two and threedimensional models simulating the formation of packed bed structures during filtration.


These models were coded from the ground up using the ForTran programming language, starting with the 2 D algorithm as it was a simpler algorithm compared to jumping straight to 3D systems. Once an algorithm was formed that could create realistic 2D systems of packed circular particles, it was extended so that it could also create systems of spherical particles in 3D. A variety of improvements and modifications were made to the algorithm as part of this change, including adding a stochastic optimisation function for determining particle locations, which was found to be a much more efficient method than the equations used in the 2D algorithm, so the stochastic optimisation method was used in all algorithms going forwards. The final modification made to the algorithm was the option to create systems formed of chain structures, made up of circular particles attached together; this enabled the investigation of more realistic systems.

These models use circular and spherical particles of different sizes, mimicking the bimodal particle size distributions sometimes encountered in industrial practice. The systems containing chain particles made up of these circular particles were varied by both particle size and chain length to observe the effect of these parameters on systems with more realistic particles. The statistics of packing and void formation, the distribution of inter-particle
contacts and percolation structures, and the breakage of these systems under shear forces, are presented and discussed in the context of filtration, drying and agglomeration. The 3D model was also compared to current industry standard software, Ansys Rocky DEM, as part of a placement with AstraZeneca, where it was found my model produces very similar packing fraction outputs to those produced by Rocky DEM.

The model paves the way for predictive capabilities that can lead to the rational design of processes to minimise the impact of agglomeration.

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## 1 Introduction

### 1.1 Aims of Project

The aim of this project is to better understand how agglomeration occurs during particle drying, and how it can be mitigated. To do this I have designed a computer model that can emulate the packing of particles into filter beds. This model will enable us to gain greater understanding of the properties of these packed beds, and how those properties, such as particle size distribution and the presence of percolation structures potentially affect agglomeration and fragmentation. At this time, the model does not contain enough features to describe agglomeration but is in a position to be used in future projects, therefore this thesis is mainly investigating the packing of shapes in 2D and 3D.

The model will start with circular and spherical particles due to the ease of creation as well as aligning with laboratory work undertaken at the University by PhD student Mariam Siddique investigating the agglomeration of glass beads as an insoluble substitute for crystalline particles. This will allow future comparisons of the systems created by the model with physical examples.

I have also upgraded the model to be able to produce systems involving nonspherical particles, potentially allowing us to investigate specific crystalline Active Pharmaceutical Ingredients (APIs).

The distribution of forces between these particles when a shear stress is applied has also been investigated in collaboration with MEng project students, so that weak points of the packed bed structure could be identified, to better understand how these systems would break apart under stress. The impact of structural properties, such as how the particles in the bed are arranged, can be explored in future work.

This project whilst producing this model has also given me a lot of experience into both regular programming workflow, as well as the work that goes into producing a computational model, even one as simple as mine. As part of using this model, I have shown that it produces realistic systems consistent with those formed under gravity, with parameters, such as packing fractions and number of contacts per particle, that fall within the calculated minimum and maximum ranges. As stated above, the model did not reach the stage during this project where it could be applied further beyond testing initial systems, so we were not able to investigate larger, more realistic systems.

### 1.2 Significance of Project

Agglomeration during pharmaceutical processing, particularly drying, can cause many problems further down the line such as ensuring the content uniformity of tablets. Whilst the mechanics of how agglomerates are formed are known, little is known about the best practices to avoid it. The aim is that the information gained from analysing the beds created with our model will give us greater insight into how agglomeration can be lessened and its negative repercussions prevented.

### 1.3 Limitations of Project

Due to gravity being the only force accounted for (in an approximate way) during the bed formation, our model produces a more simplistic representation of a packed bed system, than if all the forces between the particles, such as friction in a dry system or hydrodynamics in a wet system, were accounted for. This route was chosen to allow us to produce a model that enables us to have close control over its direction to keep it in line with the scope of the project, as well as significantly decreased computational times compared to more complex models.

### 1.4 Structure of Thesis

In the pages following this introduction, I will review the literature surrounding agglomeration, how agglomerates form and their impact on the pharmaceutical production process, as well as modelling as a scientific tool.

The next chapter will focus on the stages of development the 2D model underwent along the course of my project, as well as a step by step look at how the model runs to create a bed system. Following that will be a similar walkthrough and description of the 3D algorithm.

Then there will be a discussion of the results I obtained from investigating the properties of the systems created by the 2D model, and then a discussion of the systems created by the 3D model.

Next will follow a description of the algorithm used for modelling nonspherical particles, as well as the results from the systems it produced.

As part of my project, I undertook a three-month placement at AstraZeneca, Chapter 7 discusses the work performed as part of that placement.

Finally, the conclusions gained from these investigations will be discussed.

## 2 Literature Review

The global pharmaceutical industry provides medicines for the world population, now approaching eight billion people ${ }^{1}$, and has an annual turnover of around one trillion pounds ${ }^{2}$. The vast majority of these medicines are supplied as tablets and capsules ${ }^{3}$ in which the API exists as a crystalline solid formulated with multiple excipients to aid both the formulation process and as vehicles for carrying the APIs. As a consequence of this the physical properties of the APIs, including particle size distribution, crystal shape and the extent of agglomeration, are often critical quality attributes of the API because they play an important part in powder flow and hence formulation performance.

There are many problems that can occur during secondary processing of APIs. The aim of this project is to investigate agglomeration, as its effect on the filtration process is of great importance to AstraZeneca, who are funding this work, both how it occurs and what can be done to prevent it. This is in the hope of creating a model to better understand its phenomenology and then to obtain new insight into how best to negate its effects. As previously stated, the model described within is not yet capable of completing this task.

### 2.1 Agglomeration

### 2.1.1 What it is and its mechanisms

Agglomeration can be defined as the process of particulate solids gathering into an agglomerate, which is a robust cluster of these particulate solids ${ }^{4}$. This can sometimes be preferable as the larger agglomerates have better flowability compared to groups of smaller particles. However, during drug processing agglomeration can result in various inconveniences, such as affecting content uniformity, through increasing variation in the quantity of API contained within individual tablets, and damaging processing machinery ${ }^{5}$.

The binding mechanisms present during agglomeration, shown in Figure 2.1, were defined and ordered by H. Rumph et al ${ }^{4}$ and will each be briefly explained below. My model assumes solid bridges are the mechanism by which particles are joined together within the systems, shown in Figure 2.1a.




Figure 2.1: Representation of the different mechanisms for
Agglomerate formation (redrawn from ${ }^{6}$ ) a) Solid Bridges b) Adhesion and Cohesion Forces c) Surface Tension and Capillary Forces d) Attraction Between Solid Particles e) Interlocking Bonds

### 2.1.1.1 Solid Bridges (Figure 2.1a)

In systems where the temperature rises sufficiently, the particles start to melt. This can result in the particles merging at contact points with other particles, when the temperature cools the melted material solidifies causing the particles to fuse together, forming an agglomerate. Solid bridges can also occur even below the melting temperature of the solids present, as diffusion of atoms or molecules can occur across the contact points, over time forming bridges. This process is known as sintering and the bridges called sinter bridges. This heat can be from a deliberate heat source due to the processing requirements of the reaction or to enable agglomeration in reactions where it is favourable. This is mostly applied in industries that process minerals and ores, to combine fines
into agglomerates for easier handling ${ }^{7}$, and not in pharmaceutical processes as high temperatures can lead to chemical degradation ${ }^{4}$.

### 2.1.1.2 Adhesion and Cohesion Forces (Figure 2.1b)

In the instances when agglomeration is preferred, a binding agent can be added to the system to aid in the formation of agglomerates and to increase their strength. These are generally viscous substances that cause particles to stick together by filling in the gaps between them. Resin and tar are used in non-medical applications, however there are also binders that are suitable for pharmaceutical processing ${ }^{4}$ such as sugars like sucrose and liquid glucose and binders such as microcrystalline cellulose ${ }^{8}$.

### 2.1.1.3 Surface Tension and Capillary Forces (Figure 2.1c)

Liquid bridges can also form between particles which have strong forces that maintain the bond between the particles. These forces are created by a negative capillary pressure that occurs when a liquid is filling the whole pore volume between two particles, causing the particles to be pulled together ${ }^{4}$. If the liquid is a solvent used in a previous purification process, when it evaporates it will leave behind the dissolved impurities and API, which can then form solid bridges between the particles. These bridges then act as bonding agents in the solvent's place, holding the particles together ${ }^{9}$. This is one of the most common mechanisms of agglomeration in pharmaceutical manufacturing.

One example of this, known as Snowballing or balling up, occurs during agitated drying with too much solvent present. The agitation causes the clusters to move throughout the system, allowing them to come into contact with more solvent-wet particles, which then join the cluster. This process then repeats with very large agglomerates forming due to the increased opportunities to bind to particles. ${ }^{9}$

### 2.1.1.4 Attraction Between Solid Particles (Figure 2.1d)

It is possible that there are interactions occurring between the particles that cause them to attract each other, such as hydrogen bonding, if there is a suitably electronegative atom present, as well as the van der Waals forces that occur at all solid surfaces. ${ }^{4}$

### 2.1.1.5 Interlocking Bonds (Figure 2.1e)

Interlocking Bonds occur when the particles have irregular shapes so that they can intertwine and become entangled with each other, so forming the agglomerates. ${ }^{4}$ This occurs more readily in systems of needle like particles, where groups of particles snag on each other as they pass. Such agglomerates often look like sea urchins.

### 2.1.2 Problems caused by Agglomeration

Agglomeration frequently occurs during secondary processing, particularly during washing and drying. Due to their ability to differ greatly in size and strength, agglomerates cause various problems during the processing of drug products, some of which are discussed below.

### 2.1.2.1 Content Uniformity

Content uniformity is a property that needs to be maintained to ensure quality control of capsules and tablets and is assessed as follows. Randomly selected capsules or tablets are taken from a batch of product and then tested to determine if they each contain an amount of active ingredient that falls within the acceptable range ${ }^{10}$. Multiple studies to determine the effectiveness of methods of ensuring content uniformity have been carried out. ${ }^{11,12,13,14}$

There are guidelines which set out the acceptable ranges for how much drug substance should be present in each type of tablet, capsule and other dosage
types. Maintaining content uniformity across the tablets is essential ${ }^{6}$ as if tablets or capsules are produced that contain too little active ingredient, a patient will not be getting the treatment they need, and if a tablet or capsule contains too much active ingredient, it increases the possibility of an overdose ${ }^{15}$.

The variation in size between agglomerates results in a broad particle size distribution within the system. This in turn increases the difficulty of maintaining content uniformity between individual tablets or capsules. Therefore, the presence of agglomerates within a processing system will result in extra care having to be taken to ensure the consistency of the tablets, through specific use of solvents to try and prevent agglomeration or by further processing, typically milling, after agglomeration has occurred. ${ }^{15}$

### 2.1.2.2 Processing Issues

The formation of agglomerates also greatly decreases the efficiency of drug processing, as any product that is part of a large agglomerate needs to go through further processing. Some agglomerates can be too difficult to break open due to the strength of the contacts. Some agglomerates may have impurities trapped inside, meaning it is not always cost effective to send the material through processing a second time ${ }^{16}$. This may occur when mother liquor is trapped inside agglomerates during ineffective washing, thus the agglomerates can take longer to fully dry, and the purity of the product is impacted ${ }^{17}$.

Particularly large and strong agglomerates can also cause damage to the machinery itself, due to their size and strength blocking powder flow within the machines and grinding against parts, as well as causing difficulties in removing the batch so it can be processed further ${ }^{9}$.

### 2.1.3 Continuous Systems

The importance of being able to efficiently process larger quantities of product at the same time is relatively obvious, as it would potentially reduce the costs and time that would be required to process the same amount in multiple smaller batches. A good deal of the work investigating the drying process has been done into how to scale it up to be able to process larger quantities or to create a continuous system. ${ }^{18}$

A continuous system would speed up the process as the system would be capable of removing its own waste and transferring the products onto the next step of processing without someone having to be present to do it. This means, in principle, that the machines would require less supervision and also increase the speed of the process as any transfer time between steps of the process would be cut out, as well as allowing for full end to end processing. ${ }^{19}$

One of the issues with creating a continuous system is ensuring that the machinery is able to deal with any unwanted circumstances that occur within the system during each of the processing stages; for example, if agglomerates form during drying, they should not be ignored and passed along onto the next processing stage. Instead, they would need to be separated out, broken down and potentially rewashed or dried before being able to be added back into the system. Additionally, if an error occurs within the system, it is easier to identify in a batch system where the issue originated so a fix can be sorted. Whereas in a continuous system, it can be hard to identify at what point the issue arose. ${ }^{19}$

### 2.2 Modelling

Computational modelling of complex systems has become more widely available due to the increase in computational power over time. This has allowed researchers to analyse systems that were previously difficult to investigate experimentally, for example due to stability issues or lack of availability of reactants. ${ }^{20}$

One of the ways in which computational modelling can be utilised is as a predictive tool prior to undertaking experimental work. This allows us to investigate the proposed experiment ahead of time, before any reactants are potentially wasted, and to ensure that the experiment would act as planned and produce a useful result. The model can also help show the preferred conditions for the experiment to run under; this should reduce negative effects and prevent accidents. ${ }^{21}$

Another way in which modelling can be applied is alongside experimental work, so that the data produced from the model can be compared with data collected from physical experiments. This is especially useful whilst the model is relatively new to ensure that the data it is producing is similar to the results from a physical experiment to check whether there may be a calculation error within the model. But once the model has been validated, it can also be used to produce data that would otherwise be difficult to collect with laboratory experiments, for example due to lack of access to reactants, danger to researchers or unrealistic time lengths. ${ }^{22}$

Some examples of types of models and their capabilities are discussed below.

### 2.2.1 Molecular Dynamics

Molecular dynamics (MD) is a type of simulation that analyses the physical movement of molecules. The most common versions of MD simulations use Newton's equations of motion to calculate the trajectories of the particles; the forces between them are calculated using interatomic potentials or molecular mechanics force fields ${ }^{23}$. As molecular systems generally consist of large quantities of particles, it is often impossible to determine properties of very complex systems analytically, therefore MD simulations use numerical methods. As a result, these systems are an approximation to reality, often not covering all the complexities a real system would have to compromise for the computational power that would be required to run a truly realistic simulation. This makes longer MD simulations less viable, as a single error early in the simulation would propagate throughout the simulation potentially causing the later stages to be far less accurate. Algorithmic developments mean that such an error is more likely to be from the user, in the way that they set up the simulation, rather than a failure of the numerical procedures.

One advantage of MD simulations is that they work on an atomistic level therefore they can give information about the molecular detail of a system. However, as with most computer simulations, MD is computationally intensive and depending on the specific system being investigated could require a dedicated computer setup to run. Due to the timeframes of MD simulations being extremely short (typically on the 100 ns timescale), it can mean that vast quantities of simulations need to be run to gather enough data on a system ${ }^{24}$. Additionally, MD simulations are not useful when investigating large scale systems due to their small-scale nature (typically on the 10 nm scale), so a different modelling method would be needed, otherwise the MD simulation runtime would be unacceptably long.

### 2.2.2 Discrete Element Method

Discrete Element Modelling (DEM) is closely related to molecular dynamics, where it differs is that it includes more complicated geometries as well as rotational degrees of freedom. An important distinction is that the elements of the model are the granular particles rather than atoms, so it works on much longer length and time scales. The force fields and equations of motion used must therefore embody all the relevant physics.

A DEM simulation works by setting up a model with all of the particles placed within it and given an initial velocity. The forces acting on each particle are then calculated based on factors such as friction, gravity, or attractive and repulsive forces between particles. These forces and the initial velocities can then be used to compute an updated location of each particle following a short time step. These updated positions are then used to calculate the next round of forces, and the process then loops until the simulation ends. More detail is giving on the workings of a DEM system in section 7.2.

DEM has many advantages, including its ability to simulate a variety of particle flow mechanics, as well as being able to be implemented into other engineering applications. DEM also allows for more detailed analysis of powder systems than would normally be achievable using physical experiments, allowing for a greater range of data to be collected.

As with other computational modelling, the extent of the system being investigated is limited by the computational power available. Due to DEM being relatively computationally intensive compared to other model types, its capabilities are limited in relation to the size of the system being analysed and the duration of the simulations being run ${ }^{25,26}$. In a simulation of a fluidized bed, a time step of $10^{-3}$ s has been used ${ }^{27}$, with other experiments using smaller timesteps of down to $10^{-5} \mathrm{~s}^{28}$.

During my project I used Rocky DEM modelling software (part of ANSYS), however there are many more packages available. Another source of DEM modelling is EDEM ${ }^{29}$, simulation software that uses DEM simulations for "bulk and granular material simulation". EDEM has been used across multiple industries in different applications, such as investigating the strength of potato starch agglomerates for the food industry ${ }^{30}$, simulations of fluidized beds ${ }^{27}$, and modelling granular flow of systems to analyse the effect of different blade shapes ${ }^{31}$.

Within the filtration space, DEM has been used in multiple instances to simulate filtration processes, for example to determine the porosity of systems ${ }^{32}$ or to compare wet and dry filtration, where either hydrodynamic or gravitational forces are used to filter the small particles ${ }^{33}$. Simulations have also been done with a variety of particle shapes and sizes, ranging from more spherical particles ${ }^{34}$ to fibrous particles ${ }^{35,36}$.

Whilst the above methods could have been used for this project, the approach of creating a new model was decided upon as it ensures that we had direct control over the direction and application of the model, keeping it simple compared to other models to aid in the speed of bed creation, as well as providing a unique learning opportunity for me as part of the project.

### 2.3 Areas Investigated

There are many different parameters across processing that affect agglomeration, as detailed in Figure 2.2.


I aim to investigate some of these parameters, specifically the particle size and shape, particle size distribution, and the packing behaviour, through investigating simulated packed bed structures. Discussed below is some of the previous research into each of these properties and how they are relevant to agglomeration.

### 2.3.1 Packing

### 2.3.1.1 Packing of objects in two dimensions (2D)

The packing of shapes in 2D has been extensively researched and many models have been created to determine the possible packing fractions under different circumstances. The most random of these types of packing is Random Sequential Adsorption (RSA), where "particles" are added to a system entirely at random, with the only restriction being that they cannot overlap. This results in low packing fractions, with the maximum packing fraction when using RSA in a system with single sized circular particles being roughly $0.547^{38}$, due to the lack of order.

Previous investigations have also looked into the maximum possible packing of different systems. The highest packing fraction possible in a system of identical circles is $\frac{\pi}{\sqrt{12}} \approx 0.9069^{39}$, when the circles form a triangular lattice.

### 2.3.1.2 Packing of objects in three dimensions (3D)

Packing of 3D shapes has also been previously investigated. When using identical spherical shapes, there are two lattices that can occur to achieve the highest packing fraction ${ }^{40}$, which is $\frac{\pi}{3 \sqrt{2}} \approx 0.74048^{41}$. These two lattices, as seen in Figure 2.3, are face-centred cubic (FCC) and hexagonal close-packed (HCP) and are formed dependant on the symmetry of the system.


Figure 2.3: An FCC lattice (left) and HCP lattice (right) (redrawn from ${ }^{42}$ )

Other examples of packing types and their maximum densities are: random close packing, $0.6400^{43}$; the tetrahedral lattice, $\frac{\pi \sqrt{3}}{16} \approx 0.3041^{44}$; and the loosest possible density that has been found is 0.0555 in the Heesch and Laves loosepacking structure ${ }^{45}$.

Spherical packing was first analysed around 1587, when the question was posed about whether or not there was a method to quickly determine the number of cannonballs in a square pyramidal stack, which is known as the cannonball problem. ${ }^{46}$

### 2.3.1.3 Packing of Multiple Sized Particle Systems

Most of the research into systems where there are multiple sizes of particle present investigate binary systems, i.e. those with two distinct particle sizes present. In a 2D square packing system, it has been found that up until a radius ratio of $0.41: 1^{47}$, the system packs densely by filling in the voids created by the
larger particles with the smaller particles. However, after this point, due to the sizes of the particles being more similar, the system rearranges into a different structure in order to maintain their density ${ }^{47}$. Additionally, if the radius ratio is above $0.742: 1$, the binary system is no longer able to pack better than a system with same sized particles. ${ }^{48}$ The binary system with the highest possible packing fraction is with a particle ratio of $0.1: 1$, having a packing fraction of $0.9624 .{ }^{47}$

Descartes circle theorem, shown in Equation 2.1, can be used to determine the radius of the particle that would fit perfectly between three particles, so that all four of them would share an edge with all of the others, as shown in Figure 2.4.

$$
\begin{equation*}
k_{4}=k_{1}+k_{2}+k_{3} \pm 2 \sqrt{k_{1} k_{2}+k_{2} k_{3}+k_{3} k_{1}} \tag{2.1}
\end{equation*}
$$

where $k$ is the curvature, $1 /$ radius, of each of the circles 1 to 4 . The two solutions to this theorem, through the $\pm$, are due to the possibility of a large circle encompassing the three present circles, as well as a smaller one present between them. When the radii of the three present circles are the same, the ratio of their radii to the radius of the circle in between them is $0.1547 .{ }^{49}$


Figure 2.4: Example of tangent circles with the black circles being present particles, and red circles being possible solutions through Descartes theorem

Binary systems have also been investigated in 3D, where it has been found that if the radius ratio is $0.299099: 1$ or lower, then it is always possible for smaller spheres to pack inside the interstices between the larger spheres ${ }^{50}$. When the radius ratio exceeds $0.4142: 1^{51}$, the smaller spheres are no longer able to pack inside even the octahedral voids within the structure, meaning that above this ratio, the structure either needs to expand to allow the more similarly sized smaller particles to fill the voids inside, which decreases the overall density, or it would rearrange into a more complex structure ${ }^{51,52}$.

The packing fractions of binary systems of a radius ratio either side of the perfect 0.4142 value have been investigated. The packing fractions of the systems below this value were generally greater than the systems with a ratio above that value, except when comparing the minimum and maximum of some of the systems ranges. The systems with a radius ratio lower than the perfect value having packing fractions of around 0.8 and the systems with a radius ratio higher than the perfect value having packing fractions around 0.75 . All of the systems packing fractions with a ratio below the value, except one, decrease when the ratio increases. The only system that increases alongside an increase in radius ratio is an orthorhombic lattice system with six small particles for each large particle. When the radius ratio is above the perfect value, of the five systems investigated, two showed a decrease in packing fraction, two showed an increase in packing fraction, and one showed no change in packing fraction. ${ }^{53}$

### 2.3.2 Percolation

Percolation theory is the study of percolation, which is generally used to investigate how fluids flow through porous materials through the connectivity of the pores. The theory describes how a network is affected when nodes or links between them are added or taken away. It was first elucidated in the Flory-Stockmayer Theory ${ }^{54}$, which governs the point at which a gel forms from a system of polymers ${ }^{55}$. This point is generally known as the percolation
threshold, which is the critical value for a system where below it a giant connected component does not exist, and above it one does exist. However, in this work we are instead looking at the connectivity of particles within the system, describing a percolation chain as a chain of particles connecting edges of the box, instead of a group of pores for fluid to pass through.

There are two different "models" for investigating percolation: bond percolation and site percolation. Bond percolation uses the frequency of the presence of bonds between nodes to determine if a percolated structure is present. Site percolation determines whether or not a site is open and connected open sites form percolated structures. To visualise this using a grid of squares, bond percolation works using the connections between the vertices, whereas site percolation connects whole squares of the grid that are "open", as can be seen in Figure 2.5. ${ }^{56}$


Figure 2.5: Representation of Bond and Site Percolation (redrawn from ${ }^{57}$ )

Generally, systems of infinite size are examined, so a percolated structure would be a connected cluster of infinite length. Kolmogorov's zero-one law states that, 'the probability of an infinite cluster existing is either zero or one, for any given probability of a site being open or closed'58. In our systems, the chance of a percolation structure occurring is based on the probability of large
particle to large particle contacts forming. This allows us to investigate the critical value of the site probability to determine the critical probability, known as the percolation threshold, at which the cluster forms.

Previously exact and approximate values of percolation thresholds for different lattices have been successfully calculated. It has been found that regular triangular lattices, shown in Figure 2.6, have a site percolation threshold of $0.5^{59}$, which is the type of lattice that a fully regular system of circle packing could be likened to, with the centre of each circle a point on the lattice. In 3D, the site percolation threshold for FCC lattices has been calculated to be $0.1998 \pm 0.0006$ and the bond percolation threshold is $0.1198 \pm 0.0003^{60}$. This shows that a percolated structure is much more likely to occur in 3D, as the percolation threshold in 3D systems is much lower than in 2D systems.


Figure 2.6: Triangular Lattice
The investigation of percolation theory can give insights into multiple different disciplines, including studying the flow of traffic through cities when certain roads are available, or not, to determine bottlenecks ${ }^{61}$, as well as in ecology to study environmental fragmentation effects on habitats ${ }^{62}$. Our interest lies in its uses, investigating how contacts within beds of particles might break when the bed system is altered, through the presence of differing particle sizes and other factors.

### 2.3.3 Finite Size Effect

Models also need to deal with the finite size effect ${ }^{63}$, which is where, potentially due to the small size of a system, the edges of the system can skew the data. Using one of our produced systems as an example, the packing of the particles at the edges of the box is distinctly different to the packing in the centre, with denser packing in the centre of the bed. In a small enough system, this difference would affect the average data values and therefore give an incorrect outcome, compared to a larger system where the edge values are not as big a part of the system as a whole.

Models can either be run with increasingly large systems to determine at which size there is no longer a skewing effect from edge cases, and the data used to extrapolate to an infinite system, or smaller systems run and the data from the edge cases discarded. Both strategies have their pros and cons, with larger systems taking longer and more computational power to complete however being able to lessen or remove the finite size effect, and smaller systems being easier to produce however still retaining the finite size effect as well as the potential of producing skewed results when looking at averages of a system as a large fraction of it has been removed.

### 2.3.4 Angle of Repose

The angle of repose is defined as the steepest angle of descent, relative to a horizontal surface, that a material can be piled without slumping. ${ }^{64}$

There are various methods for determining the angle of repose for a material. The simplest is using the following equation if the coefficient of static friction is known for the material,

$$
\begin{equation*}
\tan (\theta) \approx \mu_{s} \tag{2.2}
\end{equation*}
$$

where $\mu_{s}$ is the coefficient of static friction and $\theta$ is the angle of repose. ${ }^{65}$

The other methods are experimentally based and are each suitable for a different type of material. The tilting box method is suitable for fine-grained materials with a grain size of 10 mm or less and allows the coefficient of static friction to be determined for a material, from which the previous equation can be used to determine the angle of repose. This method works by filling a box with the granular material, and then tilting it gradually until the material begins to slide, as depicted in Figure 2.7.66


Figure 2.7: Depicting the Tilting Box Method (with permission from ${ }^{66}$ )

Another method is the fixed funnel method, where the material is poured through a funnel to allow it to form a cone shape on a base. Once the cone has reached either a set height or a set width, the angle of repose can then be calculated using the following equation,

$$
\begin{equation*}
\theta=\tan ^{-1}\left(\frac{2 h}{b}\right) \tag{2.3}
\end{equation*}
$$

where $\theta$ is the angle of repose, $h$ is the height of the cone, and $b$ is the width of the base of the cone. ${ }^{66}$

The angle of repose is useful to investigate as it has links to the flowability of granular materials, which helps when designing processing equipment and storage for particulate solids as it ensures the stability of the material and reliable flow from hoppers. ${ }^{67}$

Another use of the angle of repose is to allow calibration of models for when a specific material is being simulated, the angle of repose of the system created in the model can be compared to the expected value to determine if the model is running accurately. ${ }^{68}$ However, as the model designed for this thesis does not consider frictional forces, only gravity, it is likely that this method will not be applicable to my model.

### 2.3.5 Bed Fragmentation

With the help of two final year MEng project students, we were also looking to investigate the effect of a shear force on the contacts between the particles within the modelled systems, discussed further in section 3.1.1.12. This allows us to see how they break apart, and so we can potentially compare different system parameters, such as particle size distribution, with how clusters can form within the systems.

Agglomerates are generally defined by their size and strength, with the strength being defined by how difficult they are to break apart. Different factors have been investigated for their effects on agglomerate properties, including particle size and shape distribution, the solvents used during processing, and agitation during filtration. ${ }^{69,70}$ Higher agitation does result in smaller agglomerates, however also runs the risk of particle breakage, so often it is a
balancing act between reducing particle size to an acceptable level, without breaking them down too far. ${ }^{71}$

Investigation has also gone into the factors that affect the breakage of agglomerated systems in industries other than pharmaceutical, such as within the food industry, where DEM has been used to investigate how cereal grains break apart under impact within an agitated system. ${ }^{72,73}$

There is no unified way of reporting agglomerate properties, although some methods are becoming more consistent, such as the agglomerate brittleness index which describes the strength of an agglomerate. ${ }^{74}$ We anticipate that with the basis of the model complete, it can be used to add some more knowledge to how agglomerates act under various stresses and circumstances to greater aid the industries that need to find a solution to this issue.

### 2.3.6 Non-Circular / Non-Spherical Particles

Whilst spherical particles are a good starting point for simulating packed beds, being able to simulate specific particle shapes and sizes is incredibly useful. Whilst some modelling algorithms are capable of simulating nonspherical shapes and sizes, to accurately simulate a specific substance, many more parameters describing its particles are required beyond its shape and size, all of which massively increases the computational time and power required. This is briefly discussed further in Chapter 7.

Therefore, when simulating non-spherical particles, it is often done using spherical particles as a starting point ${ }^{75}$, forming them into chains as illustrated in Figure 2.8. This allows simulation of more sophisticated systems without driving up the computational power required as far. The use of the circular particles as building blocks instead of swapping to polygons was to allow the new algorithm to build off the old one, thus decreasing the workload.


Figure 2.8: Example of a chain made up of circular particles.

Generalisations about system properties, like packing fractions, cannot be made across all systems of non-circular particles due to the wide range of particle shapes and sizes possible, only being somewhat possible when examining systems made up of a specific set of particles, due to the large variance that can now occur, even when only accounting for shape and size. Therefore, I will specifically be investigating chains made up of spherical particles.

Research has gone into the packing on non-spherical 3D shapes, with the two shapes closest to my research being cylinders and spherocylinders: spherocylinders being cylinders with rounded ends. The maximum packing fraction found for both cylinders and spherocylinders is $\sim 0.9069^{76}$, dependant on the ratio between the diameter and height of the shape. Figure 2.9 shows the effect on changing the ratio of the diameter and height of cylinders and spherocylinders was found to have on the packing fraction of their systems using a relaxation algorithm. This algorithm works by filling the system with randomly placed shapes, i.e. cylinders, with large overlaps. When the system
then iterates, the particles move away from each other, lessening the overlaps, and the system size increases. The algorithm ends once the total overlap has become lower than a predefined value. ${ }^{77}$


Figure 2.9: Packing fractions of systems of cylinders or spherocylinders at different aspect ratios of height/diameter (redrawn from ${ }^{76}$ )

Both the cylinder and spherocylinders have a peak packing fraction, with the cylinder graph having a more defined peak. The cylinder systems are also shown to have higher packing fractions across the range of aspect ratios simulated.

The packing of these shapes under gravity has also been investigated using DEM ${ }^{78}$, where the effect of different parameters within the DEM software on the packing fraction of a system were analysed and compared to experimental data. In contrast to Figure 2.9, this research found that when increasing the aspect ratio, it often resulted in the packing fraction plateauing instead of showing a consistent decrease, which is likely due to the different addition methods and the complexity of the simulation methods used.

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## 3 Methodology

The aim of this work is to produce a model that can produce realistic representations of packed beds of particles formed under gravity that can be used to investigate agglomeration during isolation. This started with a 2D algorithm as it was initially easily produced, before upgrading it to a 3D algorithm.

A new ab initio model was developed instead of using pre-existing software as it allows targeting the model towards specific issues that we want to investigate, as whilst current modelling software can achieve many goals, due to their complexity they can take up much more computational time and power than would be needed to solve a single problem within these systems.

The following chapter discusses the stages that the 2D and 3D algorithms went through from initial conception to their current states. It also discusses the other functionalities that the model is able to perform, and the specifics of the experiments performed for data collection. The creation of these algorithms continued all the way up to the end of my project, with the 2D algorithm being finalised after roughly two years, the 3D algorithm finalised after the third year, and the chain particle algorithm being developed in the last year. The algorithm was created using the ForTran programming language, learnt using online resources and literature. ${ }^{1,2}$

### 3.1 2D Algorithm

### 3.1.1 Timeline of Model

This section looks through the stages that the 2D algorithm went through and the reasons behind each of the changes, from its initial setup to the algorithm used to produce data discussed in the later sections.

### 3.1.1.1 Initial Program

The first step taken in producing the model was to create a box such that the boundaries could be edited and it could have particles, made up of covered points within the system, placed inside it. Initially this was done by creating a 2D array, allowing each co-ordinate to have an individual value. The values used were a 0 , denoting that its location was empty, or a 1 , showing that a particle was present at that location. The array could then be printed, showing the particles using a grid of $0 s$ and 1 s . The size of the box could be changed by simply editing the $x$ and $y$ ranges of the array.

Once the box was set up, the particles could be added. This was done by randomly generating an $x$ value, then a loop was initiated, with the starting value being the maximum $y$ value present in the array, decreasing towards 0 in intervals of -1 . The loop repeated until either the particle reached the bottom of the box, in which case the particle would be placed there, or the falling particle impacted a previously placed particle. Impacts were determined by looking at the array and determining if the falling particle overlapped any coordinates in the array containing a value of 1 . When an impact occurred, a series of 'if, then, else' statements were run that determined where the falling particle had impacted and how to react, until a suitable position was found for the particle to be placed. For example, if the falling particle had been impacted (i.e. encountered an existing particle in the bed) on its left side, then it would "slide" down to the right to find a stable resting place. An example of the structure formed in this algorithm is shown in Figure 3.1.

Due to the high specificity of the impact determining statements, this method worked for the situations that were found. It is very likely, however, that many interactions were not accounted for, due to the large number of ways two particles, even with set sizes and shapes, can impact. This method was also specific to the shape and size of the particle, as the calculations were made using exact distances, therefore it would not be very useful going forward as if
we wished to model a different size or shape of particle, the whole algorithm would need to be rewritten. This was important as the more varied the particles the model can account for, the more useful it will be. Even with the minimal number of interactions actually accounted for, the model was slow as it had to check through each interaction before finding the relevant one. Finding all of the possible interactions for the specific particle shape and size would have taken an inordinately long time and not been useful, therefore, a new method was investigated. In Figure 3.1, the particles added are displayed as integer values from 1 to 9 , with the gaps between them shown as 0 s.


Figure 3.1: An example of a system created by the early 2D algorithm, with the diamond particle shapes, denoted by non-0 values, highlighted

### 3.1.1.2 Implementation of the Contour Plot Method

In the previous model, the particles were a diamond shape as it was the easiest to draw and stack without calculations. However, in this revised model the particles were altered to be circular. By inputting a radius, the user was able to choose the size of the particles at the beginning of each run. The input of the particle into the array could also be done more simply by using the radius and Pythagoras theorem.

The new particle addition method not being specific to shape or size, rather being variable, made this possible. The size of the overall box was also now based upon the particle size that was entered, and when multiple particle sizes were added, the largest radius was used to calculate the box size. This ensures that a sensible number of particles are able to be added to a system.

In addition to the original array, which showed where the particles were placed, and the space they took up in the same way as the previous model, there was a second array which showed a 'contour plot' of the grid. This contour-plot showed the particle bed with no distinction between individual particles, and with a line across the edge of the current particle bed showing the closest "safest spots" that a particle could be added on top of the particle bed. This allowed the lowest point along this line to be identified for the new particle to be placed, within certain bounds of the impact point. The model now also outputted the grid to a text file in a format that could be read by MATLAB; this allowed for improved presentation, as the command line output was difficult to observe for long periods of time.

A new particle would be inputted into the system at a random $x$ coordinate at the top of the system and then fall until it impacted with a previously placed particle. At this point, the above mentioned contour plot would be created to determine the nearby low point for the particle to roll to from its impact point.

This model was a considerable step up from the initial model, however it still needed to search through the grid to find the contour plot points, at this point the grid was relatively small, as it would need to be scaled up later this method would also become less and less feasible the larger the grid became.

### 3.1.1.3 Removing the Grid

To address this, the 'real' grid, that denoted each spot with ' 1 's and ' 0 's, was removed and replaced with arrays that saved the centre points and radii of the
particles. For the initial version of this model the contour plot was removed, and instead distance calculations were made between the centres of the current particles and the proposed centre of the new particle. By checking the distance against the combined radius of the particles, it could be determined if they were too close to each other (i.e. overlapping) or not, and so whether the particle could be placed there. However, due to this being the only check present, the particles filled up the grid leaving some unwanted gaps between them, as the only check was whether or not the particles were overlapping, with no preferences for realistic stacking.

The model now had to change how it output the particles, as the previous output, the array, no longer existed to be printed. Instead, the centre coordinates and radii of each particle was output to a file, and the code was written to allow MatLab to take the output and visualise them.


Figure 3.2: A system created by the 2D algorithm where particles are only placed if they contact another particle

### 3.1.1.4 Sections and Variable Grid

Now that the model was running faster due to the removal of the visual array, the contour plot was reintroduced alongside the new distance calculations, both making sure that the particles were not overlapping and were in more realistic stable positions. However, in order that the contour plot did not have to be created for the whole grid, the large grid was split into $5 \times 5$ sections; when
a particle's centre point was saved, it was also noted in which section it was placed. Therefore, when a new particle was added, a local contour plot was created of that section, allowing the model to finalise the placement based upon the initial distance calculation. Initially these sections, and the grid itself, had set sizes due to it being simpler at the time. However now that different particle sizes were able to be added, which is discussed further below, the smaller sections, and the grid as a whole, needed to be able to accommodate this variation. Therefore, the sections and grid were changed to have a variable size, dependant on the largest particle radius that had been entered, thus ensuring that both the grid and the contour plot would be able to handle the size of the particles, ensuring a sensible number of particles were present in each grid section. The reintroduction of the contour plot along with the changes to how the particle data was saved, greatly increased the speed at which the model ran as well as improving its accuracy.

### 3.1.1.5 Top-Down Filling

All iterations of the model, after the first, simulated a particle falling into a box. This worked by looping the particle's location from the bottom to the top of the box, so that the lower points would be found first. However, when working with particles of different sizes, this resulted in smaller particles being placed in gaps between larger particles that should no longer be accessible. At first a method of trying to determine if a space would be underneath another particle was investigated, however this greatly increased the runtime of the model, as well as not always functioning correctly. Therefore, the model was changed so that instead of searching upwards for the first available space, the particles are lowered into the box until they impacted something else. The contour plot would then be used to refine the final position after impacting with the bed, in the same method as in the previous model algorithms.

Initial Impact



Final Placement


Figure 3.3: The stages a particle goes through when being added to the system. a) Falling at a random $x$-coordinate until impacting the bed. b) The contour plot being formed to show possible points of rest.
c) The particle moving down the contour plot to a low point.

### 3.1.1.6 Score Based Positioning

Previously, the particle would simply pick the lowest point along the contour plot that was within a certain distance of the initial impact point. However, this was very basic and it did not result in particles being placed in inappropriate positions. As shown in Figure 3.4, the closest low point, (b), to the impact point, (a), would not be the correct final position as it would instead roll down the slope to the right and rest at (c).
a)
b)


Figure 3.4: An example of a possible incorrect position. a) The point of impact. b) The closest low point. c) The correct resting point.

Therefore, once the contour plot was created, each valid position along it was given a score based upon how close it was to the initial impact point, and how high up in the box it was. Preference was given to being close to the initial impact site and being lower down in the box. Each point was then ordered based upon its score, and the model then looped through them from best to worst until a point passed the final checks. This helped with the realism issue, however it did not fix it completely. Therefore, the score system was implemented in a way that when more criteria were conceived to make the point selection more accurate, they could easily be added to the model.

### 3.1.1.7 Set Allocatable Array

Once the functionality of being able to add particles of a chosen size was added, the arrays used in the model were made so that their size was allocatable at the beginning of the model, allowing them to be changed to fit the size of the particles being added. The contour plot array had its size changed each time it was created as depending on the location of the particle it might need to search adjacent sections of the box.

Due to the array having to be reset each time a new particle was added, it occasionally caused the model to crash. Even after attempting a debugging of this issue, it still is not fully understood why these crashes occurred, only that they were caused by the re-allocating of the array. Owing to this, from here on in, the contour plot array was set to have the largest size it would need, instead of having its size changed each time it was used.

### 3.1.1.8 Increase Position Criteria

To increase the accuracy of the selection of the final position of the new particle, a check was added to ensure that the new particle was resting on top of two others. This was first done by confirming that there were two particles
close to the new location being tested, and then ensuring the centre point of the new particle would rest in between, above and in contact with them.

The other change was made to ensure that this would work from the beginning of a run was that the model now started with the box having a base layer of particles already present instead of being empty, as a particle landing on the bottom of the box would have failed this check.

### 3.1.1.9 Sliding downhill instead of jumping to final position

As the score-based positioning was still occasionally resulting in an inaccurate placement for the particles, as sometimes it would jump over particles to get to its resting place shown in Figure 3.4, the way the particles interact with the contour plot was changed. A simpler approach of having the particle jump to the nearest contour plot point to its impact location, and then looking at the height of the contour plot points to either side of it. It then moved to the point that was lower than it, if they are the same height then it moves to a random side, which then repeats until both points either side of the resting point are higher than it. This method means that particles now accurately slide as if under gravity to their final destination without jumping over particles they would normally be stopped by. Note that the algorithm does not consider conservation of momentum or frictional forces explicitly, but instead the model assumes a gentle settling of the particles with motions dampened by the solvent.

### 3.1.1.10 Real Final Values

Currently, whilst the particles are not placed on a grid as in the method initially used, the outputs are still based upon a coordinate system. This resulted in the MatLab output having some gaps between particles due to the coordinates being integers and drawing circles within the grid. The next step was to edit the model so that once the integer positions for each particle have
been found, the integer values are edited to real values to eliminate the unphysical gaps appearing in the visualisation.

This was done by removing the rounding from the calculations and allowing the values to be saved as real variables. This required a change in how the values were then referenced as the real variables were not able to be used as coordinates for the arrays, so instead of referencing the particle number by location, the location was now referenced by the particle number.

### 3.1.1.11 Final Optimisations

It was at this point that the 2D algorithm was deemed to be working, however a few more optimisations were added so that it ran more efficiently. These included removing looking at smaller boxes as it did not increase the speed of the model and instead resulted in more work for the model to separate the system. This is due to the size of the systems being simulated, as splitting up and reforming the whole systems into smaller boxes, was not efficient due to the small size of the overall system. Were the system to be scaled up to a much bigger size, this method would likely again become more efficient. As work on the 3D algorithm progressed and the stochastic optimisation method was finalised, discussed in section 3.2.1.2, this was retroactively added into the 2D algorithm as although it gave the same results as the equations discussed in section 3.1.2, the stochastic optimisation method was much more efficient.

Finally, more checks were added for instances when the model cannot find a valid spot for the particle to rest; this ensured that there is not a valid point close by that the model has missed.

### 3.1.1.12 Undergraduate MEng masters project work, Lewis Cartwright and Luke Convery.

The work around the forces present at the contact points of the particles under a shear force was carried out by two MEng students, Lewis Cartwright and Luke Convery, using structures supplied by the 2D model I generated.

When forces are applied on the top and bottom of a system, it results in torque on the outer particles on which the force is applied, that is then transferred through particle-to-particle contacts throughout the system. To balance this torque, the angle of rotation for each particle is required, which then allows the relative stress at each point of contact to be calculated. This was done by using the following steps and equations. The variables used within these equations are defined at the end of this section in Table 3.1.3,4

1: Calculate the position of the ends of the springs on each particle ( $i=1$ to n).

$$
\begin{align*}
& x_{i_{2}}=\left(x_{i_{1}}-x_{i_{c}}\right) \cos \theta_{i}+\left(y_{i_{1}}-y_{i_{c}}\right) \sin \theta_{i}+x_{i_{c}}  \tag{3.1}\\
& y_{i_{2}}=\left(x_{i_{1}}-x_{i_{c}}\right) \sin \theta_{i}+\left(y_{i_{1}}-y_{i_{c}}\right) \cos \theta_{i}+y_{i_{c}} \tag{3.2}
\end{align*}
$$

2. Calculate the forces caused by the particle-particle interactions ( $\mathrm{i}=1$ to n).

$$
\begin{equation*}
F_{h_{i_{\text {jnew }}}}=\binom{x_{j_{2}}-D_{x_{j}}}{y_{j_{2}}-D_{y_{j}}}-\binom{x_{i_{2}}-D_{x_{i}}}{y_{i_{2}}-D_{y_{i}}} \tag{3.3}
\end{equation*}
$$

3. Calculate the forces caused by particle-wall interactions ( $\mathrm{i}=1$ to n ).

$$
\begin{equation*}
F_{h_{w_{i}}}=\binom{x_{w_{i}}}{y_{w_{i}}}-\binom{x_{i_{2}}}{y_{i_{2}}} \tag{3.4}
\end{equation*}
$$

4. Calculate the resultant force through the sum of all forces acting on a particle ( $\mathrm{i}=1$ to n ).

$$
\begin{equation*}
F_{R_{i}}=F_{s_{i}}+\sum F_{h_{i j}}+F_{h_{w_{i}}}=\binom{x_{R_{i}}}{y_{R_{i}}} \tag{3.5}
\end{equation*}
$$

5. Calculate the torque from the initial shear force on each particle (for $\mathbf{i}=1$ to n ).

$$
\begin{align*}
& P_{s_{i}}=\binom{x_{s_{i}}}{y_{s_{i}}}-\binom{x_{i_{c}}}{y_{i_{c}}}  \tag{3.6}\\
& \tau_{s_{i}}=F_{s_{i}}^{P_{s_{i}}}=F_{s_{x_{i}}} P_{s_{y_{i}}}-P_{s_{x_{i}}} F_{s_{y_{i}}} \tag{3.7}
\end{align*}
$$

6. Calculate the torque caused by particle-particle interactions (for $\mathrm{i}=1$ to n ). Note that $F_{h_{i j}}$ is used here and not $F_{h_{i j_{n e w}}}$ as only the torque from the particles rotation is calculated here, not the particles displacement.

$$
\begin{align*}
& P_{p_{i j}}=\binom{x_{i_{j}}}{y_{i j_{2}}}-\binom{x_{i_{c}}}{y_{i_{c}}}  \tag{3.8}\\
& \tau_{p_{i j}}=F_{h_{i j}}^{P_{p_{i j}}}=F_{h_{x_{i j}}} P_{p_{y_{i j}}}-P_{p_{x_{i j}}} F_{h_{y_{i j}}} \tag{3.9}
\end{align*}
$$

7. Calculate the torque caused by particle-wall interactions (for $\mathrm{i}=1$ to n ).

$$
\begin{align*}
& P_{w_{i}}=\binom{x_{w_{i_{2}}}}{y_{w_{i_{2}}}}-\binom{x_{i_{c}}}{y_{i_{c}}}  \tag{3.10}\\
& \tau_{w_{i}}=F_{h_{w_{i}}}^{P_{w_{i}}}=F_{h_{w_{x_{i}}}} P_{w_{y_{i}}}-P_{w_{x_{i}}} F_{h_{w_{x_{i}}}} \tag{3.11}
\end{align*}
$$

8. Calculate the torque created from the displacement of each particle (for i $=1$ to $n$ ).

$$
\begin{equation*}
\tau_{D_{i j}}=F_{R_{i}}^{P_{p_{i j}}}=F_{R_{x_{i}}} P_{p_{y_{i j}}}-P_{p_{x_{i j}}} F_{R_{y_{i}}} \tag{3.12}
\end{equation*}
$$

9. Calculate the overall torque on each particle from the sum of their torques (for $\mathrm{i}=1$ to n ).

$$
\begin{equation*}
\tau_{R_{i}}=\tau_{s_{i}}+\tau_{w_{i}}+\sum \tau_{p_{i j}}+\sum \tau_{D_{i j}} \tag{3.13}
\end{equation*}
$$

10. If the overall torque and resultant force are below 0.001 , exit the program and output results.
11. If either value of the overall torque or resultant force is over 0.001 , adjust the value of the angle of rotation and the displacement vector (for $\mathrm{i}=1$ to n ).

$$
\begin{align*}
& \theta_{i}=\theta_{i}+\left(0.2 \frac{\tau_{i}}{r_{i}^{2}}\right)  \tag{3.14}\\
& D_{i}=D_{i}+\alpha F_{R_{i}} \tag{3.15}
\end{align*}
$$

12. Return to step 1.

Table 3.1: Variables used within the above equations to determine the forces present at each contact point in a system when placed under a shear force.

| Variable | Symbol | Unit |
| :---: | :---: | :---: |
| Angle of rotation for particle $i$ | $\theta_{i}$ | radians |
| Updated $x$ or $y$ coordinate of the spring location for particle $i$ | $x_{i_{2}}, y_{i_{2}}$ | mm |
| Current $x$ or $y$ coordinate of the spring location for particle i | $x_{i_{1}}, y_{i_{1}}$ | mm |
| $x$ or $y$ coordinate of the centre of particle $i$ | $x_{i_{c}}, y_{i_{c}}$ | mm |
| Updated force between particles $i$ and $j$ | $F_{h_{i j n e w}}$ | N |
| Updated $x$ or $y$ coordinate of the spring location for particle $j$ | $x_{j_{2}}, y_{j_{2}}$ | mm |
| Displacement of the $x$ or $y$ coordinate of particle $i$ | $D_{x_{i}}, D_{y_{i}}$ | mm |
| Displacement of the $x$ or $y$ coordinate of particle $j$ | $D_{x_{j}}, D_{y_{j}}$ | mm |
| Force caused by particle-wall interactions for particle $i$ | $F_{h_{w_{i}}}$ | N |
| $x$ or $y$ coordinate of the contact point between the wall and particle $i$ | $x_{w_{i}}, y_{w_{i}}$ | mm |
| Resultant force acting on particle $i$ | $F_{R_{i}}$ | N |
| Applied shear force to particle $i$ | $F_{s_{i}}$ | N |
| Position vector used for shear force torque for particle $i$ | $P_{s_{i}}$ | mm |
| $x$ or $y$ coordinate of the shear force being applied to particle $i$ | $x_{s_{i}}, y_{s_{i}}$ | mm |
| Torque due to applied shear force for particle $i$ | $\tau_{s_{i}}$ | nm |
| $x$ or $y$ coordinate of the position vector used for shear force torque | $P_{S_{x_{i}}}, P_{s_{y_{i}}}$ | mm |
| Position vector used for particle-particle torque between particles $i$ and $j$ | $P_{p_{i j}}$ | mm |
| $x$ or $y$ coordinate spring end attached to particle $i$ after rotation | $x_{i j_{2}}, y_{i j_{2}}$ | mm |
| Torque due to particle-particle interactions between particles $i$ and $j$ | $\tau_{p_{i j}}$ | nm |
| $x$ or $y$ coordinate of the position vector used for particleparticle torque between particles $i$ and $j$ | $P_{p_{x_{i j}}}, P_{p_{y_{i j}}}$ | mm |
| Position vector used for particle-wall torque for particle $i$ | $P_{w_{i}}$ | mm |
| Updated $x$ or $y$ coordinate of the contact point between the wall and particle $i$ | $x_{w_{i_{2}}}, y_{w_{i_{2}}}$ | mm |
| Torque due to particle-wall interactions for particle $i$ | $\tau_{w_{i}}$ | Nm |
| $x$ or $y$ coordinate of the position vector used for particleparticle torque between the wall and particle $i$ | $P_{w_{x_{i}}}, P_{w_{y_{i}}}$ | Mm |
| Torque due to the displacement of particle $i$ by particle $j$ | $\tau_{D_{i j}}$ | Nm |
| Resultant torque for particle $i$ | $\tau_{R_{i}}$ | Nm |
| Torque for particle i | $\tau_{i}$ | Nm |
| Radius of particle $i$ | $r_{i}$ | Mm |
| Displacement of particle $i$ | $D_{i}$ | Mm |
| Angle between contact point and $x$-axis | $\alpha$ | radians |

### 3.1.2 Code Walkthrough

This next section will go through the algorithms used in the final version of the 2D model to show how it works through each stage.

The code is broken into three subroutines: the initial setup; when the particle is falling; and then its final placement. In addition, there is one module that contains all of the universal variables that are carried across all three subroutines.

The main variables contained within the module are: the box dimensions; the number of particles; the radii being used; and the stored positions of the already placed particles.

The first part of the initial setup subroutine sets up the local variables that are required, and then requests the user to start the program. The user is then prompted to enter how many different radii they would like to be present in the system and to enter those radii. Next, the model determines which of the entered radii is the smallest and which is the largest, to use when determining the size of the box. When the program is being looped to produce multiple results, this section is omitted, since the radii is already known and to stop the program being interrupted by prompting the user for inputs.

Now that the size of the particles present is known, the box size can be determined. This is based on the largest particle radius so that a sensible number of large particles can fit, instead of having a system containing too few particles to form a sufficiently sized bed. The box size can then be used to allocate the size to various arrays used later in the algorithm. These include the array that contains the entire contour plot, which is still a grid of the box that contains a point for each integer spot within the box, and the "Ones" array, which stores the coordinates of the valid points on the contour plot, so named as a contour plot point is one of three options, either " 0 " denoting a blank
space, a "-", denoting being covered by a particle, or a "1" denoting being a valid point based on the distance from the current bed.

In the looped algorithm, the model now enters the section of code that will be looped for a number of times equal to the number of overall beds that has been requested to be simulated.

The next stage of the model is to place the initial bed layer of particles into the box, shown in Figure 3.5. This is done by randomly picking a radius, from the inputted radius options, and an $x$ coordinate within the boundaries of the box. The model confirms that this position, using the particles radius as its $y$ coordinate, is not already covered by another particle. As the particle is resting upon the base of the bed, no other conditions are required, so once this check is passed the particle location is saved, and this section of the algorithm looped to place the rest of the initial bed layer. This loop goes for a sufficiently large number of iterations, currently set at 10000000. Due to the possibility of there still being a position where a particle could still rest upon the bed, the model then loops across all of the bottom layer of the bed, using the smallest particle radius as the $y$ coordinate, checking if there are any more places for a particle to fit.

Following this the program starts looping the second subroutine to add in the rest of the particles to the box, shown in Figure 3.6. This is done as many times as needed until the box is full, or the number of particles specified has been reached.

After initialising the second subroutine's local variables, the first check made is whether the box is full or not, as this check comes before adding a new particle in every loop. Each time the algorithm tries to place a particle beyond the roof of the box, a counter is iterated. Once this value reaches a sufficiently large value the box is deemed full, and no more particles added.


Figure 3.5 - Flowchart showing the stages the algorithm goes through to produce the base layer of particles for a bed system

For each particle added, a random particle radius is chosen from the list of entered radii and a random starting spot is chosen at the top of the bed, by generating an $x$ coordinate within the bounds of the box size. The third subroutine is called at this point whilst the particle is falling. This subroutine takes the starting position of the particle and iterates the $y$ coordinate
downwards one step at a time. At each point the model confirms that it is not touching another particle allowing the loop to continue. Once an impact does occur, the model saves the location of the impact and moves back into the main second subroutine.

At this point the model creates a contour map of the system, to locate the highest points that a particle can rest upon. The particle jumps from the location of impact to the nearest of these points, and then compares the height of the two points either side of it. The model then moves in the direction with the lowest $y$ value, simulating gravity, until it reaches a point where the contour points on both sides are higher than it, so it rests there.

However, at this point the location of the particle is still saved as an integer, resulting in gaps between particles due to rounding. As a result, using the location of the two particles it is resting on, and the distances between them, the model calculates the triangle that the three particles make to determine the final real values of the new particles coordinates. The distances between the original particles and the new particle are the sum of the radii of the particles. Knowing these three distances, a triangle can be formed between the centre of the three particles of which the angles can then be calculated. The gradient of the lines connecting the new particle with the old particles can then be calculated, then allowing the final determination of the centre point of the new particle.

Checks are then run to confirm that: the new particle is resting upon the old ones instead of attempting to balance over an edge; that the new particle is not overlapping with any old particles; and that it is contained within the box. Having passed these tests, the coordinates are then saved into the list, and the model then resets the appropriate values and loops back to the start of the particle addition subroutine.


Figure 3.6 - Flowchart showing the stages the algorithm goes through to add particles to fill up a bed system

Once the box is full, or a specified number of particles have been added, the model returns to the initial subroutine where the user is prompted as to whether they want to save the list of particle locations, their contacts, the contour map from any particle addition, or calculate the particle fraction of the system. Currently, the model saves these files to the same folder as it is contained in.

A final query then confirms the user understands the model is about to end.

### 3.1.3 Simulations Run

All of the runs completed using the 2D algorithm were completed on ARCHIE-WeSt ${ }^{5}$, a regional supercomputer centre based at the University of Strathclyde.

500 systems were created for each of the following systems: radius 10 , radius 10 and 20 , and radius 10 and 50 (henceforth when referring to particle sizes in a system, the notation $r_{p}=$ "radius" will be used. Binary mixture systems shall be referred to as $r_{p}=$ "radius a ", "radius b"). The ratio of addition for each radii in these system is $1: 1$.

Each of these systems had its packing fraction calculated, the number of contacts each particle had determined, and the size of individual voids present calculated. The algorithms that determine these values are described in section 3.3.

100 runs were also created for investigating percolation with $r_{p}=10,20$ at the following ratios of addition Large:Small particles: 1:1, 1:1.5, 1:2, 1:2.25, and 1:2.5. The percentage of these structures that contained a percolation chain was determined.

Particle sizes in these and future runs were chosen as round numbers that could easily be used for different size ratios, as the model can handle particles
with non-rounded values, however is it much easier to discuss particle ratios of 10:20 than e.g. 17:34.

### 3.2 3D Algorithm Methodology

As mentioned above, the program was modified so that it could replicate the packing of particles in 3D as well as 2D and produce images as well. A 3D version of this model would allow us to gain a much better insight into how the packed bed forms, and its properties, due to the increase in accuracy that the third dimension brings, and also due to it being a more realistic simulation of what would be happening in a real-life experiment.

### 3.2.1 Timeline of Changes

This section looks through the stages that the 3D algorithm went through and the reasons behind each of the changes, from its initial setup to the algorithm used to produce data discussed in the later sections.

### 3.2.1.1 2D to 3D changes

Whilst changes had to be made to create the 3D algorithm from the 2D version, it retained its previous structure of three subroutines and a module. The first thing changed from the 2D algorithm was the addition of the $z$ axis into every stage of the model, and variables to account for the new coordinates in the particles' locations.

Another change from the 2D algorithm is that the particle is now looking for three particles to rest on instead of just two. It was decided that the possibility of a perfect square forming and requiring four particles to be rested on was exceedingly rare and not worth adding into the model.

With the extra dimension also comes the possibility of a particle resting in a corner spot, so the model is now able to detect when a new particle is close
enough to two walls, and therefore only needs one particle to rest on, and then be up against the corner. A discussion was held with my supervisors as to whether to implement periodic boundary conditions, and at this stage it was decided to leave its implementation until later. Unfortunately, this did not come to pass as focus was shifted to work on the chain particle algorithm.

### 3.2.1.2 Stochastic placement

The main detail added into the 3D algorithm, different from the 2D version, is the change from calculating the final real position of the new particle; instead determining it through a stochastic optimisation function. This function works by taking the contour plot point closest to the impact and making small adjustments, in each direction, until a position is reached that satisfies the previous 2D algorithm conditions, i.e., resting on the correct number of particles, resting in between their centre points. This ensures that there are no errors during the calculation making it much more reliable, as previously on occasion the model returned a null value using the old method.

A version of this algorithm is shown in Figure 3.7, with some altered variable names for ease of presentation. Lines 1 to 7 set up the initial variables with their desired values, with newCoords containing the current position of the particle to be adjusted, stochDists containing the distances between that particle and the two particles it will be adjusted to be resting upon, sumDist being the sum of those two distances, and $d x$ being the size of the adjustments being made. The outer loop, controlled by the integer " $a$ ", is the number of times the adjustments will be scaled down, which occurs at lines 11 to 12. Each loop the adjustment factor is reduced by a factor of 10 .

The main inner loop, controller by the integer " $c$ ", is how many adjustments are made at each scale. For each adjustment, a random number is determined between -1 and 1, which is then multiplied by the adjustment scale to produce
a value which is then added to the current $x$ or $y$ value. The adjustments made to the $x$ and $y$ values of the particle are separate, shown in lines 13 to 16.

In lines 19 and 20, the distances between the particle being adjusted and the resting particles are recalculated for its new position. PartCoords(b,1) and PartCoords( $b, 2$ ) being the $x$ and $y$ values of resting particle $b$ respectively. The radii of the two particles for each distance are also subtracted, to give the distance between their edges, rather than their centres. If the distance is less than 0 , it means the particles are now overlapping and this adjustment is not saved, accomplished by setting the "ibad" variable to 1 , shown in line 22. The other check made to allow the new position to be saved is that the sums of the distances between the resting and new particles is lower than at the previous location, as the aim to is reduce this value to 0 , without going under it. If these conditions are met, the new locations are saved, shown in line 28, the sum distance stored, line 30, and then the new adjustment made.

Once all the loops have been completed, the final positions calculated are saved into new variables, lines 34 and 35 , that are then used going forward.

```
newCoords(1) = TempX
2 newCoords(2) = TempY
3 newCoords(3) = TempZ
! These variables store the current integer position of the particle to be adjusted
stochDists(1) = FinalPartDist1,2)
stochDists(2) = FinalPartDist(2,2)
stochDists(3) = FinalPartDist(3,2)
! These variables store the distances between the new particle and the particles it will
be resting upon
sumDist = stochDists(1) + stochDists(2) + stochDists(3)
! . This variable stores the sum of the above distances, and is the value we are trying to
minimise
dx(1) = 10 * RadLarge
9 dx(2) = 10 * RadLarge
10 dx(3) = 10 * RadLarge
! These variables store the starting amounts by which the position will be adjusted
11 do a=1, 10
! This loop determines the number of times the adjustment amount will be shrunk
12
13
        do b=1,3
            dx(b) = dx(b) / 10 ! This shrinks the adjustment value
```

$15 \quad$ do $c=1,500$
! This loops determines the number of adjustments made to the particle

This loops determines the number of adjustments made to the particle do $b=1,3$ call random_number(RX) stochxnew $(\bar{b})=$ newCoords $(b)+d x(b)$ * (2*RX-1)
end do
! For each coordinate ( $x, y, z$ ), they are adjusted by a random fraction of the total adjustment value
$21 \quad$ do $b=1,3$
! The new distances between the particles are calculated based on the adjusted positions
22 stochDists(b) = ((PartCoords(b,1) - stochxnew(1))**2) + ((PartCoords(b,2)-stochxnew(2))**2)

```
23 stochDists(b) = sqrt(stochDists(b)) - RadT -
```

MLr(FinalPart(b,1))

24 if (stochDists $(b)<0)$ then
! If the particles are overlapping then a variable (ibad) is set to 1 , to ensure this adjustment is rejected
$25 \quad$ ibad $=1$

26
27
28
! The new total distance is calculated
29 if (stochynew < sumDist .and. ibad == 0) then
! If this distance is smaller than the previous distance and there are no overlaps, the new location is saved
! This process repeats with the adjustment distance shrinking each time to obtain more specific adjustments until a precise location is determined for the new particle

37 New $X=$ newCoords(1)
$38 \quad$ New $Y=$ newCoords(2)
$39 \quad$ New $Y=$ newCoords(3)
! The final particle location is then saved
Figure 3.7: Stochastic optimisation algorithm used for shifting particles from the integer spot on the contour plot to the real location resting on top of their nearest particles

### 3.2.1.3 Extra checks

Some extra checks were also added to ensure that the model is able to find the correct resting point, as this was where the model was having most of its issues due to the higher complexity of the 3D contour map. These involved allowing the model to change the resting particles to look at other nearby options until it found the particles that it should be being rested on. In the case of an overlap, the model replaces one of the current resting particles with the particle being overlapped with, as an overlap meant that the new particle should be resting on the overlapped particle. As shown in Figure 3.8, particle $D$ is being added to the system and incorrectly attempted to rest upon particles $A$ and $B$. This causes an overlap with particle $C$, so the algorithm swaps $C$ with the closest of particles $A$ or $B$, which in this case is particle $B$, so that it becomes a resting particle. This then allows particle D to rest correctly. Figure 3.8 is a 2D representation of the 3D issue for the ease of visualisation, however these checks were also added in future versions of the 2D code used for the chain particles algorithm.



Figure 3.8: Representation of an particle placement on the left where particle $D$ has incorrectly rested on particles $A$ and $B$, but then is corrected in the right image to be resting upon particles A and C .

Further checks were required for when the particle is near the edge of the box. Previously there has been a binary statement for if a particle was resting against an edge or not, meaning that if the particle finds itself one spot away from the edge, it would still be looking for three particles to rest upon. However,
now it is able, when near the edge to swap between looking for an edge resting spot or not, once it has exhausted its other possibilities.

### 3.2.2 3D Code Walkthrough

This next section will go through the code used by the final version of the 3D model to show how it works through each stage.

As with the 2D code, it is broken into three subroutines: the initial setup; when the particle is falling; and then its final placement, and one module which contains all of the universal variables that are carried across all three subroutines.

The main variables contained within the module are: the box dimensions; the number of particles; the radii being used; and the stored positions of the placed particles.

The first part of the initial setup subroutine sets up the local variables that are required, as mentioned in the 2D algorithm section, and then requests the user to start the program. The user is then prompted to enter how many different radii they would like to be present in the system and to enter those radii. The model then determines which of the entered radii is the smallest and largest, to use when determining the size of the box. When the program is being looped to produce multiple systems, this section is omitted as the radii are already known.

The next stage of the model is to place the initial bed layer of particles into the box. This is done by randomly generating $x$ and $z$ coordinates, confirming that there is no other particle already overlapping, and then saving the particle there. The $y$ coordinate of each of the particles is equal to their radius. A final check is then run to confirm that there are no available positions by looping through the box, looking for a position that a particle can fit in.

After this the program starts looping the second subroutine to add in the rest of the particles to the box. This is done as many times as needed until the box is full, or the number of particles specified has been reached.

After initialising the second subroutines local variables, the first check made is whether the box is full or not, as this check comes before adding a new particle in every loop. A random particle radius is then chosen from the list of entered radii and a random starting position is chosen at the top of the bed. The third subroutine is called at this point whilst the particle is falling. The particle iterates downwards one coordinate at a time, and at each point the model confirms that it is not touching another particle. Once this does occur, the model saves the location of impact and moves back into the main second subroutine.

At this point the model creates a contour map of the system, to locate the highest points that a particle can rest upon. The particle jumps from the location of impact to the nearest of these points and then starts moving along them in a downwards direction, to simulate gravity. As in the 2D model, once it reaches a point where all adjacent contour points are higher than it, it rests there.


Figure 3.9: Contour map showing possible points for a new particle in a small system of 3D particles

However, at this point the location of the particle is still saved as an integer, so there would be gaps between particles due to rounding. Therefore, as described earlier, the model uses a stochastic optimisation function to move the final location around in increasingly small increments, to try and reduce the distance between the new particle and all the particles it is resting on to 0 .

Checks are then run to confirm: that the new particle is resting upon the old ones instead of attempting to balance over an edge; that the new particle is not overlapping with any old particles; and that it is contained within the box. Having passed these tests, the coordinates are then saved into the list, and the model then resets the appropriate values and loops back to the start of the particle addition subroutine.

Once the box is full, or a specified number of particles have been added, the model returns to the initial subroutine where the user is prompted as to whether they want to save: the list of particle locations; their contacts; the contour map from any particle addition; or calculate the particle fraction of the system. The latter two of these were removed in the finalised version of the algorithm, as
the contour map was used for error checking, and an alternative method was used for calculating the packing fraction. Currently, the model saves these files to the same folder as it is contained in.

A final query then confirms the user understands the model is about to end.

### 3.2.3 Simulations Run

All of the 500 runs completed for each system using the 3D algorithm were performed on ARCHIE-WeSt ${ }^{3}$. The ratio of addition for each radii in these system is $1: 1$.

Each of these systems had its packing fraction calculated and the number of contacts for each particle was determined.

100 binary mixture systems were also created for investigating percolation with $r_{p}=10,20$ at the following ratios of addition Large:Small particles: 1:1, $1: 2,1: 3,1: 4,1: 5$, and $1: 6$. The percentage of these structures that contained a percolation chain was determined.

### 3.3 Other Functionalities and Data Collection

Throughout creating the model, there have been functionalities added and removed that have been separate to how the model runs but have given options for the user to process the information produced.

At the start of the program, it requests the input of the radius that will be used for the particles in the model. The model also asks how many different particle sizes are needed, currently allowing for between 1 and 5 , so there can be variation in the sizes present. Certain versions of the model also allow the user to enter a mean and standard deviation, to allow the model to place particles with sizes of a standard distribution based upon the inputted data instead of a binary sized system, allowing more realistic systems to be created. However
this was left as a separate option within the algorithm and not investigated further.

Different methods of particle addition have been investigated, with the packing being ordered from the bottom to the top, as well as placing the particles randomly throughout the box with no need for them to be in contact with each other. This can be used to simulate the particles in suspension in solution, however at this time it has not been investigated further in favour of refining the packed particle bed approach.

The program also has the capability to calculate the fraction of the box that is either voids between particles or occupied by particles, as well as the sizes of the individual voids present in the system. These values can be used to compare against known values to confirm the realism of the model, as well as gain more information about the structure of the system created.

The algorithm counts each particle in the system by its radius, and then works out the total area, or volume in 3D, of particles of each radius, as shown in Equations 3.16 and 3.17. When summed, this value represents the total area of the system that is present as particle surface. This is then divided by the total area, or volume, of the box to gain a fraction of the system that is then covered by particles.

$$
\begin{align*}
& \text { Area }=\left(p_{1} *\left(\pi * r_{1}^{2}\right)\right)+\left(p_{2} *\left(\pi * r_{2}^{2}\right)\right)+\cdots\left(p_{n} *\left(\pi * r_{n}^{2}\right)\right)  \tag{3.16}\\
& \text { Volume }=\left(p_{1} *\left(\frac{4}{3} \pi * r_{1}^{3}\right)\right)+\left(p_{2} *\left(\frac{4}{3} \pi * r_{2}^{3}\right)\right)+\cdots\left(p_{n} *\left(\frac{4}{3} \pi * r_{n}^{3}\right)\right) \tag{3.17}
\end{align*}
$$

where $p$ is the number of particles of radius $r$, and $n$ is the number of different radii present in the system.

The model can also determine the location of the points of contact between each of the particles, as well as noting which particles are in contact with each
other. This is done by looking at the distance between a particle and each other particle in the system. If the distance is equal to the sum of the two particles radii, then they are in contact. Each particle is numbered in order of when it was added to the system, so a file can be outputted showing each particles contacts using those assigned numbers, for example particle 1 is in contact with particle 3.

A section of the 2D model is also capable of determining the shapes that groups of particles make up within the system to form a void, and then calculate the area of that void. As mentioned above, the model can determine which particles are in contact with each other, this can now be used to investigate the shapes that chains of the particles form. The algorithm starts looking for three vertex shapes, where vertices can be a particle or an edge, and then increments the number vertices, up until ten. This limit was created for time management purposes as this algorithm could theoretically look for shapes with an infinite number of vertices, however ten was deemed sufficient to find most, if not all shapes, and did not use too much computational time. Starting from particle one, the algorithm loops through the list of its contacts, for each particle in contact, the algorithm then loops through its contacts. This is done recursively, looking through the system until a chain starts and ends with the same particle. Once a chain has been found, the recursive loop unwinds, storing the particle number at each step so that once it has fully unwound, the chain creating the shape is fully saved. This shape is then checked against two criteria to ensure that it a valid shape to save permanently, the first of which is that it must be a unique shape that has not already been found, i.e. a shape could be found multiple times starting from each of its vertices, and be saved as $1,2,3,2,1,3$, etc, even though they make up the same shape. The other criteria is that there are no particles within the shape found, as therefore the area calculated for that shape would not be entirely void. This is done by creating the outline of the shape between each of the particles centre points. Looping through every other particle in the system, a line is drawn from its centre to the left most edge of the box, and the
number of times it crosses one of the shapes outer lines is counted. If the total is odd, then the particle is inside the shape, and if it is even then it is outside the shape. Now that the shape has been deemed valid, it is saved, and its area can be calculated using Equation 3.18.

$$
\begin{equation*}
\text { Total Shape Area }=\frac{1}{2} \sum_{i=1}^{n}\left(x_{i} y_{i+1}\right)-\left(x_{i+1} y_{i}\right) \tag{3.18}
\end{equation*}
$$

Where $x$ and $y$ are the centre coordinates of each particle.

Once the total area of the shape between the particles has been determined, the sectors of each of the particles that overlap with this shape are calculated and subtracted from the total area, thus leaving behind the void area.

$$
\begin{equation*}
\text { Particle Sector Area }=\frac{\theta}{360} * \pi r^{2} \tag{3.19}
\end{equation*}
$$

Where $\Theta$ is the inner angle of the sector and $r$ is the radius of the particle.

The algorithm used to find percolation structures uses the same recursive loop as above, detailed in Figure 3.10, however instead of looking for loops back to the starting particle, the chains only start from particles that are in contact with the lefthand edge and terminate when they have reached a particle in contact with the righthand edge. The same check is performed to ensure that each chain found is unique before they are saved.

One of the main alternate functionalities is to have the model produce systems that are not circular/spherical. This was done by merging circular particles together to form chains, which is discussed in greater detail in Chapter 6.


Figure 3.10: Flowchart showing the stages the algorithm goes through to adjust a particles location from an integer to real value using stochastic optimisation

### 3.4 Summary and Conclusions

This chapter has discussed the algorithms produced to simulate the packing of particles in both 2D and 3D under gravity. The algorithms are able to produce realistic representations of these systems which we have been able to analyse, the data obtained from which is discussed in the following two chapters.

These algorithms will be saved on the University of Strathclyde Pure repository.

### 3.5 References

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## 4 Results and Discussion - 2D Algorithm

This chapter discusses the systems created by the 2D algorithm discussed in Chapter 2. Specifically investigating the different properties of these systems with emphasis on features that might affect the strength of the particle bed structure when placed under stress. We start by looking at the packing of the systems created, before investigating the sizes of the voids and number of contacts each particle has. Finally, the forces present within the systems and how breakages caused by the application of shear stress were investigated.

### 4.1 Binary System Beds

The radii 10,20 and 50 were chosen as they given radius ratios of 1:2 and $1: 5$, which would show either side of the range of particle size distributions. Ratios in between these ones were planned on being tested but were put to the side to focus on completing the later algorithms.

The packed bed with only $r_{p}=10$ present shows a mostly regular square lattice structure, as shown in Figure 4.1a, even with the irregularity of the initial placement of particles at the bottom of the bed. In the centre of the bed, it can be seen that the average number of contacts is four, since each particle contacts two existing particles below it, and two particles are then placed above. However, there are significant edge effects with the hard walls of the box due to the small size of the systems and lack of periodic boundary conditions.


Figure 4.1: Packed beds of particles across four systems with different radii particles present. $\mathrm{a}: r_{p}=10 . \mathrm{b}: r_{p}=10,20 . \mathrm{c}: r_{p}=10,50$.

The irregularity of the packing increases once the bed also includes larger $r_{p}=$ 20, as shown in Figure 4.1b. As the $r_{p}=10$ are not small enough to fit inside the voids created by the $r_{p}=20$, as with the $r_{p}=10$ falling above the critical size ratio value, $0.41: 1^{1}$, discussed in the literature review, they instead contribute to the increased irregularity in void shape and size and compel the larger $r_{p}=20$ to shift from a regular packing structure to accommodate for the smaller particles between them.

This effect is still apparent in the bed containing $r_{p}=10,50$, however to a lesser extent, as shown in Figure 4.1c. Due to the larger difference in particle size, two and occasionally three of the smaller particles can be seen to fit in between the larger particles without greatly affecting the placement of the particles landing above them. There are still instances of irregularity that spawn from the overabundance of smaller particles overfilling what might otherwise be a void, thereby forcing the addition of the next large particle to the side, preventing it from capping the putative void.

Note that the smaller particles filling in amongst the voids of the larger particles would increase the difficulty of washing the system, and the smaller particles forming clumps in between the larger particles would help bind them together, increasing the likelihood of agglomerates forming.

### 4.2 Packing Fractions

Table 4.1 shows the results of 500 runs of each system of different sized particles. Within these systems, the number ratio of large:small particles was 1:1.

Table 4.1: The Packing Fractions in Packed Bed Systems with different particle radii present.

|  | Packing Fraction |  |  |
| :---: | :---: | :---: | :---: |
| Particle Radii | Minimum | Average $\pm$ <br> Standard Deviation | Maximum |
| 10 | 0.757 | $0.766 \pm 0.007$ | 0.806 |
| 10,20 | 0.731 | $0.779 \pm 0.005$ | 0.791 |
| 10,50 | 0.770 | $0.781 \pm 0.005$ | 0.796 |

As the difference between the sizes of the particles present increases, the average packing fraction increases. The system with only $r_{p}=10$ has the lowest packing fraction, as whilst it is a partially ordered structure, with regions of short-range order, i.e. small sections of the system where the particles have packed efficiently, there is no way to fill in the voids between the particles. In the systems containing a larger size of particles, $r_{p}=20,50$, the $r_{p}=10$ particles are now able to sit in the voids created by the larger particles, thus giving these systems a higher packing fraction. The difference between the $r_{p}$ $=10,20$ and $r_{p}=10,50$ systems is likely due to the way that the particles pack together. This means that in the $r_{p}=10,50$ system, as previously mentioned, the $r_{p}=50$ are able to form a partially ordered structure, with the smaller particles more able to fill the voids in between. Whereas in the $r_{p}=10,20$ systems, the larger particles are pushed out further from a regular structure by the smaller particles, due to their closeness in size. When the particle radius ratio between smaller and larger particles is $0.41: 1,{ }^{1}$ or $10: 24.39$, scaling the 0.41 value to 10 , my smallest particle radius, the smaller particles can fit perfectly inside the voids created by the larger particles. For any size ratio less than this value the smaller particles can fit into the voids between larger particles. As the size of the void created by a set of same sized particles in a regular pattern is proportional to the size of the particles, once you have passed this ratio the void fraction will remain similar for the larger particles, as the $r_{p}=10$ do not affect the void formation and simply fill up space within them. The further variation in particle fraction would then come from the difference in the number of smaller particles that were placed within the voids, as it would hypothetically be possible to change the ratio between large and small particle
in order to get an extremely densely packed bed where enough smaller particles are placed in amongst the larger ones, so that all the voids were filled with closely packed small particles, with the larger particles still maintaining a fairly regular packing pattern.

The theoretical maximums for these binary systems is unknown, as they are not using ratios for which the compact packing exists. ${ }^{1}$ As adding more smaller particles to the systems shifts the larger particles out of an ordered hexagonal packing arrangement, the highest packing possible for the $r_{p}=10,20$ and $r_{p}=$ 10, 50 systems is likely to be one in which the large particles pack on their own in a hexagonal lattice, and then the smaller particles are used to fill in any space left at the top of the box where large particles no longer fit.

a)
c)


Figure 4.2: Examples of packing in systems with different particle addition methods. a) Random Sequential Adsoprtion (RSA). b) My Model. c) Triangular Lattice.

Packing fractions have been researched previously using random sequential adsorption (RSA) models, which calculate the maximum packing fraction to be roughly $0.547 .^{2}$ Our values exceed this by about 0.2 ; which is expected as while the packed beds presented here have a degree of randomness in the placement of the particles, the particles settle under gravity to create denser packing than with RSA, where particles are added at random without overlap until it is no longer possible. ${ }^{3}$

The highest possible packing fraction for a bed of circular particles of the same size is roughly $\frac{\pi}{\sqrt{12}} \approx 0.9069,{ }^{4}$ so our values fall comfortably below this. This is because the model will never achieve perfect packing in a triangular lattice due to the random nature of the structure, especially the randomness of the base layer of particles. A comparison of these packing methods and one of our systems is shown in Figure 4.2, demonstrating the differences in how packed the structures are.

### 4.3 Number of contacts between particles

The number of contacts each particle has was also investigated as it is a parameter that can give us more information about how densely packed a bed is. It is also another metric through which my model can be compared to expected values to confirm that the simulations run give usable results.

As shown in Figure 4.3, across the different systems, particles will most often have two to five contacts. Particles with fewer contacts than this are infrequent, as having zero contacts requires being one of the initial particles placed on the bottom of the box ending up with no particles laying on top, and one contact being a resulting of a particle resting against a wall and one other particle.


Figure 4.3: The frequency of the number of contacts per particle across the investigated systems.

In the systems with only $r_{p}=10$, there are no particles with greater than six contacts, as required by the geometry of packing. In a perfectly ordered system, each of the particles would have six contacts, as they would form a triangular lattice arrangement, and thus six is the maximum number of contacts possible. As our systems have a degree of disorder within them due to the randomness of the initial particle placements, it is rare for this to occur by chance, as shown by the frequency of occurrence bar in Figure 4.3 for six contacts being minimal compared to the other contact amounts. Therefore, in the middle of the bed, the average number of contacts will be four, since each particle added to the system creates two new contacts each shared by the two particles.

As larger particles are added into the system with the $r_{p}=10$, the number of contacts the particles are able to have with smaller particles increases, as the increased circumference of the larger particles allows for more contact points to be made. Figure 4.4a shows the frequency of each number of contacts for $r_{p}=10$ across each of the systems created. Figure 4.4b shows the frequency of each number of contacts for larger particles, $r_{p}=20,50$, present across each of the systems created.


Figure 4.4: The frequency of the number of contacts per particle, differentiated by the radius of the particle, across the investigated systems. a (top): Contact number frequency of $r_{p}=10$ in all three investigated systems. b (bottom): Contact number frequency of $r_{p}=20$, 50 in the investigated binary systems.

When comparing the number of contacts of just the $r_{p}=10$ (Figure 4.4a), in the systems in which they are mixed with larger particles, there is a clear difference in the number of contacts they make. In the $r_{p}=10,20$ systems, the peak moves to three contacts, with roughly half as many particles having four
contacts, then very few one or two contact particles. This is due to the increased irregularity in the systems, pushing the particles further away from the six contact "perfect" structure of the triangular lattice. Recall that the beds created with $r_{p}=10$ only have a fairly regular structure, whereas systems with larger particles present are more disordered (see Figure 4.1). The $r_{p}=10,50$ systems have similar sized peaks for both two and three contacts, with very few particles having one or four. This increase in two contact particles will be due to small particles that are resting inside a void created by larger particles, therefore having no contacts from above due the void being capped off above them.

When looking at the larger particles present within their systems (Figure 4.4b), their graphs both follow a similar pattern, with increasing frequency up to five contacts, but then decreasing from that point. The presence of the smaller particles allows for these larger particles to make many more contacts due to their increased circumference, hence the shift towards the higher number of contacts. The particles with lower numbers of contacts, such as two and three, will be due to those sitting at the bottom of the box and at the edges, as contacts with the edges of the system were not counted.

### 4.4 Individual Void Areas

Individual voids are determined as described in section 3.3, with loops of particles found that start and end with the same particle, as shown in Figure 4.5.


Figure 4.5: The order of particle looped through to find a shape that creates a void addition to create a void.

As shown in Table 4.2, the size of the smallest void present does not vary across the different beds, which is due to the high likelihood of a triangle of $r_{p}$ = 10 existing across all the beds formed, therefore the smallest void would have little variation of the area formed by these particles.

Table 4.2: The smallest, average, and largest void areas in packed bed systems with different particle radii present.

| Particle <br> Radii | Void Areas |  |  | Average Void Area Scaled <br> by Largest Particle Area |
| :---: | :---: | :---: | :---: | :---: |
|  | Min. | Average | Max. |  |
| 10 | 16 | $78 \pm 2$ | 930 | 0.25 |
| 10,20 | 16 | $190 \pm 6$ | 3300 | 0.15 |
| 10,50 | 16 | $610 \pm 23$ | 10000 | 0.08 |

The average and largest void sizes increase as the width of the size distribution is increased, which is expected as there will be voids formed solely by larger particles therefore having larger gaps in between them. However, when the void areas are scaled to be proportional, by area, to the size of the largest particle area present in the system, the scaled sizes decrease with increased size distribution. This is because the voids in between the particles
are proportional to particle area, however the larger particles allow the smaller particles to fit in between them filling up the gaps, whereas in the systems with more similarly sized particles, the gaps remain empty.

The sizes of the voids at the edges of the box are also included in the calculations, which contribute to the large maximum void sizes, as these voids will be bigger due to the flat surface of the box making up an edge, instead of the curved edge of a particle.

### 4.5 Percolation Structures

We hypothesise that the existence of percolated structures ${ }^{5}$ in the packed beds are relevant to its structural properties. The presence of these structure may inform the strength the beds have when looking at how contacts within the system are broken, discussed in section 4.8, as well as having implications on the porosity on the bed for other investigations that could be done using this model in future research.

As discussed in section 2.3.2, for our purposes, a percolation chain is a chain of connected large particles joining the left and right sides of the box. In Figure 4.6, structures formed with varying number ratios of $r_{p}=20$ to $r_{p}=10$ are shown. Percolation pathways connecting large particles only from one side of the box to the other are also shown where they exist. The results of multiple runs are reported in Table 4.3. 100 runs were completed for each ratio of the different particle sizes, and the presence of percolation structures within the bed systems determined. The shortest chains, by number of particles, are counted where they exist.


Figure 4.6: The $r_{p}=10,20$ system with different number ratios of large-to-small particles. Top left 1:1, top right: 1:1.5, bottom left 1:2, bottom right 1:2.5.

Table 4.3: The percentage of particle system runs that contained an edge-to-edge percolation chain and the shortest chain lengths present in systems with various number ratios of large-to-small particles in the $r_{p}=10,20$ system.

| Particle <br> Addition Ratio <br> (Large:Small) | Percentage of <br> Systems with <br> Percolation <br> Chains <br> Present (\%) | Avg <br> Chains | Max <br> Chains | Min <br> Length | Avg <br> Length | Max <br> Length |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1: 1$ | 98 | 102.73 | 400 | 18 | 66.28 | 108 |
| $1: 1.5$ | 82 | 113.19 | 319 | 16 | 41.98 | 81 |
| $1: 2$ | 59 | 62.29 | 300 | 17 | 32.10 | 66 |
| $1: 2.25$ | 33 | 27.27 | 350 | 17 | 32.69 | 62 |
| $1: 2.5$ | 23 | 17.48 | 200 | 18 | 30.04 | 59 |

For the purpose of determining if a percolation chain was unique, they were counted as unique chains if they were not made up of the exact same particles. For example, the blue and green chains shown in Figure 4.7 would be counted as separate chains, however the red and orange chains would be treated as the same chain and therefore only counted once.


Figure 4.7: Example percolation chains showing unique chains (blue and green), and chains treated as identical (red and orange).

As shown in Table 4.3, as the ratio of larger particles within the system decreases it becomes more difficult for percolation chains to form, however even at the lower ratios there are still some chains present, indicating that we have not yet reached the percolation threshold for this system. The site percolation threshold for a regular triangular lattice is $0.5^{6}$, and $\sim 0.59$ for a square lattice, however due to the irregularity of our structures, and the addition of smaller blocking particles, our value would likely be lower, due to these additional constraints making a chain from edge-to-edge less likely to form. The minimum possible length of a chain is 15 particles, so the minimum lengths in Table 4.3 are very close to this value, showing that almost direct chains across the bed are forming at all these ratios.

The number of chains within each system also sees an overall decrease across the systems investigated, along with the length of the chains found. This is again supported by the chains becoming more difficult to form, therefore
less are able to be made. The chain lengths do start to become more consistent at the higher particle proportion ratios. This is because in the lower particle proportion ratios, longer chains are able to be formed due to the greater number of contacts between pairs of large particles. However, once there are less contacts, the pathways are more restricted and so the shorter route becomes the only route.

### 4.6 Finite Size Effect

Runs could also be completed using larger box sizes to investigate the finite size effect ${ }^{7}$ within the model. As the packing of the particles will differ against the edge of the box compared to the centre of the bed, a larger box size will negate the effect of the edges so we can determine a more consistent packing fraction. Roughly 20 runs were completed on the system containing a 1:1 ratio of $r_{p}=10,20$ with a box four times the normal size, one of which is shown in


Figure 4.8: $r_{p}=10,20$ system at a 1:1 addition ratio in a larger box size

Figure 4.8. The average packing fraction across these systems was $0.787 \pm$ 0.003, which is more densely packed than the systems in the smaller box sizes. There was also less variation between the larger systems than between the smaller systems. This shows initially that the properties of the systems in the smaller box sizes are getting affected by the finite size effect, therefore more runs should be completed as part of future work to fully comprehend the effect of box size on these systems and a system size where the effect is minimal.

### 4.7 Bed Fragmentation

The algorithm discussed in this next section was produced by two MEng students at the University of Strathclyde working alongside my PhD project. ${ }^{8,9}$ Their projects involved taking the structures produced by my model and calculating the forces present at the contact points between the particles, using the steps described in section 3.1.1.12.

Figures 4.9 a and b show the forces present at the contact points between particles within four structures with different sized particles present. The structures used for these investigations are smaller than those used for the packing and percolation work discussed above as currently running these systems takes a long time due to the algorithm being written in VBA. The forces are represented by the coloured shapes at the contact points, with the darker blue colour representing a lower force, then colour shifting through green to yellow to represent a higher force present. The red square marks the contact point with the largest force present.

A shear force was applied to the systems with a 1-unit force across the top in the positive $x$ direction and a 1-unit force across the bottom in the negative $x$ direction. These forces were split equally between the particles on the top and bottom of each of the systems, so if there were 5 particles resting on the bottom layer of a system, 0.2-units of force would be applied to each.

b)

Figure 4.9: Forces present at the contact points within packed beds of particles across four systems with different radii particles present. The arrows show the direction of the shear forces applied to the systems. a: $r_{p}=$ 10. $\mathrm{b}: r_{p}=10,20$.

As shown in Figure 4.9a, and mentioned previously when discussing packing fractions, the system with just $r_{p}=10$ present is packed in a relatively ordered fashion when compared to the other systems. Because of this the forces are similar across the whole system, with forces being higher in the areas with more irregularity. The point with the highest force is present in the bottom left of the system, most likely due to the particle on the base of the bed having the shear force directly acting upon it, and only having one contact point for the force to be distributed through.

In Figure 4.9 b , the system with $r_{p}=10,20$ present, the structure is more disordered and therefore there is less consistency between the forces present at the contact points. The highest force is again present near the base of the bed, on a particle pressed between two base layer particles and another larger particle above it. The large void to the right of the particle also means that the increased disorder of the area of the system means the force can not spread out as easily, resulting in it accumulating on the adjacent particle.

Figures 4.10a and $b$ show the same systems as Figures $4.9 a$ and $b$, however they show the order in which contacts break upon multiple runs of the algorithm. After each run is completed, the contact point with the highest force present in the system is removed from the next round of calculations, simulating the bond being broken and allowing us to investigate the cracks that could form through the structure. If this breakage resulted in a top or bottom particle that had the shear force applied to it no longer having any contacts, the force was removed from this particle and redistributed evenly between the other particles on its level.

Both of the systems show a mostly continuous chain of breakages through the system. Figures 4.10a and b both contain cracks through the systems near the top or bottom of the bed, likely due to this being close to where the shear force is being applied. The bottom of Figure 4.10a's bed is more irregular than the top therefore it is expected for it to be less stable and have higher forces present between the particles. In Figure 4.10b, the top and bottom of the bed are closer in regularity, however the bottom of the bed does contain larger voids so the packing is not as tight, resulting in higher forces there.

a)

b)

Figure 4.10: The order of contact breakage within packed beds of particles across four systems with different radii particles present. a (left):

$$
r_{p}=10 . \mathrm{b} \text { (right): } r_{p}=10,20 .
$$

Figures 4.11a and 4.11b show the contact point forces present in two structures, one which contains a percolation chain (4.11a) and one which does not (4.11b). As shown previously, the forces present in the ordered areas of the systems are more consistent compared to the forces in areas with less ordered packing. The forces are also higher near the top and bottom of the systems, where the shear force is being initially applied, and then spreads out closer to the centre of the systems.



Figure 4.11: Forces present at the contact points within the $r_{p}=10,20$ system with different number ratios of large-to-small particles. The arrows show the direction of the shear forces applied to the systems a:

1:1, b: 1:2.5

Figure 4.11b has more ordered areas due to a higher proportion of smaller particles present allowing them to pack more tightly together, compared to Figure 4.11a which has a more equal ratio of particle sizes, causing the structure to be more irregular.

Figures 4.12a and 4.12 b show the systems from Figures 4.11 a and 4.11 b , having gone through the same analysis as in Figures 4.9a and b. The initial contact breakages in both structures occur at the base of the beds, likely due to the proximity to the application of the force. However, once these initial contacts are broken, the next contacts to break form a chain closer to the centre of the beds. In Figure 4.12a, the breakage initially follows the percolation chain through the centre of the bed from contacts three through six. Contacts seven and eight then break the percolation chain which moved downwards, maintaining the horizontal fragmentation created by the previous contacts breaking, and ending with contact nine breaking on the left edge of the bed. The last contact then breaks as still in line with the previous breakages but back on the righthand side of the bed.

Figure 4.12b contains no percolation chain, however the fragmentation also created a chain within the centre of the bed. Compared to Figure 4.12a however, the chain breaks in smaller clusters between contacts three and four, five and six, and then seven to ten.

Both breakage chains occur in the regions of the beds that have larger voids and more irregular packing structures, as these areas are less stable within the bed due to the system finding it harder to distribute the forces evenly.



Figure 4.12: The order of contact breakage within a system with a percolation chain (a: left) and a system without a percolation chain (b: right).

### 4.8 Summary and Conclusions

When comparing the packing fractions for my simulated systems to calculated values from literature, it was found that my values fell in the expected range being higher than RSA packing fractions, due to the addition of gravity simulated in the system, however they had a lower packing fraction than the calculated maximum, as there is a degree of randomness stemming from the initial base layer of particles that causes the system to shift out of a perfectly ordered lattice. There is an increase in the average packing fraction as the particle size distribution is increased, due to the ability of the smaller particles to fit inside the voids created by the larger particles, thereby decreasing the void area of the system.

When investigating the number of contacts that each particle had, the starting assumption was that in the single sized particle system, each particle would have four contacts, two from particles being rested on, and two from particles resting on it. This was found to be the case, with the majority of particles having four contacts, however there were particles with fewer contacts, likely due to the finite size effect in the small system, and some particles with more contacts, in areas where the particles were packed closer together.

The introduction of larger particles within the binary systems, caused a decrease in the number of contacts per small particle, as the systems became more irregular. In the $r_{p}=10,50$ systems, the majority of small particles had two or three contacts, as they were likely placed in between two larger particles, with potentially one more small particle, before the void was capped off. The larger particles in the binary systems have a similar contact graph to the single sized system, with the peaks being around four to six particles. This is shifted upwards from the four shown in the single sized particle system due to the additional contacts with smaller particles in the voids between the larger particles.

When calculating the sizes of the individual void areas between particles, it was found that when the average void area across a system was scaled by the largest particle area present within that system, it decreased when the particle size distribution increased. This is expected because, as previously discussed, the smaller particles in these systems are able to fill in void spaces between larger particles, so reducing the sizes of the voids within the system.

When looking for the presence of percolation chains, in this thesis defined as a chain of large particles connecting the left- and right-hand side of the box, it was found, as expected that increasing the number of small particles within the system would disrupt the formation of percolation chains. There was always a system that did not contain a percolation chain, even at a ratio of $1: 1$ large:small particles, and as the ratio of smaller particles increased the percentage of systems that contained a percolation chained decreased massively from $98 \%$ to $23 \%$ across the systems tested. The average number of chains per system, and the average length of chain per system also decreased as the number of small particles in a system increased.

When looking at the forces present at the contact points between particles, it was found that the forces were much more evenly spread in the system with the same sized particles compared to the binary particle system. This is likely
due to the packing in the binary system being less uniform, therefore creating a less stable structure, with areas of higher stress within the system where contacts are more likely to break. The order of breakage contacts do follow chains in both same sized and binary particle systems, as once a contact breaks the contacts around it are put under more stress as there is one less contact for the forces to be shared between.

When investigating the contact breakage of systems that did contain a percolation chain, it was found that the order of contact breakage followed the percolation chain through the system almost fully. However, more investigation will need to be done into these systems to determine if there is a link between the presence of percolation chains and contact breakage paths as this initial system could be due to random chance.

The 2D algorithm was created as an initial starting point due to the simplicity of creating it, and it has been shown to be capable of producing realistic systems of packed bed particles formed under gravity. It has also shown the possibility of different applications it can be applied to, such as further investigation of how the beds break apart and how the existence of percolation structures affects this. However, it was intended to be a stepping stone into the 3D algorithm, the results of which are discussed in the next chapter.

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## 5 Results and Discussion - 3D Algorithm

This chapter discusses the systems created by the 3D algorithm discussed in Chapter 2. This chapter investigates the different properties of these systems in contrast with similar systems in two dimensions. We start by looking at the packing of the systems created, before investigating the sizes of the voids and number of contacts each particle has.

### 5.1 Visual Inspection

Figure 5.1 shows some examples of 3D packed beds, with different radii of particles present, that were created using the model presented in Section 2.3.


Figure 5.1: Packed beds of 3D particles across three systems with different radii particles present. a (top left): $r_{p}=10 \mathrm{~b}$ (top right): $r_{p}=10,20$. c (bottom middle): $r_{p}=10,50$. Note that the size of the bounding box increases with the largest particle dimension.

The 3D systems have much lower packing fractions when compared to the 2D systems, which is expected when comparing the maximum possible packing fractions, $\sim 0.9$ in 2D and $\sim 0.7$ in 3D, as there is an extra dimension leading to more variability in particle placements. This makes the chance of an ordered system where each sphere has twelve contacts extremely unlikely, therefore an "ordered" system for our cases would be one where each sphere has six contacts, with both three above and three below. As even the systems with spheres of the same size present are disordered, the addition of smaller particles does not affect the order of the system significantly due to arrangement of the particles in the first layer. However, we can see, in contrast to the 2D systems, that particles which are sufficiently small are now able to fall through the gaps between the larger particles. In Figure 5.1b, the small particles are not small enough to fit between most of the gaps between the larger particles and therefore there are still small particles throughout the height of the system. However, in Figure 5.1c, the small particles are now small enough compared to the large particles to be able to fall through the majority of the gaps between them, resulting in a collection of small particles at the base of the bed. This is a significant observation since it is consistent with the widely held belief that the presence of fine particles which may be transported through a bed of particles are responsible for significant increases in the filter cake resistance when filtering particle suspensions with a wide particle size distribution. ${ }^{1}$

### 5.2 Packing Fractions

The packing fractions determined for the 3D systems follow a different pattern to that of the 2D systems. As shown in Table 5.1, the systems become more packed with the introduction of a larger sized particle, with the system that contained $r_{p}=10,20$ particles having a larger packing fraction than the other systems. As with the 2D systems, the smaller particles are able to fill in the voids between the larger particles when they are present, however the 1:1 addition ratio of the particles sizes means that whilst the $r_{p}=10,50$ systems
could have a higher packing fraction if the voids were filled with smaller particles, there are not enough small particles placed within the systems to fill the voids, thus leaving the $r_{p}=10,20$ systems with a higher packing fraction.

Table 5.1: The Packing Fractions in 500 generated 3D Packed Bed Systems with different particle radii present.

|  | Packing Fraction |  |  |
| :---: | :---: | :---: | :---: |
| Particle Radii | Minimum | Average | Maximum |
| 10 | 0.434 | $0.460 \pm 0.007$ | 0.475 |
| 10,20 | 0.480 | $0.497 \pm 0.006$ | 0.513 |
| 10,50 | 0.452 | $0.468 \pm 0.006$ | 0.486 |

These values are lower than the highest packing fractions that have been calculated in systems of same sized spheres. There are two lattices that can occur to achieve the highest packing fraction ${ }^{2}$, which is $\pi / 3 \sqrt{2} \approx 0.74048^{3}$. These two lattices, as seen earlier in Figure 2.3, are face-centred cubic (FCC) and hexagonal close-packed (HCP). It has been found that the highest packing fraction in 3D binary sphere packings, such as our $r_{p}=10,50$ system, in which the smaller particles are able to pass between the voids formed by the larger particles is $0.8617 .{ }^{4}$

Other examples of packing types and their maximum densities are: random close packing, $0.6400^{5}$; the tetrahedral lattice, $\pi \sqrt{3} / 16 \approx 0.3041^{6}$; and the loosest possible density that has been found is $0.0555^{7}$. Our values fit between these as expected, as they are lower than the more packed systems due to our inherent randomness but more packed than the more irregular systems due to the presence of the simulated gravity forcing particles downwards to pack more tightly. Another reason behind our systems having a lower packing fraction than the higher density packing methods is due to the small box size being used for our systems, resulting in significant edge effects reducing the packing fraction.

### 5.3 Number of Contacts

In the FCC and HCP lattices discussed above, the expected number of contacts for each sphere is twelve, with three below, six on the same plane, and three above. However even the slightest irregularity causes the spheres on the same plane to be further away and no longer in contact with each other. Therefore, the number of contacts that each sphere would have in a regularly structured system would be six, accounting for the three touching spheres above and below.


Figure 5.2: The frequency of the number of contacts per particle has across the investigated 3D systems.

As seen in Figure 5.2, the systems containing only $r_{p}=10$ do show the most frequent contact number is six, however not by a large margin. Due to the large amount of disorder in these systems, the number of contacts ranges all the way from one to ten contacts in the single particle size bed. Whilst there are some particles with contact numbers close to the FCC and HCP lattice value of 12 , they are extremely outnumbered by the number of particles with 6 contacts or less. This shows how the packing of these systems is far away from the ordered packing of the HCP and FCC lattices, due to the randomness of the placement of the particles.

The beds with different sized particles present show a maximum at three contacts, also with high occurrences of four to seven contacts. These are still around the expected value of six, with the lower ones being particles in contact with the edge of the box, due to the finite size effect. ${ }^{8}$ The lower end of the contact values is also due to particles that are in contact with the edges of the box, as contacts between particle and boundary are not counted, as well as smaller particles resting inside voids capped by larger particles. As part of future work, discussed further in Chapter 8, future investigations would go into the finite size effect so that these data points will not impact the averages as much.

As shown in Figure 5.3a, there is a large variance between the number of contacts each of the smaller particles across the three investigated systems has. The increased number of particles with one contact in the $r_{p}=10,20$ and $r_{p}=10,50$ systems, is due to the higher box area, and therefore more small particles falling to the bottom of the box, and only having a single contact with a particle resting above them. The large number of small particles with three contacts is due to a small particle resting on three larger particles with the void then capped above by another large particle, not allowing the smaller particle now trapped inside the void to gain any more contacts.


Figure 5.3: The frequency of the number of contacts per particle, differentiated by the radius of the particle, across the investigated 3D systems. a (top): Contact number frequency of $r_{p}=10$ in all three invesitated systems. b (bottom): Contact number frequency of $r_{p}=$ 20, 50 in the investigated binary systems.

Figure 5.3b shows the difference between the number of contacts of the larger particles in the $r_{p}=10,20$ and $r_{p}=10,50$ systems. The $r_{p}=10,50$ data in Figure 5.3b is similar to the $r_{p}=10$ data in Figure 5.3a, as similar to the 2D systems they pack similarly, however the $r_{p}=10,50$ graph has a slower decline at the higher end of the number of contacts due to the smaller particles now present that will also be resting upon them.

These graphs give more information about my systems, and is another metric by which the simulated systems can be compared when subjected to shear forces, which would hopefully be performed as part of future research using this model.

### 5.4 3D Percolation Structures

We also investigated the presence of percolation structures in the 3D systems. With the addition of the third dimension, chains spanning the box in either the $x$ - or $z$-direction are sought using the same method as discussed in Section 2.2.3 for the 2D structures.

Table 5.2: Data on Percolation Structures in 100 generated 3D structures containing $r_{p}=10,20$ in various proportions

| Particle <br> Proportion <br> (Large:Small) | Systems with <br> Percolation <br> Chains Present <br> $(\%)$ | Minimum <br> Number of <br> Percolation <br> Chains <br> Present | Average <br> Number of <br> Percolation <br> Chains <br> Present | Maximum <br> Number of <br> Percolation <br> Chains <br> Present |
| :---: | :---: | :---: | :---: | :---: |
| $1: 1$ | 100 | 7 | $15.46 \pm 4.94$ | 26 |
| $1: 2$ | 100 | 2 | $11.04 \pm 5.38$ | 27 |
| $1: 3$ | 98 | 0 | $6.91 \pm 5.17$ | 26 |
| $1: 4$ | 84 | 0 | $4.36 \pm 3.26$ | 14 |
| $1: 5$ | 59 | 0 | $2.01 \pm 3.04$ | 19 |
| $1: 6$ | 36 | 0 | $0.89 \pm 1.82$ | 9 |

The 3D data shown in Table 5.2 show the same pattern as the 2D data in Table 4.3, with a higher frequency of percolation structures present when the number of large and small particle present are similar. However, there are still many more percolation structures present at higher ratios in the 3D systems compared to the 2D systems, with only $59 \%$ of systems containing a percolation structure in the 2D system with a ratio of 1:2 large:small particles, but the 3D system with the same ratio having $100 \%$ percolation chain presence. This is because in 3D the particles tend to have more contacts,
giving more options for the larger particles to connect to each other across the system. As shown, even at a ratio of 1:6 the percolation threshold has not been found and more percolation chains are being found than in the 2D system with a third of the ratio. Another factor is that whilst the radius ratio is the same in both the 2D and 3D systems, the area/volume ratio is not, as in the 2D systems the 10:20 area ratio is also 1:4, however in 3D the volume ratio between radius 10:20 particles is 1:8, giving them much more surface area to make contacts with other particles in the system, and thus form percolation chains.

Table 5.3: The minimum, average and maximum lengths of percolation chains in 100 generated 3D structures containing $r_{p}=10,20$ in various proportions

| Particle <br> Proportion <br> (Large:Small) | Minimum Length <br> of Percolation <br> Chain Present | Average Length <br> of Percolation <br> Chain Present | Maximum <br> Length of <br> Percolation <br> Chain Present |
| :---: | :---: | :---: | :---: |
| $1: 1$ | 7 | $7.56 \pm 0.94$ | 18 |
| $1: 2$ | 7 | $7.79 \pm 1.02$ | 16 |
| $1: 3$ | 7 | $7.94 \pm 1.31$ | 15 |
| $1: 4$ | 7 | $7.80 \pm 1.11$ | 17 |
| $1: 5$ | 7 | $8.14 \pm 1.18$ | 15 |
| $1: 6$ | 7 | $8.02 \pm 0.98$ | 12 |

Again, the minimum length of chain is close to the minimum possible but slightly above, with the 3D box dimensions being 6 particle diameters. The average chain lengths across the different ratios are consistent, likely due to the smaller size of the box resulting in much longer chains being unable to form. The maximum chain lengths are also relatively consistent compared to the 2D data, still with a small decline, again likely due to the comparatively smaller box size. Producing more systems in larger boxes for all these tests on a larger scale is the next step for this area of the project, and is discussed more in the Future Work section, as further investigation can then be
undertaken into how these percolation structures may reflect fracture patterns within the systems.

### 5.5 Summary and Conclusions

When investigating the packing fractions of the 3D systems created by my model, I found that whilst they followed the same pattern as the 2D systems, they overall had much lower packing fractions, with a difference of about 0.3. My systems packing fraction values did rest between the precalculated minimum and maximum packing fraction values for single sized and binary particle systems, showing that initially these values are realistic.

The 3D contact graphs also show similar patterns to the 2D contact graphs, however the 3D graphs are much more affected by the finite size affect, as well as the ability of the small particles to fall through voids to the bottom of the box. This results in a large number of small particles with very few contacts, especially in the binary $r_{p}=10,50$ systems. The single sized $r_{p}=10$ system would have each particle having 12 contacts if it was perfectly packing in a FCC or HCP lattice, however as previously stated we expect our particles to have 6 contacts. There is a peak at this value, however the lower contact number values occur almost as frequently, showing that the structure is quite far removed from the ordered lattices, especially with very few particles having above 7 contacts. The larger particles that have more contacts will also be due to the small particles resting around them, rather than the packing of the systems shifting towards one of the ordered lattices.

When investigating the presence of percolation chains within the 3D structures, it was found that they are much more prevalent in 3D systems than in 3D, likely due to the increase in contact area available, thus more contacts being formed, in 3D systems. When comparing across the 3D systems, the expected pattern of finding less percolation chains occurring the more smaller particles are in the system is found, with the minimum, average and maximum
number of chains per system decreasing as well as the average length of a chain increasing as it becomes harder to make a direct chain across the system.

The 3D algorithm that has been produced is able to simulate more realistic systems that the 2D algorithm, purely given the extra dimension that exists in laboratory experiments. The 3D algorithm has also been shown to replicate phenomena experienced in laboratory experiments, such as smaller particles filtering to the bottom of a system, through the gaps made by larger particles. Given the various parameters investigated here, this model can hopefully be used in future research to see the effect on these systems when the parameters are further varied.

### 5.6 References

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## 6 Non-Spherical Particle Chains

As discussed in Section 2.3.6, when we are modelling chain particles, we are doing so by attaching multiple circular particles together to form the chain. This decreases the complexity of the algorithm as it can be created by building upon the previous 2D algorithm, however this approach does mean the chain particles are not accurate to how a rectangular or needle-like structures would pack, due to the ridges present in our chain structures. The following algorithm was created as an extension for the 2D algorithm due to its simplicity. A 3D version of the algorithm has also been started but is not complete due to time constraints.

### 6.1 Initial Code Edits

A new section was added into the algorithm that took place immediately after a particle was added into the system. Instead of looping back to the start to place another particle, the model created a localised contour plot based around the most recent particle, which followed its edge. This places the new particle with its edge on the centre of the previous particle, overlapping with it to form a chain, but still being unable to overlap with other particles.


Figure 6.1: Flowchart showing the stages of adding particles to form a chain particle from the initial particle

Once this contour plot is formed, the model then randomly picks a direction for the next particle in the chain to fall to from the centre of the particle, as it is assumed the chain is falling vertically and then tilting to one side upon impact. It then moves along the contour plot as before until it impacts with another particle. It then follows the algorithms previous path of particle impact, where the new particle is being balanced on one particle and joined with another, using stochastic optimisation to determine the real coordinates for its final position.

For a system of chains containing only two particles, the model would then loop back to the start as before and repeat these steps. However, for chains containing three or more particles, a new step is added.

As the chains direction has been determined by the first two particles, the contour plot is no longer required to place further particles in the chain. Instead, the radius of the particles and the direction that they are being placed in can be used to simply place the rest of the particles in the chain along its line.

However, as each particle in the chain is placed, it checks that it is not overlapping with any other particles or outside the box. In either of these cases, the offending particle is moved to be balanced on what it is impacting, as shown in Figure 6.2, whilst still being the correct distance away from the original particle in the chain. The particles in between these two on the chain are then readjusted to ensure they are all connected and in a straight line. This process is looped until the chain is the requested length of particles, and then the model loops back to the very start to place a new chain.


Figure 6.2: Steps taken to adjust a growing chain to balance on an overlapping chain in the event the growth of the new chain causes an overlap with an old chain. A) New chain (currently 4 particles) overlapping with a previously placed chain b) New chain readjusted to be balancing instead of overlapping c) New chain (now 5 particles) overlapping with a previously placed chain d) New chain readjusted to be balancing instead of overlapping.

### 6.2 Chain Particle Complexities

As the length of the chain increased, the complexity of the systems being formed also increased, with new possible balancing possibilities between particles becoming possible.

Due to the first particle being placed on its own, there was now the possibility of a particle being placed in a situation where a chain could not grow from it.

To combat this, in this instance, the particle would slide back along the path it took to get to its final position, until a chain was able to be formed. This then ran in to the issue that previously the first particle being placed needed to be balancing on two other particles, however in these situations, it is possible, and indeed correct, for the initial particle to be only in contact with one particle, and then be balanced by another contact further along the chain. Therefore, once the particle has determined it needed to slide upwards from a trapped position, some additional leeway was added to allow the first particle to have only one contact, provided the following conditions were true:
a) The base particle of chain had a contact on the opposite side to the direction the particle was leaning, i.e. if the particle is leaning right, the contact is on the left.
b) The contact that is furthest from the initial particle is also beyond the centre point of the chain.
c) There is at least one contact point, not on the initial particle, that is on the underside of the particle.

With these additional conditions, stable chain structures were able to be produced.


Figure 6.3: Chains labelled with the conditions $a, b$ and $c$ listed above that must be fulfilled to allow the placement of a chain with only have one contact at its base

### 6.3 Results

All of the 500 runs completed for each of the systems, listed below, using the 2D chain algorithm were performed on ARCHIE-WeSt. The ratio of addition for each different chain or particle type in these systems is $1: 1 . n_{p}$ refers to the number of particles that made up an individual chain.

Each of these systems had its packing fraction calculated and the angle of each chain was determined.

Systems investigated:

- A) $r_{p}=10, n_{p}=2$
- B) $r_{p}=10, n_{p}=3$
- C) $r_{p}=10, n_{p}=4$
- D) $r_{p}=10, n_{p}=5$
- E) $r_{p}=10, n_{p}=5$ and $r_{p}=10, n_{p}=1$
- F) $r_{p}=10, n_{p}=5$ and $r_{p}=5, n_{p}=1$
- G) $r_{p}=10, n_{p}=5$ and $r_{p}=5, n_{p}=5$


### 6.3.1 Visual Inspection

Examples of each of the different systems produced, $A$ to $G$, are shown in Figures 6.4, 6.5 and 6.6.

Figure 6.4 shows systems $A$ to $D$, where the $n_{p}$ increases from system to system but remains consistent within each system. In each of these systems, once a chain has fallen, it often results in the chains placed above it adopting the same angle, creating sections within the system with chains stacked together, an example of which in the System D example at $x=300$ and $y=$ $\sim 150$ to $y=\sim 350$. As the chain length gets longer, these groups of chains at the same angle take up much more of the systems. These clusters are broken up when a chain is placed to the side of it but leans over enough to cause the next chain that would want to join the cluster to lean differently.

Some perfectly vertical chains are present leaning up against the wall of the box in the base layer of particles, which is a very unstable position. This is because when I added a section of code to the algorithm to favour falling away from the edge of the box if a chain found itself directly up against it, I forgot to also add that section of code to the part of the algorithm that placed the base layer of chain particles. Therefore these vertical chains will only appear in the bottom left and right corner of the box, using this algorithm, but this issue would be easily solved in a future version.





Figure 6.5: Examples of systems E and F

Figure 6.5 shows systems E and F, where single particles have been added into a system containing 5 length chains of $r_{p}=10$. The single particles make forming clusters of aligned chains much more difficult, especially when they are the same size as the chain, as their placement on top of a cluster will immediately stop its continuation. This shows that whilst processing these chain-like particles, the introduction of small particles can dissuade clusters of chains from joining together, and therefore reduce the size of the same angled groups that form.


Figure 6.6: Example of system G

Figure 6.6 shows an example of system $G$, which has some similarities to system E as it contains smaller particles, however being chains instead of single particles causes them to have much less ability to fit into voids between
the larger chains, instead each size of chain causing the other to be unable to join clusters as they block regular placement of each other.

### 6.3.2 Packing Fraction

Table 6.2: The Packing Fractions in the investigated 2D chain systems.

| System | Packing <br> Fraction |
| :---: | :---: |
| A | $0.790 \pm 0.008$ |
| B | $0.772 \pm 0.019$ |
| C | $0.795 \pm 0.011$ |
| D | $0.781 \pm 0.018$ |
| E | $0.795 \pm 0.006$ |
| F | $0.788 \pm 0.013$ |
| G | $0.800 \pm 0.006$ |

The packing fractions across each of the investigated systems remain relatively consistent compared to the original 2D algorithm with no real pattern found throughout systems $A$ to $G$, although there is a small increase in packing fraction for the systems that introduce another size of chain or single particles. As observed before, these single particles are able to pack in between the chain particles, filling in voids.

The differences in packing between systems $A$ to $D$ are likely due to the randomness inherent within these systems, as there is an additional factor of randomness added to these systems in the form of the rotation of the chains, which was not present in systems only containing single particles. This is shown by the increased standard deviations in these systems compared to the regular 2D systems discussed in Chapter 4. Research has gone into the packing of 3D chain shapes, such as cylinders and spherocylinders, which have a maximum packing fraction at a specific ratio of height to diameter. ${ }^{1}$ Spherocylinders, which are closer to the particles which I am simulating due to the curved ends, have been found to have a peak packing fraction of 0.6896 at a ratio of 0.35 , with packing fractions then having a small decrease on
increasing ratio. This could explain why there is no discernible pattern across systems A to D, as the ratios explored here are 1.5 to 3 , which is far above the ratios explored within this research. In the research into cylindrical packing, a peak packing fraction of 0.7185 was found at a ratio of 0.9 , which is still much below the ratios we investigated. Future research could look into simulating ratios closer to these to determine if a similar pattern was found, thought our systems are in 2D and have the slight difference in shape with rounded edge along the sides of the particles.

Another study looked at the simulation of cylinders compared to chain structures made up of "glued spheres" to mimic a cylindrical shape, similar to the particles investigated here. ${ }^{2}$ It was found that the systems with cylindrical particles had higher packing fractions that the systems with glued sphere particles, found to be due to the higher volume each individual cylindrical particle has compared to the glued sphere particles. As the number of spheres used to make a particle was increased but the overall dimensions of the shape kept the same, a trend was found where the packing fraction increased, becoming closer to the packing fraction found in the true cylindrical particle systems. However, even with more spheres making up a particle, the packing fractions do not reach the same packing efficiency as the true cylindrical particles.

The introduction of singular particles in systems E and F, increase the packing fraction to be on the higher side of the range of packing fractions previously seen in systems A to D. System E has a packing fraction on par with the highest of systems A to D, likely due to the addition ratio of the particles still being 1:1, so whilst the particles in system E would affect the structure more, an equal amount of particles to the small particles in system F, cover more space. If the small particles in system $F$ were added in a greater amount, the packing fraction would likely be higher as they would be able to fill in many more of the voids, that shown in Figure 6.5 are still quite empty.

The addition of smaller chains in system $G$ does increase the packing fraction to be above the range shown in systems A to D, again due to the small chains ability to fit in gaps that the larger chains cannot, however as expected they cannot fill in voids as well as single particles of the same size. Research has also gone into the packing of binary mixtures of cylindrical particles ${ }^{3}$, mixing particles with a height to diameter ratio (AR) of 1 with particles with an AR of 2 and 3 separately. It was found that as a higher percentage of AR 1 particles were added to a system, the packing fraction increased for both the systems containing AR 2 and AR 3. The AR 1 and AR 2 mixture showed a smaller increase in packing fraction when increasing the percentage of AR 1 particles present but had higher packing fractions than the AR 1 and AR 3 systems overall. These patterns match other research carried out both in physical ${ }^{4}$ and simulated ${ }^{5}$ experiments. As my binary mixture chain system contained chains that did not differ by AR, being 3, but instead by the scale of their height and diameters this data is useful to investigate but can not be directly compared to my systems. Future runs on my model can be done to investigate particles with different $A R$ to see if similar patterns emerge.

### 6.3.3 Chain Angles

A new property that can be investigated within the chain systems is the angle at which each chain is lying, with $0^{\circ}$ being directly vertical, then $-90^{\circ}$ being lying flat to the left and $+90^{\circ}$ being lying flat to the right.

Figure 6.7 shows histograms of the chain angles present in systems A to D. Each graph shows a clear curve with two peaks, starting at the $50^{\circ}$ to $55^{\circ}$ mark in System $A$ and moving closer to $0^{\circ}$ as the chains get longer, ending up at the $30^{\circ}$ to $35^{\circ}$ mark in System D. This shows the chains are becoming more vertical the longer they become, which is likely due to the increased complexity of the systems leading to less orderly packed systems, as a more ordered system of chains would be made up of chains resting horizontal on top of each other.

The peaks at $90^{\circ}$ exist as $\tan \left(90^{\circ}\right)$ is an undefined value, therefore when the calculations gave an error it was recorrected to be a $90^{\circ}$ value, thus no corresponding peak appears at the $-90^{\circ}$ mark.


System B



Figure 6.7: Histograms of the angles of chain placement across systems $A$ to D

There is also a peak in the $\left[-10^{\circ},-15^{\circ}\right]$ bin in each of the systems. This is due to the large number base layer particles that are directly next to another particle and leaning against it, having an angle of $-14.48^{\circ}$, as shown in Figure 6.8. The abundance of these chains comes from the setup of the base layer, as after the model has run for a large number of times to try and fill the base layer, to confirm it is filled, the model runs across the base layer from left to right looking
for empty space, as discussed in section 3.1.2. This results in initial particles being placed directly adjacent to horizontal chains, and when they tilt to the left, have an angle of $-14.48^{\circ}$. This could be fixed by increasing the counter used when placing random particles, or by altering the algorithm to be able particles landing on the edge of the box, instead of requiring an initial layer of particles.


Figure 6.8: Base layer particles with angle $-14^{\circ}$ particles highlighted with a red line marker.



Figure 6.9: Histograms of the angles of chain placement across systems E and $F$

The introduction of single particles in the chain systems, E and F, does not appear to have much of an effect on the angle histograms with the peaks still being at $\pm 30^{\circ}$ to $35^{\circ}$. System F does not have a peak in the $\left[-10^{\circ},-15^{\circ}\right]$ bin, as the small single particles are being used to fill in the gaps in the base layer, meaning there is not an abundance of chains in the base layer resting at the specific $-14.48^{\circ}$ angle.


Figure 6.10: Histogram of angles of chain placement in system G overall and separated by chain size

The system $G$ histograms, Figure 6.10, shows the same pattern in its histogram as is within systems $A$ to $D$, though with the peaks being at $\pm 25^{\circ}$ to $30^{\circ}$, showing the chains are more vertical than in the previous systems. This is more vertical than system D just containing length 5 chains, showing that the introduction of the smaller chains decreases the order of the system, resulting in the chains being pushed further from a regular horizontal packing.

When looking at the angles of the chains in system G separated by size, the previously observed pattern remains, with the smaller chains in these systems creating the peak at $-10^{\circ}$ to $-15^{\circ}$, as the smaller chains are used to fill in gaps in the base layer if they are not filled randomly. Research on the angle of cylinders resting in binary mixtures ${ }^{3}$ has been done, and found the opposite
trend that was reported here, with the cylinders preferring to lay horizontal over vertical. This is likely due to a few factors, including my systems being 2D and the literature systems being 3D, the system size, with my systems still affected by the finite size effect, and remaining issues within my code, such as what leads to the peak at $-14^{\circ}$. Were the code to be updated and system size increased, my model would hopefully also follow the reported pattern, with chains resting more horizontal than vertical.

### 6.4 Summary and Conclusions

The expansion of the algorithm allows us to investigate systems containing particles that are closer to real needle-like particles, therefore it can be used to make more accurate simulations compared to perfectly circular particles. It was found that when small singular particles are added into a system of chain particles, they reduce the size of clusters of those chain particles, which could be used to lessen the effect of agglomeration in similar systems.

The packing fractions in the investigated systems remained consistent, however with an increase when singular particles are added into the systems, as noted in previous chapters, they are able to fit into the voids created by the chains.

When investigating the angles of the chains within the investigated systems, it was found that increasing the length of the chain caused the particles to become more vertical, likely due to the increased complexity caused by larger particle structures, moving the system away from a more ordered system with chains lying horizontal on top of each other. The preference to vertical over horizontal in my systems is potentially also due to the curved edges of individual particles in the chains still being present, allowing new chains to rest partway along them, instead of sliding along the chains to the edges and so becoming more horizontal.

Due to time constraints, these were the only systems that were able to be investigated, however there are many more experiments that could have been done given more time. Such as increasing the chain length further, investigating a wider range of particle radii within the same system, as well as chains that are made up of different sized particles instead of all the same. This algorithm does give us a good starting point from which to further investigate these systems, so going forward these additional systems would also be looked into.

### 6.5 References

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## 7 AstraZeneca Placement

During the fourth year of my PhD project, I spent 12 weeks on a placement at the AstraZeneca ${ }^{1}$ Macclesfield campus, where I compared the commercial Ansys Rocky DEM ${ }^{2}$ software with my own model, as well as then using the commercial DEM software in a Design of Experiments (DoE) ${ }^{3}$ approach to determine parameters for an AZ Compound.

AstraZeneca are currently in the early stages of investigating various DEM modelling software packages, looking at which one best suits their needs at various stages of chemical and pharmaceutical development and processing. The main aim of my placement was to investigate Rocky DEM and its suitability for use modelling AstraZeneca particles and processes. My personal aims for this placement were to gain some professional experience working in an industry setting, as well as being able to get hands on experience with industry standard modelling software and be able to compare it to my own model.

Within the pharmaceutical industry Rocky DEM modelling software is used to investigate behaviours of particles, such as particle breakage, with varying particle sizes, and shapes in systems of different geometries. ${ }^{4}$

The parameters investigated were: the Basic Flowability Energy (BFE, mJ); the Rolling Resistance (no units); the Static and Dynamic Friction Coefficients (no units); the Young's Modulus (Pa); and the Coefficient of Restitution (no units). The BFE of a powder is a measure of its flow properties when it is in a loosely packed state, in our case defined by the energy required for the mixing blade to move downwards through the powder. ${ }^{5}$ This can be used to quantify how changing various parameters of the particle affect how it flows. The Rolling Resistance quantifies the resistance that occurs when a particle rolls, either over another particle or a surface of the bounding box. The Static Friction Coefficient measures the friction that exists between two surfaces whilst they are at rest, whilst the Dynamic Friction Coefficient denotes how much friction
will occur when two surfaces are sliding over one another. The Youngs' Modulus is a measure of the elasticity of the particles, denoting how much a particle shape will be affected by the forces being placed upon it. The Coefficient of Restitution is the ratio between the final and initial relative speeds between two particles after they have collided.

### 7.1 Familiarisation with Rocky DEM

As discussed in Section 2.2, there are multiple different types of models used within computational sciences. For these experiments I am using a DEM package called Ansys Rocky DEM. For new users of Ansys Rocky DEM, there are a series of tutorials that guide the user through various examples to familiarize them with the software and how to use it. Relevant topics include: setting up equipment geometries; establishing particle interaction characteristics; performing simulations and data visualization. Some of the advanced topics address capabilities which are relevant to this research including: particle addition; motion frames which allow geometries placed within the system to move; wear arising from multiple particle impacts; and particle breakage from an impact.

The Rocky DEM training material also included a workshop on creating custom particle shapes including fibres and multiple particle sizes. Although during my short industrial placement, I did not get the time to run simulations using non-spherical shapes, it was useful to see how Rocky DEM handled them, I was however able to use different sized particles in my Rocky simulations.

Another useful element in the training material was a simulation of a conical double screw vacuum dryer which involved multiple stacking motions, as geometries were rotating on multiple axes, both vertically and rotationally, and enabling thermal modelling within the system to see how the heat propagated through the system.

The Rocky training materials gave me a working understanding of the software such that I could use it for simulations.

### 7.2 Comparing Rocky DEM with my model

My model uses a simpler algorithm, described in Chapter 3, compared to Rocky DEM, with my model only simulating gravity when placing particles one at a time. Rocky however involves many particles moving within the system at the same time, and for each particle in each timestep has to identify that particle's neighbours, calculate the forces that they exert on each other, whether through contacts, electrostatic forces, or other interactions, as well as other forces present in the system, such as gravity, as shown in Equation 7.1.

$$
\begin{equation*}
\sum F_{n e t}=\sum F_{b o d y}+\sum F_{\text {surface }}=m \frac{d v}{d t} \tag{7.1}
\end{equation*}
$$

where $F$ is Force, $m$ is mass and $t$ is time. ${ }^{6}$

Once all of these forces have been determined, they can be used to calculate how they affect an individual particle's velocity so the model can calculate the position and rotation of that particle in the next timestep, based on its old position and current new velocity, as shown in Equations 7.2 and 7.3.

$$
\begin{align*}
& v_{\text {new }}=v_{\text {old }}+\int_{t}^{t+\Delta t} \frac{\sum F_{\text {net }}}{m} d t  \tag{7.2}\\
& x_{\text {new }}=x_{\text {old }}+\int_{t}^{t+\Delta t} v_{\text {new }} d t \tag{7.3}
\end{align*}
$$

where $F$ is Force, $m$ is mass, $t$ is time, $v$ is velocity and $x$ is position. ${ }^{6}$

These calculations are completed for every particle in the system, the timestep iterated to the next one, and then the whole process repeated until the simulation end time is reached or all particles have left the range of the system. Note that in principle, the simulations conserve energy however
frictional forces damp motions so that thermal energy of the particles must be considered. Each Ansys Rocky DEM run used the Hysteretic Linear Spring Model, first proposed by Walton and Braun ${ }^{7}$, which is an elastic-plastic (repulsive and dissipative) normal contact model. ${ }^{6}$ The means that, unlike my model, the particles are "soft" and can be compressed when coming into contact with another particle. The model is implemented in Ansys Rocky DEM using the following equations 7.4 and 7.5.

$$
F_{n}^{t}=\left\{\begin{array}{l}
\min \left(K_{n l} s_{n}^{t}, F_{n}^{t-\Delta t}+K_{n u} \Delta s_{n}\right) \text { if } \Delta \mathrm{s}_{\mathrm{n}} \geq 0  \tag{7.4}\\
\max \left(F_{n}^{t-\Delta t}+K_{n u} \Delta s_{n}, \lambda K_{n l} s_{n}^{t}\right) \text { if } \Delta \mathrm{s}_{\mathrm{n}}<0
\end{array}\right.
$$

$\Delta s_{n}=s_{n}^{t}-s_{n}^{t-\Delta t}$
where $F_{n}^{t}$ and $F_{n}^{t-\Delta t}$ are the normal elastic-plastic contact forces at the current time $t$ and at the previous time $t-\Delta t$, respectively, where $\Delta t$ is the timestep. $\Delta s_{n}$ is the change in the contact normal overlap during the current time, otherwise described as the change in the size of the overlap between two particles, illustrated in Figure 7.1. It is assumed to be positive as particles approach each other and negative when they separate. $s_{n}^{t}$ and $s_{n}^{t-\Delta t}$ are the normal overlap values at the current and at the previous time, respectively. $K_{n l}$ and $K_{n u}$ are the values of loading and unloading contact stiffnesses, respectively. $\lambda$ is a dimensionless small constant. Its value in Ansys Rocky DEM is 0.001 . The part of the expression in which this constant is active ensures that, during the unloading, the normal force will return to zero when the overlap decreases to zero. ${ }^{6}$


Figure 7.1: Two particles overlapping during a simulation with the contact normal overlap ( $\mathrm{S}_{\mathrm{n}}$ ) labelled

As Rocky incorporates many more parameters than my model, it can be used to simulate much more complicated systems, but at the cost of having large parameters spaces that can be complicated to explore. It also has the cost of taking much more computational power and greater time to complete each run. Each of the Rocky simulations was run on the AstraZeneca supercomputer and took around one to three hours to complete each, with my model being run on a on the ARCHIE-West supercomputer and each run taking around a few minutes each.

### 7.2.1 Method of Particle Addition Comparison

Initial comparisons were completed between Rocky DEM and the model I created, using the same scale between particle and box size, with one box side being six particle diameters. Runs were completed in Rocky DEM using both the volume and continuous fill methods to also be able to analyse the difference between them.

The Volume fill method involves choosing a point within the system as an origin point for the particles, which for my systems was the centre of the box.

A particle is placed at this origin point, and then all subsequent particles are placed attached to this origin particle to form a ball of particles. No forces are accounted for during these additions, instead, once the model has added the requested number of particles, the forces are applied to the system, and the particles settle. Compared to this, the continuous fill method acts much more similarly to my model, with each particle entering the system from a random point in a designated inlet, which for my systems is the top of the box, and forces are immediately applied to them so they can settle. In Rocky DEM, multiple particles are added at the same time however, resulting in the possibilities of impacts and interactions as the particles are falling, instead of just once they impact the pre-existing bed.

The volume fill option was difficult to set up as it either overflowed over the top of the box, or under-filled depending on which volume was set to be filled. This problem was overcome by placing a solid lid over the top of the box, and the volume fill set to overflow. Any particles outside of the lid were then not counted in the calculations, and any particles that were initially overlapping with the box lid were removed from the system at the simulation start, as shown in Figure 7.2

The continuous option was much easier to set up as the inlet for the particles to be added to the system from could be placed at the top of the box, acting similarly to how my model functions.

The packing fractions of the systems were examined as a simple point of comparison between the different types of particle addition in Rocky DEM, and as a comparison to my model.

As shown in Table 7.1, across each of the systems investigated, the continuous addition method had a higher packing fraction than the volume fill method. This will be due to both the particles' ability to pack whilst they are being added in the continuous method, as in the volume fill method, all the
particles are added in one go and then allowed to settle, which can cause gaps to occur which would allow additional particles to fit, if all particles for that system had not already been added.

Table 7.1: Packing fractions of systems created with different particle addition methods and radii

| Radii <br> Present | Particle Addition Method | Rocky Packing <br> Fraction | My Packing <br> Fractions |
| :---: | :---: | :---: | :---: |
| 10 | Volume Fill | $0.439 \pm 0$ | $0.460 \pm 0.007$ |
|  | Continuous Fill | $0.461 \pm 0.005$ |  |
| 10,20 | Volume Fill | $0.460 \pm 0.004$ | $0.497 \pm 0.006$ |
|  | Continuous Fill | $0.475 \pm 0.007$ |  |
| $0.468 \pm 0.006$ |  |  |  |
|  | Volume Fill | $0.466 \pm 0.017$ |  |



Figure 7.2: Continuous addition method (left) and Volume Fill addition method (right)

The packing fractions across the volume fill methods are also very consistent, with there being no differentiation between the repeats run in the single sized particle system. This is due to the small size of the box limiting the number of particles that can be placed around the initial centre particle, causing systems which form to be largely the same, and in the case of the only $r_{p}=10$ system, identical.

Figure 7.2 shows the difference between the different types of particle addition, with continuous addition filling closer to the top of the box, having a higher packing fraction, and also not leaving additional particles outside it.

### 7.2.2 Model Packing Fraction Comparisons

As the continuous fill method is closer to how my model acts, and gives a better representation of a system being filled by particles from above than the volume fill method, it was the method used going forwards when comparing the two models. Some additional runs were conducted looking at how the different ways the particles were added in the continuous addition methods can affect the speed of the simulation runs, in order to reduce time spent waiting for them to be completed. Initially, particles were added in a consistent speed from the start to end of the simulation. However, nearer the end of the simulation, this resulted in the model attempting to add particles to the system when there was no room, wasting processing time and causing the simulation to take longer. Therefore, it was investigated what happened if particles were not added nearer the end of the simulation when the box got too full. This resulted in boxes that were not completely full as particles near the top were still able to pack down once addition had been halted. The solution used to correct this issue was to stagger the particle injections, to give each one some time to settle so that they are not immediately in the way of the next group of particles to be added.

Table 7.2: Comparison of packing fractions calculated for systems created by Rocky DEM and our model

| Radii Ratio <br> Present | Packing Fraction |  |
| :---: | :---: | :---: |
|  | Rocky DEM | My Model |
| 1 | $0.460 \pm 0.005$ | $0.460 \pm 0.007$ |
| $1: 2$ | $0.475 \pm 0.007$ | $0.497 \pm 0.006$ |
| $1: 5$ | $0.466 \pm 0.017$ | $0.468 \pm 0.006$ |

In the Rocky DEM experiments, the ratios between the different radii, and between the radii and box size, within the investigated systems were kept consistent with the ones used within my model, and each radius having an equal number of particles added to the system. The larger radius in each case was also kept the same, so that the box size would remain consistent across each of the simulation runs.

The values obtained by the Rocky DEM simulations and my model are very similar, with the main difference coming in the $r_{p}=10,20$ systems. The $r_{p}=10$ and $r_{p}=10,50$ systems gave almost identical results, giving more confidence in the reliability of my model, as it is consistent with this industry standard software. The small differences will come from the randomness of particle placement inherent in both systems, however the consistency shows that my model is able to match up with the industry standard.

### 7.3 Edge Effects Investigation

Because the boxes sizes used in my model are rather small, Rocky DEM was used to investigate the edge effects present on the packing fraction at different sizes of box using one size of spherical particle. The packing fraction was determined as a whole, and then individually for different sections of the system, as shown in Figure 7.3. Note that some areas overlap, so some particles are counted twice and areas are larger than their colours show. The roof packing fraction is denoted by the area covered by red particles (and some yellow particles), the wall packing fraction is denoted by the area covered by yellow particles (and some pink particles), the floor packing fraction is denoted by the area covered by pink particles, and the whole packing fraction uses the area of the whole system. There is an additional section that cannot be seen inside accounting for the centre packing fraction (which would be coloured green), which starts where each of the floor, wall and roof areas end.


Figure 7.3: Rocky DEM systems created with different particle to box size ratios. (a) 1:6 (b) 1:24 (c) 1:60

The order of packing fractions from highest to lowest is expected to be: the centre, the floor, the walls and then the roof, as the centre of the box has no edge effects to be affected by. The floor and walls of the box are then the edges where the effect will be less due to not being the point of entry, resulting in the floor being the next most packed and the walls coming after that, as they are partly affected by the roof area. Finally, the roof section would be expected to have the lowest packing fraction as its largest surface area is affected by the entry point of the particles, where the edge effects of the box will be at their greatest. The overall packing fraction of the system would then be an appropriate weighted average of these sections, as there is some overlap between the areas and multiple walls areas to account for. This pattern is confirmed by the data shown in Tables 7.3 and 7.4.

Table 7.3: Comparison of packing fractions of different sections of particle systems with different particle:box size ratios

| Particle <br> Diameter <br> to Box <br> Width | All | Wall | Centre | Roof | Floor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Ratio |  |  |  |  |  |
| $1: 6$ | $0.461 \pm$ | $0.393 \pm$ | $0.611 \pm$ | $0.180 \pm$ | $0.464 \pm$ |
|  | 0.005 | 0.029 | 0.035 | 0.017 | 0.008 |
| $1: 24$ | $0.561 \pm$ | $0.548 \pm$ | $0.612 \pm$ | $0.419 \pm$ | $0.600 \pm$ |
|  | 0.002 | 0.003 | 0.002 | 0.010 | 0.002 |
| $1: 60$ | $0.588 \pm$ | $0.582 \pm$ | $0.609 \pm$ | $0.531 \pm$ | $0.604 \pm$ |
|  | 0.001 | 0.001 | 0.001 | 0.005 | 0.001 |

The systems used to test the edge effects contained same sized particles equivalent to the small particles from our model systems. As the box size increases, the majority of the packing fractions increase, with the exception of the centre section, as it is not affected by the box size. The ordering of the sections packing fractions still remains the same, though the values become closer, and the overall packing fraction of the system starts to become closer to the value of the centre of the box. The increase in wall and overall packing fraction also comes from the decreased effect of the roof, as it is the area with the lowest packing fraction due to it not getting completely filled. Therefore, as the box gets taller, more area can be filled below the roof area increasing the overall packing fraction of that section.

Using this data, a set of systems were created to investigate the effect of particle size distribution, with a Particle:Box diameter ratio of $1: 33^{1 / 3}$, using the larger particle diameter, as it is in between two higher values tested, however it would not have as long a runtime as the 1:60 ratio systems, taking roughly two hours each instead of four, as the time on my placement was a factor. Once again, the number of particles of each size is $1: 1$.


Figure 7.4: Three systems created with different particle sizes present. a) $r_{p}=10$, b) $r_{p}=10,20$, c) $r_{p}=10,50$

Table 7.4: Comparison of packing fractions of different sections of particle systems with different particle size distributions

| Radii <br> Ratio | Box Section |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | All | Wall | Centre | Roof | Floor |
| 1 | $0.576 \pm$ | $0.553 \pm$ | $0.610 \pm$ | $0.371 \pm$ | $0.594 \pm$ |
|  | 0.002 | 0.003 | 0.0004 | 0.021 | 0.001 |
| $1: 2$ | $0.592 \pm$ | $0.572 \pm$ | $0.626 \pm$ | $0.379 \pm$ | $0.612 \pm$ |
|  | 0.001 | 0.002 | 0.0004 | 0.009 | 0.002 |
| $1: 5$ | $0.576 \pm$ | $0.551 \pm$ | $0.613 \pm$ | $0.342 \pm$ | $0.603 \pm$ |
|  | 0.001 | 0.002 | 0.0003 | 0.015 | 0.001 |

When looking at the different sections of the box across the different systems, they maintain the same pattern as previously shown. This is expected as the size of the particles will not have any real interaction with the edge effects, instead only affecting the packing fraction of the system as a whole. Across the different systems, the packing fractions also showed the same pattern as above, with an increase between the $r_{p}=10$ to $r_{p}=10,20$ systems, and then a decrease to the $r_{p}=10,50$ system. However, in these cases, the $r_{p}=10$ and $r_{p}=10,50$ systems are much closer together compared to the smaller box systems, with some of the sections of the $r_{p}=10,50$ system having a smaller packing fraction than the respective area in the $r_{p}=10$ system.

### 7.4 Design of Experiments using Rocky DEM

The second part of my placement involved using Rocky DEM to determine various properties of an AstraZeneca compound, referred to here as Compound A. A Design of Experiments (DoE) approach was used to ensure that the experiments performed gave useful outputs, instead of using a trial-and-error approach. Within these simulations, we are modelling Compound $A$ as a spherical particle, as modelling the exact shape and size of it would take longer than the placement would allow. For these purposes, MODDE DoE software was used to take the inputted parameters and a starting value, shown in Table 7.5, to produce a series of experiments, shown in Table 7.6, that would give a good understanding of each parameters effect on the output value.

### 7.4.1 Parameter Setup

Five parameters were varied during our tests: which were the Rolling Resistance; Coefficient of Restitution; Static and Dynamic Friction Coefficients; and Young's Modulus, using the values shown in Table 7.5. The same values were used in each experiment for both the Static and Dynamic Friction Coefficients. In future experiments, we would want to use a wider
variety of parameters, and use different values for each of them, however the first investigations were limited to these parameters, and had two of them equal, due to time constraints.

Table 7.5: Range of parameter values used in the Design of Experiments method

| Parameter | Rolling <br> Resistance | Coefficient <br> of <br> Restitution | Static and <br> Dynamic Friction <br> Coefficients | Young's <br> Modulus <br> $(\mathrm{Pa})$ |
| :---: | :---: | :---: | :---: | :---: |
| Values | $0.125,0.15$, <br> 0.175 | $0.1,0.2,0.3$ | $0.175,0.2,0.225$ | $9 \mathrm{e}^{6}, 1 \mathrm{e}^{7}$, <br> $1.1 \mathrm{e}^{7}$ |

The simulations were done modelling a Freeman Rheometer (FT4) ${ }^{8}$, which is a small-scale powder rheometer that has been widely adopted in the pharmaceutical sector, shown in Figure 7.5, to calculate the BFE of Compound A, which can also be determined through laboratory experiments. Therefore, we can compare the model's output to the physically measured value to determine if the values for the tested parameters are possibly valid. The simulation involves filling the cylinder with the testing particles, and then the mixing blade pressing downwards whilst rotating.


Figure 7.5: The FT4 system geometries used within Rocky DEM

### 7.4.2 BFE Results

Table 7.6 shows each of the experiments run and the BFE calculated from them. The BFE is a measure of the flowability of the powder whilst it is being forced to move, in this case by the energy required for the mixing blade to move downwards. Only one run was completed per set of parameters due to the time constraint on my placement, however more simulations per set would be run usually to get a better understanding of each parameter's influence on the BFE output.

Table 7.6: Simulation runs completed and parameter values used

| Run <br> Number | Rolling <br> Resistance | Coefficient <br> of <br> Restitution | Static and <br> Dynamic Friction <br> Coefficients | Young's <br> Modulus <br> $(\mathrm{Pa})$ | BFE <br> $(\mathrm{mJ})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.125 | 0.1 | 0.175 | $9.00 \mathrm{E}+06$ | 365 |
| 2 | 0.175 | 0.1 | 0.175 | $9.00 \mathrm{E}+06$ | 432 |
| 3 | 0.125 | 0.3 | 0.175 | $9.00 \mathrm{E}+06$ | 357 |
| 4 | 0.175 | 0.3 | 0.175 | $9.00 \mathrm{E}+06$ | 427 |
| 5 | 0.125 | 0.1 | 0.225 | $9.00 \mathrm{E}+06$ | 466 |
| 6 | 0.175 | 0.1 | 0.225 | $9.00 \mathrm{E}+06$ | 634 |
| 7 | 0.125 | 0.3 | 0.225 | $9.00 \mathrm{E}+06$ | 446 |
| 8 | 0.175 | 0.3 | 0.225 | $9.00 \mathrm{E}+06$ | 612 |
| 9 | 0.125 | 0.1 | 0.175 | $1.10 \mathrm{E}+07$ | 425 |
| 10 | 0.175 | 0.1 | 0.175 | $1.10 \mathrm{E}+07$ | 534 |
| 11 | 0.125 | 0.3 | 0.175 | $1.10 \mathrm{E}+07$ | 416 |
| 12 | 0.175 | 0.3 | 0.175 | $1.10 \mathrm{E}+07$ | 505 |
| 13 | 0.125 | 0.1 | 0.225 | $1.10 \mathrm{E}+07$ | 532 |
| 14 | 0.175 | 0.1 | 0.225 | $1.10 \mathrm{E}+07$ | 716 |
| 15 | 0.125 | 0.3 | 0.225 | $1.10 \mathrm{E}+07$ | 532 |
| 16 | 0.175 | 0.3 | 0.225 | $1.10 \mathrm{E}+07$ | 739 |
| 17 | 0.15 | 0.2 | 0.2 | $1.00 \mathrm{E}+07$ | 503 |
| 18 | 0.15 | 0.2 | 0.2 | $1.00 \mathrm{E}+07$ | 527 |
| 19 | 0.15 | 0.2 | 0.2 | $1.00 \mathrm{E}+07$ | 501 |
| 20 | 0.15 | 0.2 | 0.2 | $1.00 \mathrm{E}+07$ | 512 |

By looking at how the output BFE value was affected across each experiment, the MODDE DoE software can determine the influence each parameter has on the BFE value, as well as any influence the interaction
between parameters may have. Parameters that do not have an influence on the BFE output are removed from the calculations, refining all the parameters relationships to the BFE output to Equation 7.6. It can then use this to calculate a point within the ranges tested that satisfy our desired BFE for Compound A of 542.23 mJ , shown as value set 1 in Table 7.7. The value of 542.23 mJ was previously determined in laboratory experiments, so we can therefore use this value to determine if the simulation is accurately modelling Compound $A$. An equation to calculate the BFE can also be determined, including coefficients for each of the parameters tested based on their influence on the final BFE, determined by how big a change in the BFE value each parameter caused.

$$
B F E=-5174.26 r_{r}-2825.76 f+4.13899 e^{-5} y+39127.7(r r * f)+0 c_{r}+
$$

$$
\begin{equation*}
262.533 \tag{7.6}
\end{equation*}
$$

$$
\begin{equation*}
B F E=-5174.26 r_{r}-2825.76 f+4.13899 e^{-5} y+39127.7(r r * f)+262.533 \tag{7.7}
\end{equation*}
$$

where BFE is the Basic Flowability Energy, $r_{r}$ is the Rolling Resistance, $f$ is the Static and Dynamic Friction Coefficients, $c_{r}$ is the Coefficient of Restitution and $y$ is the Young's Modulus.

Equation 7.6 shows that the Rolling Resistance and Static and Dynamic Friction coefficients had a large influence on the BFE, with the Young's Modulus having a small influence and the Coefficient of Restitution having no influence. The interaction between the rolling resistance and the friction coefficients was also determined to have an influence. This is shown by the coefficients in the equation for the parameters that have a high influence being in the order of $10^{4}$ and $10^{5}$, whereas the parameters with a small influence had a coefficient in the order of $10^{-5}$ and 0 . For each of these influential parameters, a higher value results in a higher BFE. This fitted equation has an R2 value of 0.99 and a Q2 value of 0.97 , showing that there is a high measure of both the model's fit and predictability. R2, also known as R-squared, is a measure of
the variance of a dataset, with a value ranging from 0 to 1 . A value closer to 1 denotes that there is less variance within the dataset, and a value closer to 0 denotes that there is a large degree of variance. Our value of R2 being 0.99 in this dataset shows that the variance is minimal, and changes to the outputs are based upon our changing of the parameters and not random chance. Q2, also known as Q -squared, is a measure of the predictive relevance of a model, with a positive value denoting good predictive relevance. Our Q2 value of 0.97 shows that this model has predictive relevance. ${ }^{9}$ This equation is only valid within the specific parameter ranges tested as part of the DoE runs, stated in Table 7.5, however as the target value is within this range it does not matter. Equation 7.7 shows a simplified form of equation 7.6 , removing the parameters that had no influence on the calculation.

Runs 17 to 20 were completed using the midpoints for the range of values used for each parameter. These repeats were performed to ensure the BFE values obtained were consistent with each other when the parameter values were kept the same, as there is inherent randomness within the simulations from the particle placements, and the calculations that stem from it. Therefore, ensuring that the data gained from the repeats are similar enough, even given these changes between simulations, means that we can trust the simulations and know that variations in the outputs are due to the effect of changing parameters, rather than just a random event in a simulation. These repeats gave an average of $511 \pm 10.3$, giving a variance of just under $2 \%$.

### 7.4.3 Value Confirmation

Three sets of values were then calculated using Equation 7.6, as shown in Table 7.7, that should give the target BFE of 542 mJ , then FT4 model simulation runs were completed using these sets of values to see if the simulation and equation values were the same.

Table 7.7: "Solution" parameter sets and their determined BFE

| Value <br> Set | Rolling <br> Resistance | Coefficient <br> of <br> Restitution | Static and <br> Dynamic <br> Friction <br> Coefficients | Young's <br> Modulus <br> (Pa) | Equation <br> BFE (mJ) | Simulation <br> BFE (mJ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.156334 | 0.3 | 0.212233 | 9.3264 e 6 | 538.05 | $529.72 \pm$ <br> 10.4 |
| 2 | 0.157 | 0.3 | 0.213 | 9.33 e 6 | 542.92 | $511.14 \pm$ <br> 13.8 |
| 3 | 0.16 | 0.3 | 0.21 | 9.33 e 6 | 542.10 | $534.11 \pm$ <br> 8.50 |

Three repeats were completed for each of the value sets, and the average BFEs determined. There was some variance between each of the runs for the data parameter values due to the randomness that can occur in the system, which is consistent with the previous repeats, however Sets 1 and 3 both gave values close to the desired output. Run 2 gave consistently lower BFE values than anticipated, even with the equation stating it should have been close to 542 mJ , showing that there are likely more interactions at play than our current series of experiments account for. Given more time, a larger range of values would have been used across more variables, to be able to investigate the effect of as many parameters as possible and looking for valid values within a larger range, instead of focusing on a narrower area.

As there were many sets of values that can satisfy the expected BFE condition, we then used these values to simulate a test to calculate the Angle of Repose (AoR) of Compound A, another property which can be readily compared to an experimentally measured value. The simulations involved filling a cylinder with our particles, then slowing raising the cylinder, allowing the particles to form a pile on a platform below it, as shown in Figure 7.6. Five
repeats were completed for each of the value sets identified in Table 7.7, and the angles calculated are shown in Table 7.8.


Figure 7.6: A cylinder of particles before and after it has been lifted to allow the particles to settle forming a heap.
Each simulation gave two angles, one calculated from the bottom of the pile and one calculated from the top, as illustrated in Figure 7.7. To calculate the angle, a line is drawn across the pile of particles, and the maximum height at set intervals across the line is calculated. The line then rotates $10^{\circ}$ around the $y$-axis (normal to the platform) and the heights collected again. This is repeated until the line has rotated a full $360^{\circ}$ and is back in its starting rotation.

The black dots in Figure 7.7 represent the average of the maximum heights at each of the intervals used. The light red area is the maximum of the maximum heights found, with the dark red area being the minimum of the


Figure 7.7: Example particle system with labelled Angles of Repose from Ansys Rocky DEM
maximum heights found. Using the average maximum heights, the angles are then calculated, as shown by the fitting lines.

Table 7.8: The Angles of Repose calculated for each of the parameter value sets tested

| Value Set | Bottom AoR <br> $\left({ }^{\circ}\right)$ | Top AoR $\left({ }^{\circ}\right)$ |
| :---: | :---: | :---: |
| 1 | $14.9 \pm 1.8$ | $18.9 \pm 0.9$ |
| 2 | $14.7 \pm 2.4$ | $18.2 \pm 1.2$ |
| 3 | $17.2 \pm 1.9$ | $20.0 \pm 2.3$ |

The values calculated by the model can then be compared with the laboratory value to determine which parameter value sets are closest. Alongside the data from the BFE experiments, the values can be checked to see which ones satisfy both tests. The laboratory values for the AoR for Compound A were not able to be obtained before the end of my project, however these data can still be used for comparison once the data is available.

### 7.5 Summary and Conclusions

At this point my placement came to an end, however a discussion was had about how this work would be used by AstraZeneca going forward. More conditions would be required to confirm the parameter values as only two conditions, being the BFE and AoR, do not give enough confidence in the values generated by Ansys Rocky DEM. Other possible confirmation experiments could be Ring Shear Tests ${ }^{10}$ or Granudrum ${ }^{11}$ equipment testing for powder cohesion. This would be the next stage for AstraZeneca going forward to further confirm the data values for the parameters we have tested, as well as testing as many other parameters as possible, to increase the confidence in the parameter values determined. Once a full set of model parameters are obtained, simulation of Compound A would be possible.

The Design of Experiments method was useful for having a predetermined set of experiments to run instead of taking a trial-and-error approach, as it gave more structure to the workflow. It also allowed us to properly investigate and determine the effects of each parameter, instead of just finding a value set that satisfied our condition.

The comparisons between my model and Rocky DEM showed them producing very similar packing fraction data, showing the same trend across different particle size distributions. This increases my confidence in the accuracy of my model, as it compares with professionally made software.

### 7.6 References

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## 8 Conclusions and Future Work

### 8.1 Summary and Conclusions

Over the course of the project multiple algorithms have been produced to investigate particle packing, in both 2D and 3D, and with spherical and nonspherical particles. Initial investigations were done into these systems, comparing them to systems created by other models and the expected mathematical answers to the properties, such as minimum/maximum packing fractions.

Comparisons were made between the packing of the 2D and 3D systems that were produced, containing single-sized particles, against previously calculated values of packing fractions for perfectly packed structures, and those created under different algorithms. It was found that my system's packing fraction values fell within the expected range, as they were less than the most ordered system, as my systems have a degree of randomness, and were above the packing fractions of RSA systems, where the circles are not under as many constraints as within my systems therefore pack less efficiently. Initial investigations were also made into the number of contacts each particle had compared to the expected amount, four in 2D and six in 3D, with this being mostly shown in the data however it was greatly affected by the box size therefore further investigation with larger systems sizes is needed.

An improvement was made to the model to allow chain particles to be created within the systems. The packing fractions were found to be rather consistent, especially compared to the single particle systems, and an expected increase when single void-filling particles were added into the systems. The angles of the chains were also determined, and it was found that as the chains became longer, the particles tended to rest more vertically.

The model was also compared to Industry standard software, Rocky Ansys DEM, and it was found that when similar systems were created in both models, the data found was very similar. This gives a lot of confidence in the outputs of my model as they are being corroborated by modelling software that has been used in many different scientific studies.

Once consistent note throughout each of the systems was the effect of the size of the box on the outputs. As these were only initial tests, the box sizes were often limited by the project duration, or the capabilities of the model at the time. Now the model has improved, investigations into larger systems are possible in future projects. The evidence presented provides confidence in these algorithms such that they can be used in future work to investigate these structures further and the model can be further improved to investigate a wider range of systems and properties.

The research completed through this project has given some more insight into the packing of spherical shapes when placed under gravity, as well as some investigation into non-spherical shapes. This aids other research completed into these topics and the completion of this model allows another avenue into further investigation into both these questions, as well as, once the model has had more features implemented, further areas within this topic. The creation of this model allows for more direct research into the packing of the systems it creates. Due to its simplicity, the model could be applied to a variety of different fields, beyond the initial pharmaceutical base it was created for, as with no defined scale the particle could be any size the researcher wants, e.g. larger for use in soil sciences. It is also an easy base to build on, compared to editing more complex modelling software or creating new forcefields, so can again be tailored for a variety of applications.

Some of the project objectives were achieved with the completion of the current algorithms, however preferably the 3D chains algorithm would have been completed, along with the upgraded version of the contact breakage
algorithm. Details of these plans and other future work are discussed in the next section.

### 8.2 Future Work

As this project has created the basis of a modelling system, there are many various applications for it going forward beyond my project.

Some of the most obvious are continuations of work that has been started as part of my project but could not be investigated to the extent that would be wanted, such as the investigation into the contact forces present between particles. The 3D non-spherical particle algorithm could be finalised, so that initial property investigations, as have been done for 2D and 3D spherical particle structures, can be completed. In addition, it would be preferable if the spherical basis of the chain particles could be removed to be able to model smooth edged particles. One way this could be approached with the current method is to increase the amount by which the circular particles, that make up a chain, overlap, to create a smoother surface.

Further work could be done to gain a larger range of data in 2D systems, investigating the effects, if any, of percolation structures and particle size distribution on how the bed breaks apart. The algorithm could also be expanded to be able to handle 3D structures and non-spherical particle structures.

Further investigation of some of the phenomena observed during the initial tests of the model, such as looking at the path that a small particle takes through a bed formed of larger particles would be desirable. This could also help to investigate fluid paths through the bed. As part of potentially investigating fluids, additional dynamics would be added to the model, such as solvent effects, and particles being affected by friction as they are settling.

Experimental work could also be done alongside the model systems created, one of which would be to build on recent unpublished work undertaken using the Diamond Light Synchrotron to gather images of packed systems that can be compared against those that the model produces. Breakage tests can also be done to see how systems break apart under stresses to compare to our breakage algorithm.

As the scales of the particles is separate from the units used, the particles could be any size that the user desires them to be. For example, the model could be used within soil sciences to model the settling of larger particulates than would be investigated in the pharmaceutical industry.

## Appendix 1: 2D System Algorithm

This appendix contains the algorithm used for creating 2D systems.

```
    module allSubs ! Initialises the variables used through all functions
    character, dimension (:,:), allocatable, public :: RA*4
    integer, dimension (:,:), allocatable, public :: RAMoIClose
    integer MolNo, RadLarge, RadSmall, BoxSize, GridSize, Rads, count, SN, Full,
    integer MLr, AllocateVal, RoofCount
    real MLxReal, MLyReal
    integer, dimension (:,:), allocatable, public :: Ones
    integer, dimension (:,:), allocatable, public :: Contacts
    dimension MLr(10000), Rads(10), MLxReal(10000), MLyReal(10000)
    logical FullCheck, Hit, RoofHit, StartPlace
    integer x, y, Long, Tall, RadT
    end module allSubs
```

FullCount
program packedbed
use allSubs ! Loads the variables from the module
! Initialises local variables
character t, FileName*15, FileID*3
integer m, n, check, PrintNo, ProgCount, PCId, count3
dimension FileID(1000)
real Rand, Dist
integer count2, RadTnew, TotLength
logical Finished, Cont, Impact
StartPlace = .TRUE.
$t=' y '$
if ( $t==$ ' $y$ ') then
Rads(1) = 10 ! Sets the radius of a particle. Additional radii would be
inputted as Rads( x ) = 'Radius'
$\mathrm{SN}=1 \quad$ ! Sets the number of different radii in the system
RadLarge $=0$
RadSmall $=0$
do count $=1, \mathrm{SN}$
if (RadLarge < Rads(count)) then
RadLarge = Rads(count)
end if
if (RadSmall > Rads(count) .or. RadSmall $==0$ ) then
RadSmall = Rads(count)
end if
end do
RadLarge $=10$
RadSmall $=10$
! Calculates the box size based on the largest radius present
BoxSize $=($ RadLarge*6)
GridSize $=$ BoxSize*5
AllocateVal $=(($ BoxSize*3)**2)*2
! Allocates the arrays allocate(RA(1:GridSize, 1:GridSize))
allocate(RAMoIClose(1:GridSize, 1:GridSize))
allocate(Ones(1:AllocateVal, 1:2))
do ProgCount = 1, 50
write(FileID(ProgCount), '(i0)') ProgCount
end do
do ProgCount $=1,50!$ Starts the loop for the number of systems to be created

```
! Sets variables initial values
MLxReal = 0
MLyReal \(=0\)
\(\mathrm{MLr}=0\)
TotLength \(=0\)
MolNo = 1
FileName = "
Full = 0
check \(=0\)
FullCount \(=0\)
Finished = .FALSE.
Ones \(=0\)
\(R A=' 0\)
RAMoIClose \(=0\)
RoofCount = 0
RoofHit = .FALSE.
call random_seed()
do while (count < 10000000)
Impact \(=\).FALSE.
! Picks a random radius and x coordinate, and sets y to be on
```

```
call random_number(RX)
```

call random_number(RX)
count2=1 + floor(SN*RX)
count2=1 + floor(SN*RX)
RadT = Rads(count2)
RadT = Rads(count2)
call random_number(RX)
call random_number(RX)
count2 = 1 + floor((GridSize-(2*RadT))*RX)
count2 = 1 + floor((GridSize-(2*RadT))*RX)
x = count2+RadT
x = count2+RadT
y = RadT

```
y = RadT
```

the bottom of the box
if $($ MoINo $>1)$ then $\quad$ ! Checks there is already at least
one particle in the system
hitloop: do count3 $=1$, MoINo - 1
Dist $=\quad(($ MLxReal $(c o u n t 3)-$
$\left.x)^{\star *} 2\right)+(($ MLyReal(count3)-y)**2)
Dist $=\operatorname{sqrt}($ Dist $)$
if (Dist $<=(($ RadT*2 $)+($ Mlr(count3) $)))$ then
count = count + 1
Impact = .TRUE.
exit hitloop
end if
end do hitloop
if (Impact .eqv. .FALSE. .and. $x<=$ GridSize-
(RadT*2)) then ! If the particle is not overlapping with any others and is inside the grid, its location is saved

```
                                    count = 0
                                    MLxReal(MolNo) = x
                                    MLyReal(MolNo) = y
                                    MLr(MolNo) = RadT
                                    MolNo = MolNo + 1
                    end if
            else
                        MLxReal(MolNo) =x
                            MLyReal(MolNo) = y
                            MLr(MolNo) = RadT
                    MoINo = MoINo + 1
                    end if
    end do
```

! This loops through the base line to check that there is nowhere a small particle could fall through to the bottom of the box, and if so, places a particle there
do $m=$ RadSmall, GridSize-RadSmall RadT = RadSmall Impact = .FALSE. hitloop2: do count3 = 1, MoINo - 1

Dist $=\left((\text { MLxReal }(\text { count } 3)-m)^{* *} 2\right)$
Dist $=$ sqrt(Dist)
if (Dist < ((RadSmall) $+(\operatorname{Mlr}($ count3) $)))$ then count = count + 1 Impact = .TRUE. exit hitloop2
end if
end do hitloop2 if (Impact .eqv. .FALSE.) then

$$
\text { count }=0
$$

$\operatorname{MLxReal}(\mathrm{MolNo})=m$
MLyReal(MoINo) = RadSmall
MLr(MolNo) = RadSmall
MoINo $=$ MoINo +1
end if
end do
StartPlace = .FALSE .
do $\mathrm{n}=1,2500$ ! Loops for each particle being added to the system, using the main function. At the end of each loop, it checks if the box is full and if so, leaves the loop.


```
                end if
            end do
    end if
    end program
```

subroutine molpos
use allSubs ! Loads the variables from the module
! Sets up the local variables
integer count2, Spot, Height, DoubRad, RowRad, a,b,c, Radln, m, n, TempX, TempY
real Rand, MidWay, Dist
character t, FileName*15
integer SavIncremX, SavIncremY, SafeLocCount, LR, SavOneX, SavOneY, SavDist,
SavOnePart, LRNo, OneCount, RealPos1, RealPos2
integer TempRealPos1, TempRealPos2
logical SafeLocFound, ResetCheck
real TempXa, TempXb, TempYa, TempYb, DistAB, DistBC, DistAC, AngleA, AngleB,
AngleFin, GradFin, HelpDist
real FDistA, FDistB, FDistC, FDistD
real xDiff, yDiff, FinalSavX, FinalSavY
integer FinalSavLong, FinalSavTall, checktime, Balanced
integer Balances, Touches
dimension Balances(10)
real DistFac, RadScale
integer NewPos, TRP1Swap, TRP2Swap
integer FinalPart, SideCount
dimension FinalPart( 2,3 )
real PartCoords, stochDists, sumDist, dx, stochxnew, newCoords, stochynew
integer ibad
dimension PartCoords(2,2), stochDists(2), newCoords(2), dx(2), stochxnew(2)
real RX, NewX, NewY
logical ChainAdd
real OverDist
integer OverDistNo
logical NotBal, FirstBal
dimension BalCheckNo(10000), BalCombi(100000,2)
integer BalCheckCount, BalCount, BalCheckNo, BalCombi, BalAttempt
integer OverlapCount
logical EdgeCase, FirstEdge
integer EdgeCombi, EdgeCount, EdgeAttempt
dimension EdgeCombi(10000)
real Dy, intC, CheckY
CONTINUE
if (FullCount $==2500000$ ) then
Full = 1
end if
! Setting initial values of variables
Hit = .FALSE.
ResetCheck = .FALSE.
checktime $=1$
Balanced = 0
Touches = 0

Balances $=0$
$D y=0$
intC = 0
Check $Y=0$
EdgeAttempt $=0$
EdgeCount = 0
EdgeCombi $=0$
EdgeCase = .FALSE .
FirstEdge = .TRUE.
FinalPart $=999999$
OverDist $=0$
OverDistNo $=0$
OverlapCount $=0$
TRP1Swap $=0$
TRP2Swap $=0$
ChainAdd = .FALSE.
NotBal = .FALSE.
FirstBal = .TRUE.
BalCheckNo = 0
BalCombi $=0$
BalCheckCount $=0$
BalCount = 0
BalCheckNo = 0
BalCombi $=0$
BalAttempt $=0$
RadScale $=0$
TempRealPos1 = 0
TempRealPos2 $=0$
DistFac = 0
FDistA $=0$
FDistB $=0$
FDistC $=0$
FDistD $=0$
SavDist $=0$
SavOneX = 0
SavOneY = 0
TempXa = 0
TempXb $=0$
TempYa $=0$
TempYb = 0
DistAB $=0$
DistBC $=0$
DistAC $=0$
AngleA $=0$
AngleB $=0$
AngleFin $=0$
GradFin $=0$
$x$ Diff $=0$
$y$ Diff $=0$

NewPos = 0

FinalDists $=0$
PartCoords $=0$
stochDists $=0$
sumDist = 0
$\mathrm{dx}=0$
stochxnew $=0$
newCoords $=0$
stochynew = 0
! Randomly chooses which radius will be used for this particle call random_number(Rand)
RadScale $=$ RadLarge/RadSmall
RadScale $=$ RadScale +1
count2 $=1+$ floor(2*Rand)
if (count2 == 2) then
RadT = RadLarge
else
RadT $=$ RadSmall
end if
wloop: do while (Hit .eqv. .FALSE.) ! The loop to place particles
! Randomly chooses the x value call random_number(Rand)
Spot $=1+$ floor ((GridSize-(2*RadT))*Rand)
x = Spot+RadT
do $y=$ GridSize, RadT, $-1 \quad$ ! Loops from the top of the box, and sends to
the function to determine impact
Long $=(x /$ BoxSize $)+1$
Tall $=(\mathrm{y} /$ BoxSize $)+1$
call PointSafe
! If the box is full or an impact has occured, the loop is exited
if (Full $==1$ ) then
exit wloop
end if
if (FullCheck .eqv. .TRUE.) then
RoofHit = .TRUE.
GO TO 10
end if
if (Hit .eqv. .TRUE.) then exit wloop
end if
end do
end do wloop
if (Hit .eqv. .TRUE. .and. Full /=1) then
if $(\mathrm{MolNo}>1)$ then
$R A=10 '$
RAMolClose $=0$
! Sets up the variables to be used for particle placement
Ones = 0
OneCount = 1
do $\mathrm{a}=1$, MolNo - $1 \quad$ ! Loops through the particles for contour plot
placement
MLxCor $=$ MLxReal(a)
MLyCor $=$ MLyReal(a) ! Takes the radius, $x$ and $y$ coordinates
of the current particle in the loop
RadIn $=\operatorname{Mlr}(\mathrm{a})$
DoubRad $=($ RadIn + RadT $)+1$
do Height = 0, Radln ! Draws the particle onto the contour
plot, "-"s marking blocked locations, "1"s being valid spots
MidWay = RadIn**2 - Height**2
RowRad = abs(sqrt(MidWay))
if (MLxCor+Height<=GridSize-RadT .and.
MLyCor+RowRad<=GridSize .and. MLyCor-RowRad>=RadT .and. MLxCor-Height<=RadT) then

RA(MLyCor+RowRad, MLxCor+Height) = ' - '
RA(MLyCor-RowRad, MLxCor+Height) = '-'
RA(MLyCor+RowRad, MLxCor-Height) = '-'
RA(MLyCor-RowRad, MLxCor-Height) = '-'
end if
do count2 $=-$ RowRad,RowRad
if (MLxCor+Height<=GridSize-RadT .and.
MLyCor+count2<=GridSize .and. MLxCor-Height>=RadT .and. MLyCor+count2>=RadT) then RA(MLyCor+count2,
MLxCor+Height) = '-'
RA(MLyCor+count2, MLxCor-
Height) $=$ ' - '
end if
end do
end do
do Height = 0, DoubRad ! Draws locations around the current particle that are too close for the new particle to be added due to overlap

MidWay $=$ DoubRad**2 - Height**2
RowRad = abs(sqrt(Midway))
do count2 $=$-rowrad+1, rowrad-1
if (MLyCor+count2<=GridSize .and.
MLxCor+Height<=GridSize-RadT .and.
MLxCor+Height>=RadT) then
MLyCor+count2>=RadT
.and.

MLxCor+Height) = '-'
RA(MLyCor+count2,
end if
if (MLyCor+count2<=GridSize .and.
MLxCor-Height<=GridSize-RadT .and.
Height>=RadT) then
Height) = '-'
RA(MLyCor+count2, MLxCor-
end if
end do
end do

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do Height $=-$ Radln, Radln
do count2 $=$ MlyCor-1, 1, -1
if (count2<=GridSize
.and.
MLxCor+Height<=GridSize-RadT .and. count2>=RadT .and. MLxCor+Height>=RadT) then
RA(count2, MLxCor+Height) = ' - '
end if
end do
end do
do Height $=-$ DoubRad, $0 \quad$ ! Adds the valid spots for the resting particle to be placed

MidWay $=$ DoubRad**2 - Height**2 $^{*}$
RowRad = abs(sqrt(Midway))
if (MLyCor+RowRad<=GridSize .and.
MLxCor+Height<=GridSize-RadT
MLyCor+RowRad>=RadT) then
.and. MLxCor+Height>=RadT .and.
/= '-') then
if (RA(MLyCor+RowRad, MLxCor+Height)

MLxCor+Height) = '1'
RA(MLyCor+RowRad,

MLxCor+Height) $=\mathrm{a}$
RAMoIClose(MLyCor+RowRad,
end if
end if
if (MLyCor-RowRad>=RadT .and.
MLxCor+height<=GridSize-RadT
.and. MLxCor+height>=RadT .and. MLyCor-
RowRad<=GridSize) then
if (RA(MLyCor-RowRad, MLxCor+Height) /=
'-') then
RA(MLyCor-RowRad,
MLxCor+Height) = ' 1 '
RAMoIClose(MLyCor-RowRad,
MLxCor+Height) $=\mathrm{a}$
end if
end if
if (MLyCor+RowRad<=GridSize .and. MLxCor-Height<=GridSize-RadT .and. MLxCor-Height>=RadT .and. MLyCor+RowRad>=RadT) then if (RA(MLyCor+RowRad, MLxCor-Height) /= '-') then

Height) = '1'
MLxCor-Height) $=\mathrm{a}$
RA(MLyCor+RowRad, MLxCor-
RAMoIClose(MLyCor+RowRad,
end if
end if
if (MLyCor-RowRad>=RadT .and. MLxCor-height<=GridSize-RadT .and. MLxCor-height>=RadT .and. MLyCor-RowRad<=GridSize) then
'-') then
Height) = '1'
MLxCor-Height) $=\mathrm{a}$
if (RA(MLyCor-RowRad, MLxCor-Height) /= RA(MLyCor-RowRad, MLxCor-

RAMoIClose(MLyCor-RowRad,
end if
end if do count2 $=-$ RowRad, RowRad

MLxCor+height<=GridSize-RadT .and. MLxCor+height>=RadT and. MLyCor+count2>=RadT) then
(MLyCor+count2<=GridSize .and.
if (RA(MLyCor+count2,
MLxCor+Height) /= '-') then
MLxCor+Height) = '1'
RAMoIClose(MLyCor+count2, MLxCor+Height) $=\mathrm{a}$ end if
end if
if (MLyCor-count2>=RadT .and. MLxCor+height<=GridSize-RadT .and. MLxCor+height>=RadT .and. MLyCorcount2<=GridSize) then
if
(RA(MLyCor-count2,
MLxCor+Height) /= '-') then
RA(MLyCor-count2,
MLxCor+Height) = '1'
RAMoIClose(MLyCor-
count2, MLxCor+Height) = a
end if
end if
if (MLyCor+count2>=RadT .and. MLxCor-height<=GridSize-RadT .and. MLxCor-height>=RadT .and. MLyCor+count2<=GridSize) then if (RA(MLyCor+count2, MLxCorHeight) /= '-') then

RA(MLyCor+count2,
MLxCor-Height) = '1'
RAMoIClose(MLyCor+count2, MLxCor-Height) $=\mathrm{a}$

## end if

end if
if (MLyCor-count2<=GridSize .and. MLxCor-height<=GridSize-RadT .and. MLxCor-height>=RadT .and. MLyCor-count2>=RadT) then if (RA(MLyCor-count2, MLxCorHeight) /= '-') then

RA(MLyCor-count2,
MLxCor-Height) = '1'
RAMoIClose(MLyCor-
count2, MLxCor-Height) $=\mathrm{a}$
end if
end if
end do
end do
end do
do $\mathrm{a}=1$, GridSize $!$ Finds the valid points and saves them to an array do $b=1$, GridSize
if $(R A(b, a)==$ ' 1 ') then
Ones(OneCount, 1) = b
Ones(OneCount, 2) = a
OneCount = OneCount + 1
end if
end do
end do
do $\mathrm{a}=1$, OneCount -1 ! Finds the closest of these points to the impact location and moves the particle to it

TempX = Ones(a,2)
TempY = Ones( $\mathrm{a}, 1$ )
if (TempY <= $y+1$ ) then
Dist $=\left((x-\text { TempX })^{* *} 2\right)+\left((y-\text { TempY })^{* *} 2\right)$
Dist $=$ sqrt(Dist) if (Dist < SavDist .or. SavDist $==0$ ) then

SavDist $=$ Dist
SavOneX = Ones(a,2)
SavOneY = Ones(a,1)
end if
end if
end do
TempX = SavOneX
TempY = SavOneY
if $($ TempX $==0$.and. TempY $==0)$ then GO TO 10
end if
SavOnePart = RAMoIClose $($ TempY, TempX)
SafeLocCount = 0
SavIncremX = SavOneX
SavIncremY = SavOneY
SafeLocFound = .FALSE.
FinalSavX = 0
FinalSavY $=0$
$\mathrm{LR}=0$
RealPos1 $=0$
RealPos2 $=0$
if (MLxReal(SavOnePart) == TempX) then! Determines which way
the particle should roll call random_number(Rand)
LRNo = $1+$ floor(2*Rand)
if $(\mathrm{LRNo}==1)$ then
$L R=-1$
elseif (LRNo ==2) then
$L R=1$
end if
elseif (MLxReal(SavOnePart) < TempX) then $L R=1$
elseif $(M L x R e a l(S a v O n e P a r t)>$ TempX) then
$L R=-1$
end if

RMPInter $=0$
RMPPrev = SavOnePart
RealPos1 = SavOnePart
do $\mathrm{a}=1$, OneCount -1
if (Ones( $\mathrm{a}, 2$ ) $==$ TempX) then
SideCount = a
end if
end do
do while (SafeLocFound .eqv. .FALSE.) ! Iterates in that direction until the next position would be higher, or reaching the edge of the box
if (Ones(SideCount+LR,1) > Ones(SideCount,1) .or. Ones(SideCount,2) == RadT .or. Ones(SideCount,2) == GridSize-RadT) then

SafeLocFound = .TRUE.
else
SideCount $=$ SideCount + LR
end if
end do
TempX = Ones(SideCount,2)
TempY = Ones(SideCount,1)
do $\mathrm{a}=1$, MolNo-1 ! Finds the particles closest to the low point for the new particle to be resting on
if (MLyReal(a) < TempY+RadT) then
Dist $=((M L x R e a l(a)-T e m p X) * * 2)+(($ MLyReal $(a)-$
TempY)**2)
Dist $=$ sqrt(Dist) - RadT - MLr(a)
if (Dist <= FinalPart(1,2)) then
FinalPart(2,1) = FinalPart(1,1)
FinalPart(2,2) = FinalPart(1,2)
FinalPart( 2,3 ) $=$ FinalPart $(1,3)$
FinalPart(1,1) =a
FinalPart(1,2) = Dist
FinalPart(1,3) $=$ Dist + RadT $+\operatorname{MLr}(\mathrm{a})$
elseif (Dist <= FinalPart( 2,2 )) then
FinalPart $(2,1)=\mathrm{a}$
FinalPart(2,2) = Dist
FinalPart(2,3) $=$ Dist + RadT $+\operatorname{MLr}(\mathrm{a})$
end if
end if
end do
CONTINUE
PartCoords(1,1) $=$ MLxReal(FinalPart(1,1))
PartCoords $(1,2)=$ MLyReal(FinalPart $(1,1))$
PartCoords(2,1) = MLxReal(FinalPart(2,1))
PartCoords(2,2) $=$ MLyReal(FinalPart(2,1))
if (TempX == RadT .or. TempX == GridSize-RadT) then
EdgeCase = .TRUE.
end if
if (EdgeCase .eqv. .TRUE.) then ! If the particle is on an edge, it balances the new particle on the edge + one particle
NewX = TempX

$$
\text { Dist }=\text { RadT }+ \text { MLr(FinalPart }(1,1))
$$

NewY
=
(MLxReal(FinalPart(1,1))**2)+(2*MLxReal(FinalPart(1,1))*NewX)

```
NewY = NewY + (Dist**2)-(New \(\left.{ }^{* *} 2\right)\)
New \(Y=\operatorname{sqrt}(\) New \(Y\) )
if (NewY /= NewY) then
```

CONTINUE
if (FirstEdge .eqv. .TRUE.) then do $\mathrm{a}=1$, MolNo-1

Dist $=($ MLxReal $(a)-N e w X)$
if (Dist $<$ RadT $+\quad$ MLr(a) +
(RadT*8)) then
EdgeCombi(EdgeCount) =
EdgeCount = EdgeCount +
1
end if
end do
end if
FirstEdge $=$. FALSE .
if (EdgeAttempt <= EdgeCount-1) then
FinalPart(1,1) = EdgeCombi(EdgeCount-
EdgeAttempt)
EdgeAttempt = EdgeAttempt +1
GO TO 50
end if
FullCount $=$ FullCount +1
GO TO 10
end if
if (TempY - (MLyReal(FinalPart(1,1)) + NewY) < TempY -
(MLyReal(FinalPart(1,1)) - NewY)) then
New $Y=\operatorname{MLyReal}($ FinalPart(1,1)) + New $Y$
else
New $Y=$ MLyReal(FinalPart(1,1)) - New $Y$
end if
do $\mathrm{a}=1$, MoINo- $1 \quad!$ Confirming the new particle is not overlapping with any other particles

Dist $=\left((\text { MLxReal }(a)-N e w X)^{* *} 2\right)+(($ MlyReal $(a)-$ New $Y$ ) **2)

Dist $=$ sqrt(Dist)
if (Dist < MLr(a)+RadT-0.25) then
OverlapCount $=$ OverlapCount +1 if (OverlapCount > 2500) then

GO TO 10
end if
FinalPart(1,1) = a
FullCount $=$ FullCount +1
GO TO 50
end if
end do
if (NewX < RadT .or. NewY < RadT .or. NewX > GridSizeRadT .or. New $Y>$ GridSize-RadT) then

FullCount $=$ FullCount +1 GO TO 25
end if
else ! else if the particle is not on an edge it balances on two particles through stochastic optimisation

```
newCoords(1) \(=\) TempX
newCoords(2) \(=\) TempY
stochDists(1) = FinalPart(1,3)
stochDists(2) \(=\) FinalPart \((2,3)\)
sumDist \(=\) stochDists(1) + stochDists(2)
\(\mathrm{dx}(1)=10\) * RadLarge
\(d x(2)=10\) * RadLarge
do \(a=1,10\)
    do \(b=1,2\)
        \(d x(b)=d x(b) / 10\)
    end do
    do \(c=1,500\)
        call random_number(RX)
        stochxnew \((\overline{2})=\) newCoords(2) \(+d x(2)\) *
    call random_number(RX)
    stochxnew(1) \(=\) newCoords(1) \(+d x(1)\) *
```

    (2*RX-1)
    (2*RX-1)
ibad $=0$
do $b=1,2$
stochDists(b) $=(($ PartCoords(b,1)-
stochxnew(1))**2)+((PartCoords(b,2)-stochxnew(2))**2)
stochDists(b) $=$ sqrt(stochDists(b)) -
RadT - MLr(FinalPart(b, 1))
if (stochDists $(b)<0)$ then
ibad = 1
end if
end do
stochynew $=$ stochDists(1) + stochDists(2)
if (stochynew < sumDist .and. ibad == 0)
then
stochxnew(b)

$\quad$| do $b=1,2$ |
| :--- |
| newCoords(b) |
| end do |
| end if |
| sumDist = stochynew |

end do
New $X=$ newCoords(1)
New $Y=$ newCoords(2)

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```
if (NewY < CheckY) then
    NotBal = .TRUE.
    end if
```

    CONTINUE
    OverlapCount \(=0\)
    If (NotBal .eqv. .TRUE.) then ! If the particle is not
    correctly balancing then it looks for alternate particles to be resting on and moves to that
location
if (FirstBal .eqv. .TRUE.) then
if (FinalPart $(1,1)>$ FinalPart $(2,1))$ then count $=$ FinalPart $(1,1)$
FinalPart $(1,1)=$ FinalPart $(2,1)$
FinalPart(2,1) = count GO TO 50
end if
do $\mathrm{a}=1$, MolNo-1
Dist $=\left((\text { MLxReal }(a)-\text { TempX })^{* *} 2\right)$ Dist $=$ sqrt(Dist)
if (Dist $<$ RadT $+\operatorname{MLr}(\mathrm{a}) \quad+$
(RadT*8)) then

## BalCheckNo(BalCheckCount) = a

BalCheckCount + 1
end if
end do
aLoop: do a = 1, BalCheckCount-1
do $b=1$, BalCheckCount-1
if $(b<a)$ then
if (BalCount <=
100000) then
(BalCheckNo(a) /= 0 .and. BalCheckNo(b) /=0) then
(abs(MlxReal(BalCheckNo(a)) - MlxReal(BalCheckNo(b))) <= RadT*2 + MLr(BalCheckNo(a)) + MLr(BalCheckNo(b))) then

BalCombi(BalCount,1) = BalCheckNo(a)
BalCombi(BalCount,2) = BalCheckNo(b)
BalCount $=$ BalCount +1
end if
end if
else
exit aLoop
end if
end if
end do
end do aLoop
end if

FirstBal = .FALSE.
if (BalAttempt <= BalCount-1) then
FinalPart $(1,1)=$ BalCombi(BalCount-

BalAttempt,2)
FinalPart $(2,1)=$ BalCombi(BalCount-
BalAttempt = BalAttempt + 1
if (BalAttempt <= 100000) then GO TO 50
end if
end if
if (TempX >= GridSize-(RadT*5)) then
OverlapCount = 0
TempX = GridSize-RadT
EdgeCase = .TRUE.
GO TO 50
elseif (TempX <= RadT+(RadT*5)) then
OverlapCount = 0
TempX = RadT
EdgeCase = .TRUE.
GO TO 50
end if
GO TO 10
end if
end if
if (NewX > GridSize-RadT .or. NewX < RadT .or. NewY > GridSize-
RadT .or. New $Y$ < RadT) then! Confirms the particle is within the bounds of the box
if (TempX >= GridSize-RadT-RadT) then
OverlapCount = 0
TempX = GridSize-RadT
EdgeCase = .TRUE.
GO TO 50
elseif (TempX <= RadT+RadT) then
OverlapCount = 0
TempX = RadT
EdgeCase = .TRUE.
GO TO 50
end if
GO TO 10
end if
MIxReal(MoINo) $=$ NewX
! Saves the particle location
MlyReal(MoINo) $=$ New $Y$
MLr(MolNo) = RadT
FullCount = 0
MoINo = MolNo +1
$R A=$ ' 0 '
RAMolClose $=0$
end if

CONTINUE
else

$$
\text { Full = } 1
$$

end if
end
subroutine PointSafe! Determines if the falling particle has impacted yet use allSubs ! Loads the variables from the module
integer a, b
real Dist
character t
Hit = .FALSE.
FullCheck = .FALSE.
! Checks the distance between the current falling particle location and previously placed partice to determine if it has impacted
cloop: do $\mathrm{a}=1$, MoINo - 1
Dist $=\left((\operatorname{MlxReal}(\mathrm{a})-\mathrm{x})^{* *} 2\right)+\left((\text { MlyReal }(\mathrm{a})-\mathrm{y})^{* *} 2\right)$
Dist $=$ sqrt(Dist)
if $($ Dist $<=((\operatorname{RadT})+(\operatorname{Mlr}(\mathrm{a}))))$ then
Hit = .TRUE. exit cloop
end if
end do cloop
! If the impact is above the top of the box, a counter is incremented to show the box may be full
if ((Hit .eqv. .TRUE.) .and. ( $\mathrm{y}>=($ GridSize $-\operatorname{Rad} T))$ ) then
Hit = .FALSE.
FullCount $=$ FullCount +1
RoofCount $=$ RoofCount +1
end if
if (RoofCount $>=2500$ ) then
FullCheck = .TRUE.
end if
if (FullCount $==2500000$ ) then

```
            Full = 
```

end if
end

## Appendix 2: Percolation Chain Detection Algorithm

This appendix contains the algorithm used to investigate both 2D and 3D systems for percolation chains. As it only looks at the contacts between the particles, the number of dimensions is irrelevant to it, excluding when importing file data.

```
Module VarList! Initalises variables to be used across all functions
real, dimension ()}\mathrm{ , allocatable :: MLxReal
real, dimension (:), allocatable :: MLyReal
Ireal, dimension (:), allocatable :: MLzRea- - Needs to be included for 3D systems
integer, dimension (:), allocatable :: MLr
integer, dimension (:,:), allocatable :: Contacts
integer, dimension (:), allocatable :: Visited
integer, dimension (:), allocatable :: TotShap
integer, dimension (:,:), allocatable :: Edge
integer, dimension (:), allocatable :: EdgeCount
integer :: n
integer :: nlines
integer :: GridSize
end module
program VoidCalcs
use VarList ! Loads module variables
! Initialises local variables and sets their starting values
character FileName*15, t*1
integer nlinesB, Depth, ShapeCount, CurCont, y, m
integer, dimension (1:250) :: Path
integer, dimension (1:20000,1:250) :: SetPath
integer, dimension (1:20000,1:250) :: Shapes
integer, dimension (1:20000) :: ShapesPrint
logical Found
integer, dimension (:), allocatable :: LocalShapeCount
integer, dimension (:), allocatable :: TotCont
integer, dimension (1:20000) :: ShapeLength
integer :: RadLarge
integer :: count
integer :: x
integer :: LoopCount
integer :: ProgCount
integer :: PCld
character, dimension (200) :: FileID*3
logical :: fileexists
integer :: OutCount
do ProgCount = 1,50
    write(FileID(ProgCount)، '(i')') ProgCount
end do
do ProgCount = 1,50 ! Loop for number of files to be investigated
RadLarge = 0
```

GridSize $=0$
$\mathrm{m}=0$
$x=0$
$\mathrm{n}=0$
nlines $=0$
nlinesB = 0
ShapeCount = 1
CurCont = 0
$y=0$
FileName '""
FileName = tri177djusttl(FileID(ProgCount))) /‘'.c'v'
INQUIRE(File=FileName, EXIST=fileexists)
if (fileexists .eqv. .FALSE.) then
GO TO 50
end if
! Confirms the files exists and if so loads it, if not skips it and moves to the next
open(1, file = FileName, statu'='o'd')
do
read(1, *,iostat=io)
if (io/=0) EXIT nlines=nlines+1
end do
close(1)
! Determines the number of rows in that files which is equivalent to the number of particles in the system
! Allocates the arrays using this value
allocate(MLyReal(1:nlines))
allocate(MLxReal(1:nlines))
! allocate(MLzReal(1 :nlines)- - To be included for 3D system files
allocate(MLr(1:nlines))
allocate(Visited(1:nlines))
allocate(LocalShapeCount(1:nlines))
allocate(Edge(1:nlines,1:4))
allocate(EdgeCount(1:nlines))
allocate(TotCont(1:nlines))
allocate(TotShap(1:nlines))
! Sets initial value of those arrays
MLyReal $=0$
MLxReal $=0$
! MLzReal = - - To be included for 3D systems
MLr = 0
Shapes = 0
ShapeLength = 0
Visited = 0
SetPath = 0
Path = 0
LocalShapeCount $=0$
OneCont = 0
TotCont = 1
TotShap = 0
Edge $=0$

EdgeCount = 1
OutCount $=0$
open(1, file = FileName, statu'='o'd')
do $n=1$, nlines
read (1,*) MLxReal(n), MLyReal(n), MLr(n)! Include MLzReal(n), inbetween
the $y$ and radius inputs for 3D systems
end do
close(1)
! Loads in the contacts file for the system
FileName '"
FileName ' 'contac's' // tri178djustt|(FileID(ProgCount))) /' '.c'v'
open(2, file $=$ FileName, statu' $=$ 'o'd')
do

```
        read(2, *,iostat=io)
```

        if (io/=0) EXIT
    nlinesB \(=\) nlines \(B+1\)
    end do
close(2)
allocate(Contacts(1:nlinesB,20))
Contacts = 0
open(2, file = FileName, statu'='o'd')
do $n=1$, nlinesB
read (2,*) Contacts(n,1), Contacts(n,2), Contacts(n,3), Contacts(n,4), Contacts(n,5), Contacts(n,6), Contacts(n,7)
end do
close(2)
do $\mathrm{n}=1$, nlines
if ( $\operatorname{MLr}(\mathrm{n})>$ RadLarge) then
RadLarge $=\operatorname{MLr}(\mathrm{n})$
end if
end do
GridSize $=\left(\left(\left(\text { RadLarge }{ }^{*} 6\right)\right)^{*} 5\right)$
! Determines the largest radius present and the grid size
! Calculates how many particle contacts each particle has
do $n=1$, nlinesB
do while $(\operatorname{Contacts}(\mathrm{n}, \operatorname{Tot} \operatorname{Cont}(\mathrm{n})) /=0)$
$\operatorname{TotCont}(n)=\operatorname{TotCont}(n)+1$
end do
TotCont( n ) $=\operatorname{TotCont}(\mathrm{n}-\mathrm{-}-1$
TotShap $(\mathrm{n})=\operatorname{TotCont}(\mathrm{n})$
end do
do $n=1$, nlines $!$ Loops through each particle if $(\operatorname{TotShap}(\mathrm{n})>0$.and. $\operatorname{MLxReal}(\mathrm{n})==\operatorname{MLr}(\mathrm{n})$ ) then! Checks that the current particle has at least one contact and is touching the leftmost edge of the hox

DepthLoop: do LoopCount $=1,50$
MaxDepth $=250 \quad$ ! Maximum number of recursions
that can occur before automatically unwinding
Visited $=0$
CurCont $=n$

```
y = 1
Depth = 1
Found = .FALSE.
if (LocalShapeCount(n) >= TotShap(n)) then
    exit DepthLoop
    elseif (MIr(n) == 10) then !Confirms the particle is a
large one
                                exit DepthLoop
end if
! Enters the recursion
call
Searching(n,Depth,CurCont,y,ShapeCount,Found,MaxDepth,Path,SetPath,Shapes,ShapeLe ngth,OutCount)
if (Found .eqv. .TRUE.) then ! If a shape has been found, increments the number of shapes
ShapeCount \(=\) ShapeCount +1
end if
OutCount = 0
end do DepthLoop
end if
end do
! Saves the shapes to file
FileName '""
FileName ‘'shap's' // tri179djustt|(FileID(ProgCount))) / ' '.c'v'
open(3, file = FileName, statu'='n'w')
do \(\mathrm{n}=1\), ShapeCount
do \(m=1,250\)
write(','(I3,A1,')', advanc'="o') SetPath(n,m) ' ','
end do
write(3, *’"'
end do
close(3)
! Deallocates the arrays so they can be reallocated with the correct length for the next
deallocate(MLyReal)
deallocate(MLxReal)
! deallocate(MLzReal- - For 3D systems
deallocate(MLr)
deallocate(Visited)
deallocate(LocalShapeCount)
deallocate(Edge)
deallocate(EdgeCount)
deallocate(TotCont)
deallocate(TotShap)
deallocate(Contacts)
CONTINUE
end do
```

end program
RECURSIVE
SUBROUTINE
Searching(n1,Depth1,CurCont1,y1,ShapeCount1,Found,MaxDepth,Path1,SetPath1,Shapes 1,ShapeLength1,OutCount1)
use VarList ! Loads module variables and initalises local recursion variables
integer, intent(inout) :: Depth1
integer, intent(inout) :: CurCont1
integer, intent(inout) :: y1
integer, intent(inout) :: ShapeCount1
integer, intent(in) :: n1
integer, intent(in) :: MaxDepth
integer, dimension (1:250), intent(inout) :: Path1
integer, dimension (1:20000,1:250), intent(inout) :: SetPath1
integer, dimension (1:20000,1:250), intent(inout) :: Shapes1
integer, dimension (1:20000), intent(inout) :: ShapeLength1
integer :: OutCount1
integer :: SavCont
integer :: x
integer :: count
integer :: count2
integer :: count3
integer :: PathCount
integer :: NewCont
logical, intent(inout) :: Found
logical :: LT
integer :: Dupli
integer :: Insi
integer :: InsiCount
character :: t
SavCont = CurCont1
Visited(SavCont) $=1$
$x=1$
$y 1=1$
count $=0$
count2 $=0$
count3 $=0$
PathCount $=0$
Found = .FALSE.
Dupli $=0$
Insi = 0
InsiCount = 0
OutCount1 = OutCount1 + 1
if (Depth1 <= MaxDepth) then ! Confirms the recursion has not gone too deep
llop: do $x=1$, TotShap(CurCont1) ! Loops through the current particle contacts
$\mathrm{LT}=. \mathrm{FALSE}$.
if $(x==1$ ) then
ThisLoop: do count $=1$, Depth1-1 ! Makes the path travelled through ordered in ascending particle numbers
if (CurCont1 < Path1 (count)) then
LT = .TRUE.
exit ThisLoop
end if
end do ThisLoop

```
    if (LT .eqv. .TRUE.) then
        do count2 = Depth1, count+1, -1
            Path1(count2) = Path1(count2-1)
            end do
            Path1(count) = CurCont1
    else
            Path1(Depth1) = CurCont1
            nd if
    end if
    if (MLr(Contacts(CurCont1,x)) == 10) then ! If the connected particle is
small, then it is skipped
                    GO TO 20
    else
    NewCont = Contacts(CurCont1,x)
    if (OutCount1 > 100000) then! Looped for too many times and may
be stuck so exits the outer loop
                        exit llop
    end if
    if (MLxReal(NewCont) == GridSize-MLr(NewCont)) then ! Current
contact is on the right hand edge of the box, in 3D systems, all instances of MLxReal can be
swapped for MLzReal to look for chains crossing in the perpendicular direction
                                    if (ShapeCount1>1) then!Determining if the chain has
already been found
    PathCount = 0
    Dupli = 0
    ShapeLoop: do count = 1, ShapeCount1-1
        PathCount = 0
        do count2 = 1, ShapeLength1(count)
            do count3 = 1, Depth1
                            if (Shapes1(count,count2)
== Path1(count3)) then
                                    PathCount =
PathCount + 1
                    end if
                    end do
        end do
        if (PathCount == ShapeLength1(count)) then
                        Dupli = 1
                        exit ShapeLoop
        end if
        end do ShapeLoop
        end if
                        if (ShapeCount1 == 1 or. Dupli == 0) then ! If unique
chain (or the first one) then it is saved as the recursion unwinds
    LT = .FALSE.
    ThatLoop2: do count = 1, y1-1
                            if (SavCont
Shapes1(ShapeCount1,count)) then
                        LT = .TRUE.
                                exit ThatLoop2
end if
end do ThatLoop2
```


end if

CONTINUE end do llop
end if
Visited(SavCont) $=0 \quad$ ! Unwinding the recursion, marks the particle as no longer visited, and removes the particle from the path
do count = 1, Depth1
if (Path1 (count) $==$ SavCont) then
do count2 = count, Depth1-1
Path1 (count2) $=$ Path1 (count2 +1 )
end do
Path1 (Depth1) $=0$
exit
end if
end do
Depth1 $=$ Depth1-1
END SUBROUTINE Searching

## Appendix 3: 3D System Algorithm

This appendix contains the algorithm used for creating 3D systems.

```
    module allSubs ! Initialises the variables used through all functions
    character, dimension (:.,::), allocatable, public :: RA*4
    integer MolNo, RadLarge, RadSmall, BoxSize, GridSize, Rads, count, SN, Full,
FullCount, OneLegacyCount
    integer MLr, AllocateVal, RoofCount
    real MLxReal, MLyReal, MLzReal
    integer, dimension (:), allocatable, public :: OneLegacyCounterCount
    integer, dimension (:,:), allocatable, public :: Ones
    real, dimension (:,:,:), allocatable, public :: OnesLegacy
    integer, dimension (:,:), allocatable, public :: Contacts
    real, dimension (:,,,:), allocatable, public :: yVal
    integer, dimension (:,:), allocatable, public :: OrderyVal
    integer, dimension (:,:), allocatable, public :: FinalTriCombi
    dimension MLr(10000), Rads(10), MLxReal(10000), MLyReal(10000),
MLzReal(10000)
    logical Hit, FullCheck, FirstCusps, RoofHit
    integer x, y, z, RadT, RestartNo
    integer HMAllo
    end module allSubs
    program packedbed
    use allSubs ! Loads the variables from the module
    ! Initialises local variables
    character t, FileName*15, FileID*3
    integer m, n, o, check, PrintNo, iSeed, ProgCount, PCId
    dimension FileID(200)
    dimension iSeed(50)
    real RX, Dist, DistCheck
    real PartArea, VoidArea, VoidFrac, Pi
    integer count2, TotLength, count3, RunAmo, RunRedo
    logical Cont, Impact
    MLxReal = 0
    MLyReal = 0
    MLzReal = 0
    MLr = 0
    RunAmo = 250
    RunRedo = 0
    FirstCusps = .FALSE.
Dist = 0
DistCheck = 0
RestartNo = 0
PartArea = 0
```

VoidArea $=0$
VoidFrac = 0
$\mathrm{Pi}=3.141596535$
TotLength $=0$
MolNo = 1
OneLegacyCount = 1
FileName = "
Full = 0
check $=0$
FullCount $=0$
Impact $=$. FALSE .
count3 $=0$
count $=0$
count2 $=0$
$t=' y '$
if ( $\mathrm{t}==\mathrm{y}$ ') then
Rads(1) = 10 ! Sets the radius of a particle. Additional radii would be inputted
as Rads(x) = 'Radius'
SN =1! Sets the number of different radii in the system

```
RadLarge =0
RadSmall = 0
do count = 1, SN
    if (RadLarge < Rads(count)) then
                RadLarge = Rads(count)
    end if
    if (RadSmall > Rads(count) .or. RadSmall == 0) then
                                    RadSmall = Rads(count)
    end if
end do
```

RadLarge $=10$
RadSmall = 10
! Calculates the box size based on the largest radius present
BoxSize = (RadLarge*6)
GridSize = (BoxSize*2)
AllocateVal $=(($ BoxSize*3)**2)*2)
HMAllo $=$ GridSize + (2*RadLarge)
! Allocates the arrays
allocate(RA(1:HMAllo, 1:GridSize, 1:GridSize))
allocate(Ones(1:AllocateVal,1:3))
allocate(FinalTriCombi(1:AllocateVal,1:3))
allocate(yVal(1:GridSize,1:GridSize,2))
allocate(OrderyVal(1:GridSize*GridSize,2))
do ProgCount = 1, RunAmo
write(FileID(ProgCount), '(i0)') ProgCount
end do
do ProgCount $=1,50!$ Starts the loop for the number of systems to be created

PCld = ProgCount
! Sets variables intial values
MLxReal $=0$
MLyReal $=0$
MLzReal $=0$
$\mathrm{MLr}=0$
FirstCusps = .FALSE.
Dist $=0$
DistCheck $=0$
RestartNo $=0$
PartArea $=0$
VoidArea $=0$
VoidFrac $=0$
TotLength $=0$
$\mathrm{Pi}=3.141596535$
MolNo = 1
OneLegacyCount =1
FileName = "
Full = 0
check $=0$
FullCount $=0$
RoofCount = 0
Roof $\mathrm{Hit}=$. FALSE.
Impact $=$. FALSE.
count3 $=0$
count $=0$
count2 $=0$
Ones $=0$
OnesLegacy $=0$
OneLegacyCounterCount = 0
$y \mathrm{Val}=0$
$R A=' 0 '$
call random_seed()
do while (count < 1000000)
Impact $=$. FALSE.
to be on the bottom of the box
call random_number(RX)
count2 $=1+$ floor(SN*RX)
RadT = Rads(count2)
call random_number(RX)
count2 $=1+$ floor ((GridSize-(2*RadT) $)^{*}$ RX)
$\mathrm{x}=$ count2+RadT
call random_number(RX)
count2 $=1+$ floor((GridSize-(2*RadT))*RX)
z = count2+RadT
$\mathrm{y}=\mathrm{RadT}$
if $($ MoINo $>1)$ then ! Checks there is already at least one particle in the system
hitloop: do count3 $=1$, MoINo - 1
Dist
((MLxReal(count3)-
$\left.x)^{* *} 2\right)+\left((\text { MLyReal }(\text { count3 })-y)^{* *} 2\right)+\left((\text { MLzReal }(\text { count3 })-z)^{* *} 2\right)$
Dist $=$ sqrt(Dist)
if $($ Dist $<=(($ RadT $)+(M l r(c o u n t 3))))$ then
count = count +1
Impact = .TRUE. exit hitloop
end if
end do hitloop
if (Impact .eqv. .FALSE.) then ! If the particle is not overlapping with any others and is inside the grid, its location is saved

$$
\text { count }=0
$$

MLxReal(MolNo) $=x$
MlyReal(MoINo) $=y$
MlzReal(MoINo) = z
$\mathrm{MLr}(\mathrm{MolNo})=$ RadT
$\mathrm{MoINo}=\mathrm{MolNo}+1$
end if
else
MlxReal(MolNo) $=x$
$\operatorname{MlyReal}(\mathrm{MolNo})=y$
MlzReal(MolNo) $=\mathrm{z}$
MLr(MolNo) = RadT
MoINo $=\mathrm{MolNo}+1$
end if
end do
! This loops through the base line to check that there is nowhere a small particle could fall through to the bottom of the box, and if so, places a particle there
do $m=$ RadSmall, GridSize-RadSmall
do $\mathrm{n}=$ RadSmall, GridSize-RadSmall Impact = .FALSE.
hitloop2: do count3 $=1$, MoINo -1
Dist $=\quad(($ MlxReal $($ count 3$)-$
Dist $=$ sqrt(Dist)
if (Dist $<=(($ RadSmall $)+($ Mlr(count3) $)))$ then count $=$ count +1 Impact = .TRUE. exit hitloop2
end if
end do hitloop2
if (Impact .eqv. .FALSE.) then
count $=0$
$\operatorname{MlxReal}(\mathrm{MolNo})=m$
MlyReal(MoINo) $=$ RadSmall
MlzReal(MoINo) $=\mathrm{n}$
MLr(MolNo) $=$ RadSmall
MoINo $=$ MolNo +1

```
                                    end if
    end do
end do
```

do $\mathrm{n}=1,2500$ ! Loops for each particle being added to the system, using the main function. At the end of each loop, it checks if the box is full and if so, leaves the loop.

Call molpos
if (Full $==1$ ) then
exit
elseif (RoofHit .eqv. .TRUE.) then exit
end if
end do
$t=$ ' $y$ '
if ( $t==$ ' $y$ ' .and. RoofHit .eqv. .TRUE.) then ! Saves the particle
locations to a file
FileName = "
FileName = trim(188nitia(FileID(PCId))) // '.csv’
open(1, file = FileName, status = 'new')
do $\mathrm{y}=1$, MolNo-1
write(1,*) MlxReal(y), ',', MlyReal(y), ',', MlzReal(y),
',' , MLr(y)
end do
close(1)
else
RunAmo = RunAmo +1
RunRedo $=$ RunRedo +1
end if
$t={ }^{\prime} y$ '
if ( $\mathrm{t}==$ ' y ' .and. RoofHit .eqv. .TRUE.) then ! Saves the particle
contacts to a file

$$
\text { allocate(Contacts(1:MolNo, } 1: M o l N o))
$$

Contacts = 0
do $y=1$, MolNo-1
$\mathrm{n}=1$
do $x=1$, MolNo-1 if $(x /=y)$ then

Dist $=(($ MlxReal $(\mathrm{y})$
$\left.\operatorname{MlxReal}(\mathrm{x}))^{* *} 2\right)+\left((\operatorname{MlyReal}(\mathrm{y})-\operatorname{MlyReal}(\mathrm{x}))^{* *} 2\right)+\left((\operatorname{MlzReal}(\mathrm{y})-\operatorname{MlzReal}(\mathrm{x}))^{* *} 2\right)$
Dist = sqrt(Dist)
if $($ Dist $<=(M \operatorname{Lr}(\mathrm{y})+\mathrm{MLr}(\mathrm{x})+0.01))$
then

Contacts( $\mathrm{y}, \mathrm{n}$ ) $=\mathrm{x}$
$\mathrm{n}=\mathrm{n}+1$
end if
if ( $\mathrm{n}>$ TotLength) then
TotLength $=\mathrm{n}$
end if end if
end do
end do
FileName = "
FileName = 'contacts' // trim(188nitia(FileID(PCld))) // '.csv'

$$
\text { open }(3, \text { file }=\text { FileName, status }=\text { 'new') }
$$

do $y=1$, MolNo-1
do $x=1$, TotLength
write(3,'(14,A1,X)', advance='no')
Contacts(y, x), ','
end do write (3, *) "
end do
close(3)
deallocate(Contacts)
end if
end do
FileName = " ! Outputs any files that failed and were not saved
FileName = 'redo.csv'
open(5, file $=$ FileName, status $=$ 'new')
write(5,'(I4,A1,X)', advance='no') RunAmo
write(5,'(I4,A1,X)', advance='no') RunRedo close(5)
end if
end program
subroutine molpos
use allSubs ! Loads the variables from the module
! Sets up the local variables
integer count2, Spot, Height, DoubRad, RowRad, a,b,c, TempX, TempZ, Radln, m, n,
o, Width
real TempY
real RX, MidWay, MidWayZ, Dist, RowRadReal
character t, FileName*15
integer SavOneX, SavOneY, SavOneZ, SavDist, OneCount
integer Zrad, ZdoubRad
integer MlxCor, MlyCor, MlzCor
logical SafeLocFound, CuspFound
integer OldX, OldZ, FinCount
real Grad1a, Grad2a, Grad1b, Grad2b, CurrentY, ZradReal, MidWayReal
integer FinalPartNo
real FinalPartDist
dimension FinalPartNo(5), FinalPartDist(5,2)
real EquA1, EquA2, EquA3, EquB1, EquB2, EquB3, EquC1, EquC2, EquC3, EquD1,
EquD2, EquD3, NewX, NewY, NewZ, NewYa, NewYb
real EquValuesA, EquValuesB, k1, k2, Outputs
dimension EquValuesA(3,3), EquValuesB(3), Outputs(20)
integer EdgeSide
logical EdgeCase, NewXVal, NewZVal
real PartCoords, stochDists, sumDist, dx, stochxnew, newCoords, stochynew
integer ibad
dimension PartCoords(3,3), stochDists(3), newCoords(3), dx(3), stochxnew(3)
real FinalDists, FinalCuspsSaved
dimension FinalCuspsSaved(15000,4)
dimension FinalDists(3), CuspHighList(16,3)
real CuspHighList, FurthDist
integer CuspLowCount, CuspHighCount, CuspLowMoveTo
logical OuterLayer
real TriCheckA, TriCheckB, TriCheckC
logical TriCheckInside
real LowYVal
integer LowYLoc
dimension LowYLoc(2)
real Sempi, SetTri, TriA, TriB, TriC, SempiA, SempiB, SempiC
real DistAN, DistBN, DistCN, DistAB, DistBC, DistCA
real EdgeLowVal
integer EdgeLowA, EdgeLowB, bSide1, bSide2
logical InitialCusp
integer TriCheckCount, TriCheckNo, TriCount, TriCombi, TriAttempt, ReTriAttempt
logical FirstTri, FirstEdge
real TriCoords, OverDist
integer OverDistNo
dimension TriCheckNo(10000), TriCombi(100001,3), TriCombi2(10000000,3),
TriCoords(3,3)
dimension EdgeCombi(1000000)
integer EdgeCount, EdgeCombi, EdgeAttempt
integer SideCheckCount, SideCheckNo, SideCount, SideCombi, SideAttempt
integer FinalTriCount
logical FirstSide
real SideCoords
dimension SideCheckNo(10000), SideCombi(100001,3), SideCoords(3,3)
integer OverlapCount, HMSize
real DistCheck1, DistCheck2, DistCheck3, DistCheck1Val, DistCheck2Val, DistCheck3Val

FinalCuspsSaved $=0$
CONTINUE
RestartNo $=$ RestartNo +1
! Setting initial values of variables
Hit = .FALSE.
EdgeSide $=0$
HMSize $=0$
OverDist = 0
OverDistNo $=0$
OverlapCount $=0$

DistCheck1 = 0
DistCheck2 $=0$
DistCheck3 = 0
DistCheck1 Val $=0$
DistCheck2Val $=0$
DistCheck3Val $=0$
CuspLowCount $=0$
CuspHighCount $=0$
FurthDist = 0
CuspLowMoveTo = 0

```
TriCheckNo \(=0\)
TriCheckCount = 1
TriCount = 1
EdgeCount = 1
TriCombi \(=0\)
TriCombi2 \(=0\)
EdgeCombi \(=0\)
TriCoords \(=0\)
TriAttempt \(=0\)
EdgeAttempt \(=0\)
FirstTri = .TRUE.
FirstEdge = .TRUE.
ReTriAttempt \(=0\)
FinalTriCombi \(=0\)
FinalTriCount = 1
```

SideCheckNo $=0$
SideCheckCount = 1
SideCount = 1
SideCombi $=0$
SideCoords $=0$
SideAttempt $=0$
FirstSide = .TRUE.

Sempi $=0$
SetTri $=0$
TriA $=0$
TriB $=0$
TriC $=0$
SempiA = 0
SempiB $=0$
SempiC $=0$
DistAN = 0
DistBN $=0$
DistCN $=0$
DistAB $=0$
DistBC $=0$
DistCA $=0$
LowYLoc $=0$
LowYVal $=0$
FinalDists $=0$
PartCoords $=0$
stochDists $=0$
sumDist $=0$
$\mathrm{dx}=0$
stochxnew $=0$
newCoords $=0$
stochynew = 0
NewXVal = .FALSE.
NewZVal = .FALSE.

```
EquValuesA \(=0\)
EquValuesB \(=0\)
k1 \(=0\)
\(\mathrm{k} 2=0\)
Outputs \(=0\)
TRP1Swap = 0
TRP2Swap = 0
ZradReal \(=0\)
MidWayReal \(=0\)
```

FinCount $=0$
CuspFound = .FALSE.
Current $\mathrm{Y}=0$
OldX = 999
OldZ = 999
SavDist $=0$
SavOneX = 0
SavOneY = 0
MidWay = 0
MidWayZ = 0
Grad1a $=0$
Grad2a $=0$
Grad1b $=0$
Grad2b $=0$
FinalPartNo = 999999
FinalPartDist $=999999$
EquA1 $=0$
EquA2 $=0$
EquA3 $=0$
EquB1 $=0$
EquB2 $=0$
EquB3 $=0$
EquC1 $=0$
EquC2 $=0$
EquC3 $=0$
EquD1 $=0$
EquD2 $=0$
EquD3 $=0$
NewX $=0$
New $Y=0$
NewZ $=0$
NewYa $=0$
NewYb = 0

RowRadReal $=0$

EdgeCase = .FALSE.
! Randomly chooses which radius will be used for this particle call random_number(RX)
count2 $=1+$ floor (2*RX)
if (count2 == 2) then
RadT = RadLarge
else
RadT = RadSmall
end if
wloop: do while (Hit .eqv. .FALSE.)
! Randomly chooses the $x$ value
call random_number(RX)
Spot $=1+$ floor $\left(\left(\text { GridSize- }\left(2^{*} \operatorname{Rad} T\right)\right)^{*} R X\right)$
x = Spot+RadT
call random_number(RX)
Spot $=1+$ floor $\left(\left(\text { GridSize- }\left(2^{*} \operatorname{Rad} T\right)\right)^{*} R X\right)$
z = Spot+RadT
do $y=$ GridSize, RadT, $-1 \quad$ ! Loops from the top of the box, and sends to the function to determine impact
call PointSafe
! If the box is full or an impact has I, the loop is exited
if (Full $==1$ ) then
exit wloop
end if
if (FullCheck .eqv. .TRUE.) then
RoofHit = .TRUE.
GO TO 10
end if
if (Hit .eqv. .TRUE.) then exit wloop
end if
end do
end do wloop
if (Hit .eqv. .TRUE. .and. Full /= 1) then
if (MolNo > 1) then
'A = '0'
! Sets up the variables to be used for particle placement
Ones = 0
OneCount = 1
do count $=1,-$ MoINo -1 ! Loops through the particles for contour plot

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MLxcor $=$ MLxReal(count)
MLycor = MLyReal(count)
MLzcor = MLzReal(count) ! Takes the radius, $x, y$ and $z$
coordinates of the current particle in the loop
Radln $=$ Mlr(count)
DoubRad $=($ RadIn + RadT $)+1$
ZDoubRad = (Radln + RadT $)+1$
do Width = -ZDoubRad, 0
MidWayZ = ZDoub-ad**2 - Width**2
ZRad = abs(sqrt(MidwayZ))
ZRadReal = abs(sqrt(MidwayZ))
do Height =-ZRad, $0 \quad$ ! Draws the particle onto the contour"p"ot, "-"s marking blocked loca"i"ns, "1"s being valid spots

Midway = Z-ad**2 - Height**2
RowRad = abs(sqrt(MidWay))
MidWayReal = ZRadR-al**2 - Height**2
RowRadReal = abs(sqrt(MidWayReal))
do count2 = -RowRad+1,RowRad-1
if (MLyCor+count2<=HMAllo .and.
MLyCor+count2>=RadT) then
if (MLxCor+Height>=RadT
.and. MLzCor+Width >= RadT) then
RA(MLyCor+count2, MLxCor+Height, MLzCor+Wit't) = '-' end if
if (MLxCor-
Height<=GridSize-RadT .and. MLzCor+Width >= RadT) then
RA(MLyCor+count2, MLxCor-Height, MLzCor+Wi't') = '-'
end if
if (MLxCor+Height>=RadT
.and. MLzCor-Width <=GridSize-RadT) then
RA(MLyCor+count2, MLxCor+Height, MLzCor-Wi't') = '-'
end if
if (MLxCor-
Height<=GridSize-RadT .and. MLzCor-Width <=GridSize-RadT) then
RA(MLyCor+count2, MLxCor-Height, MLzCor-Witt') = '-'
end if
end if
end do
do count2 $=-$ RowRad,RowRad ! Adds the valid spots for the resting particle to be placed MLyCor+count2<=HMAllo) then
if (MLyCor+count2>=RadT .and. .and. MLzCor+Width >= RadT) then
if (MLxCor+Height>=RadT
if
(RA(MLyCor+count2, MLxCor+Height, MLzCor+Wid'h' /= '-') then

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RA(MLyCor+count2, MLxCor+Height, MLzCor+Wi't') = '1'
end if
end if
if
(MLxCor-
Height<=GridSize-RadT .and. MLzCor+Width >= RadT) then (RA(MLyCor+count2, MLxCor-Height, MLzCor+Wid'h' /= '-') then RA(MLyCor+count2, MLxCor-Height, MLzCor+Wi't') = '1'
if
end if
end if
if (MLxCor+Height>=RadT
if
(RA(MLyCor+count2, MLxCor+Height, MLzCor-Wid'h' /= '-') then
RA(MLyCor+count2, MLxCor+Height, MLzCor-Wit') = '1'
end if
end if
if
Height<=GridSize-RadT .and. MLzCor-Width <= GridSize-RadT) then (RA(MLyCor+count2, MLxCor-Height, MLzCor-Wid'h' /= '-') then

RA(MLyCor+count2, MLxCor-Height, MLzCor-Wi't') = '1'
$\qquad$
if
(MLxCor-
end if
end if end if end do
if (MLyCor+RowRadReal>=RadT .and.
MLyCor+RowRadReal<=HMAllo) then MLzCor+Width >= RadT) then if (MLxCor+Height>=RadT .and.
if (RA(MLyCor+count2,

MLxCor+Height, MLzCor+Wid'h' /= '-') then
if
(MLyCor+RowRadReal >yVal(MLxCor+Height, MLzCor+Width,1)) then
$y \operatorname{Val}(M L x C o r+$ Height, MLzCor+Width,1) = MLyCor+RowRadReal
$y \mathrm{Val}($ MLxCor+Height, MLzCor+Width,2) = count
end if
end if end if if (MLxCor-Height<=GridSize-RadT
.and. MLzCor+Width >= RadT) then
MLxCor-Height, MLzCor+Wid'h' /= '-') then
(MLyCor+RowRadReal >yVal(MLxCor-Height, MLzCor+Width,1)) then $\mathrm{yVal}(\mathrm{MLxCor}-\mathrm{Height}, \mathrm{MLzCor}+$ Width,1) $=$ MLyCor+RowRadReal
$\mathrm{yVal}(\mathrm{MLxCor}-\mathrm{Height}, \mathrm{MLzCor}+$ Width,2 $)=$ count
end if

```
                                    end if
                    end if
                                    if (MLxCor+Height>=RadT .and.
MLzCor-Width <= GridSize-RadT) then
                            if (RA(MLyCor+count2,
MLxCor+Height, MLzCor-Wid'h'/= '-') then
```

```
(MLyCor+RowRadReal > yVal(MLxCor+Height, MLzCor-Width,1)) then
yVal(MLxCor+Height, MLzCor-Width,1) \(=\) MLyCor+RowRadReal
yVal(MLxCor+Height, MLzCor-Width,2) = count
end if
end if
end if
if (MLxCor-Height<=GridSize-RadT
.and. MLzCor-Width <= GridSize-RadT) then
if (RA(MLyCor+count2,
MLxCor-Height, MLzCor-Wid'h' /= '-') then
(MLyCor+RowRadReal > yVal(MLxCor-Height, MLzCor-Width,1)) then
yVal(MLxCor-Height, MLzCor-Width,1) = MLyCor+RowRadReal
yVal(MLxCor-Height, MLzCor-Width,2) \(=\) count
end if
end if
end if
end if end do
end do
end do
do \(\mathrm{a}=1\), GridSize \(!\) Finds the valid points and saves them to an array do \(b=1\), HMAllo do \(c=1\), GridSize if (RA(b, \(a^{\prime} c^{\prime}==\) ' 1 ') then
Ones(OneCount, 1) = b
Ones(OneCount, 2) \(=\mathrm{a}\)
Ones(OneCount, 3) = c
OneCount \(=\) OneCount +1
end if
end do
end do
end do
if (FirstCusps .eqv. .FALSE.) then FirstCusps = .TRUE.
\(\mathrm{c}=1\)
do a = RadT, GridSize-RadT
do \(\mathrm{b}=\) RadT, GridSize-RadT
if \((y \operatorname{Val}(a+1, b, 1)>y \operatorname{Val}(a, b, 1)\).and. \(y \operatorname{Val}(a-\)
\(1, b, 1)>y \operatorname{Val}(a, b, 1))\) then
\(y \operatorname{Val}(a, b-1,1)>y \operatorname{Val}(a, b, 1))\) then
if \((y \operatorname{Val}(a, b+1,1)>y \operatorname{Val}(a, b, 1)\).and.
if \(\quad(\mathrm{yVal}(\mathrm{a}+1, \mathrm{~b}+1,1)>\)
\(y \operatorname{Val}(a, b, 1)\).and. \(y \operatorname{Val}(a-1, b-1,1)>y \operatorname{Val}(a, b, 1))\) then
```

$y \operatorname{Val}(a, b, 1)$.and. $y \operatorname{Val}(a+1, b-1,1)>y \operatorname{Val}(a, b, 1))$ then
FinalCuspsSaved(c,1) =a
FinalCuspsSaved(c,2) $=\mathrm{b}$
FinalCuspsSaved(c,3) $=y$ Val(a,b,1)
FinalCuspsSaved $(c, 4)=y \operatorname{Val}(a, b, 2)$
$c=c+1$
end if
end if end if end if
end do
end do
end if
do $\mathrm{a}=1$, On-Count -1 ! Finds the closest of these points to the impact location and moves the particle to it

```
TempX = Ones(a,2)
    TempY = Ones \((\mathrm{a}, 1)\)
    TempZ = Ones(a,3)
    if (TempY <= \(y+1\) ) then
                            Dist \(=\quad\left((x-\text { TempX })^{* *} 2\right)+\left((y-\text { TempY })^{* *} 2\right)+((z-\)
```

TempZ)**2)
Dist $=$ sqrt(Dist)
if (Dist < SavDist .or. SavDist $==0$ ) then
SavDist = Dist
SavOneX = Ones(a,2)
SavOneY = Ones(a,1)
SavOneZ = Ones(a,3)
end if
end if
end do
TempX = SavOneX
TempY = SavOneY
TempZ = SavOneZ
if (TempX == 0 .and. TempY == 0 .and. TempZ == 0 ) then GO TO 10
end if
SafeLocFound = .FALSE .
FinCount $=0$
$\mathrm{LR}=0$
step $=1$
FindLoop: do while (SafeLocFound .eqv. .FALSE.) ! Rolling algorithm, moves in the direction with the deepest slope until it is fully surrounded by higher points CurrentY = yVal(TempX,TempZ,1)
if (TempX < RadT .or. TempZ < RadT .or. TempX > GridSize-
RadT .or. TempZ > GridSize-RadT) then



if $(y \operatorname{Val}($ TempX,TempZ $+1,1)>$ CurrentY .and. yVal(TempX,TempZ-1,1) > CurrentY) then if $(\mathrm{yVal}($ TempX $+1, \mathrm{TempZ}+1,1)>$ Current $Y$ .and. $\mathrm{yVal}($ TempX-1,TempZ-1,1) $>$ CurrentY) then
if $(\mathrm{yVal}($ TempX-1,TempZ+1,1) $>$ CurrentY .and. yVal(TempX+1,TempZ-1,1) > CurrentY) then

## CuspHighCount = 1

 CuspLowCount = 1 do $a=-3,3$ do $b=-3,3$OuterLayer
$=$. FALSE.
(abs(a)+abs(b) >=3) then
OuterLayer $=$. TRUE.
elseif
$(a b s(a)+a b s(b)==2)$ then
( $\mathrm{a}==0$.or. $\mathrm{b}==0$ ) then
OuterLayer = .TRUE.
end if
if
end if
if

(OuterLayer .eqv. .TRUE.) then
$(y \operatorname{Val}($ TempX $+\mathrm{a}, \mathrm{TempZ}+\mathrm{b}, 1)>=$ CurrentY .or. $\mathrm{yVal}($ TempX $+\mathrm{a}, \mathrm{TempZ}+\mathrm{b}, 1)==0)$ then
CuspHighCount $=$ CuspHighCount +1
elseif (TempX+a>GridSize-RadT.or.TempX+a<RadT.or.TempZ+b>GridSizeRadT.or.TempZ+b<RadT) then

CuspHighCount $=$ CuspHighCount +1
elseif $(\mathrm{yVal}($ TempX +a, TempZ $+\mathrm{b}, 1)==0)$ then
CuspHighCount $=$ CuspHighCount +1
elseif ( $\mathrm{yVal}($ TempX+a,TempZ+b,1) < CurrentY) then
if (TempX $+\mathrm{a}<=$ GridSize-RadT.and.TempX $+\mathrm{a}>=$ RadT.and.TempZ+b<=GridSizeRadT.and.TempZ+b>=RadT) then

CuspHighList(CuspLowCount,1) $=$ TempX+a
CuspHighList(CuspLowCount,2) $=$ TempZ+b
CuspHighList(CuspLowCount,3) $=\mathrm{yVal}($ TempX +a, TempZ $+\mathrm{b}, 1)$
CuspLowCount $=$ CuspLowCount +1
end if
end if
end if

> end do
> end do
> if (CuspHighCount $==41$ )
then
.TRUE.
CuspFound =
SafeLocFound =
.TRUE.
do $\mathrm{a}=1$,
CuspLowCount-1
((CuspHighList(a,1)-OldX)**2)+((CuspHighList(a,2)-OldZ)**2)
sqrt(Dist)
Dist =

Dist =
< Dist) then
if (FurthDist

```

> FurthDist = Dist
CuspLowMoveTo = a
CuspHighList(CuspLowMoveTo,1)
                                    end if
                                    end if
                end if
        end if
    end if
    if (CuspFound .eqv. .TRUE.) then
                        SafeLocFound = .TRUE.
        else
        LowYLoc = 0
        Low YVal = 0
        do \(\mathrm{a}=-1,1\)
                            do \(b=-1,1\)
                                    if \((\mathrm{yVal}(\) TempX +a, TempZ+b,1) \(<=\)
CurrentY) then

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FinalPartDist(3,1) \(=\) FinalPartDist(2,1)
FinalPartDist \((3,2)=\) FinalPartDist \((2,2)\)
FinalPartNo(2) = FinalPartNo(1)
FinalPartDist(2,1) = FinalPartDist(1,1)
FinalPartDist(2,2) \(=\) FinalPartDist \((1,2)\)
FinalPartNo(1) = a
FinalPartDist(1,1) = Dist
FinalPartDist(1,2) = Dist + RadT + MLr(a)
elseif (Dist <= FinalPartDist(2,1)) then
FinalPartNo(5) = FinalPartNo(4)
FinalPartDist \((5,1)=\) FinalPartDist \((4,1)\)
FinalPartDist(5,2) \(=\) FinalPartDist(4,2)
FinalPartNo(4) = FinalPartNo(3)
FinalPartDist \((4,1)=\) FinalPartDist \((3,1)\)
FinalPartDist \((4,2)=\) FinalPartDist \((3,2)\)
FinalPartNo(3) = FinalPartNo(2)
FinalPartDist \((3,1)=\) FinalPartDist \((2,1)\)
FinalPartDist \((3,2)=\) FinalPartDist \((2,2)\)
FinalPartNo(2) = a
FinalPartDist(2,1) = Dist
FinalPartDist(2,2) = Dist + RadT + MLr(a)
elseif (Dist <= FinalPartDist( 3,1 )) then
FinalPartNo(5) = FinalPartNo(4)
FinalPartDist(5,1) = FinalPartDist(4,1)
FinalPartDist \((5,2)=\) FinalPartDist \((4,2)\)
FinalPartNo(4) = FinalPartNo(3)
FinalPartDist(4,1) = FinalPartDist(3,1)
FinalPartDist(4,2) \(=\) FinalPartDist(3,2)
FinalPartNo(3) = a
FinalPartDist(3,1) = Dist
FinalPartDist(3,2) = Dist + RadT + MLr(a)
elseif (Dist <= FinalPartDist(4,1)) then
FinalPartNo(5) = FinalPartNo(4)
FinalPartDist(5,1) = FinalPartDist(4,1)
FinalPartDist(5,2) = FinalPartDist(4,2)
FinalPartNo(4) = a
FinalPartDist \((4,1)=\) Dist
FinalPartDist(4,2) = Dist + RadT + MLr(a)
elseif (Dist <= FinalPartDist( 5,1 )) then
FinalPartNo(5) = a
FinalPartDist \((5,1)=\) Dist
FinalPartDist \((5,2)=\) Dist + RadT + MLr \((a)\)
end if
end if
end do

CONTINUE
if
(FinalPartNo(1)>MolNo.or.FinalPartNo(2)>MolNo.or.FinalPartNo(3)>MoINo.or.FinalPartNo(4) \(>\) MoINo.or.FinalPartNo(5)>MoINo) then
```

FullCount = FullCount +1
GO TO 40

```
end if
PartCoords(1,1) = MLxReal(FinalPartNo(1))
PartCoords(1,2) \(=\) MLyReal(FinalPartNo(1))

PartCoords(1,3) \(=\) MLzReal(FinalPartNo(1))
PartCoords(2,1) = MLxReal(FinalPartNo(2))
PartCoords(2,2) = MLyReal(FinalPartNo(2))
PartCoords(2,3) \(=\) MLzReal(FinalPartNo(2))
PartCoords(3,1) = MLxReal(FinalPartNo(3))
PartCoords(3,2) \(=\) MLyReal(FinalPartNo(3))
PartCoords(3,3) \(=\) MLzReal(FinalPartNo(3))
EquA1 \(=2 *\) MLxReal(FinalPart-o(1)) \(-2^{*}\) MLxReal(FinalPartNo(2))
EquA2 \(=2^{*}\) MLxReal(FinalPart-o(2)) \(-2^{*}\) MLxReal(FinalPartNo(3))
EquA3 \(=2 *\) MLxReal(FinalPart-o(3)) \(-2^{*}\) MLxReal(FinalPartNo(1))
EquB1 \(=2 *\) MLyReal(FinalPart-o(1)) \(-2^{*}\) MLyReal(FinalPartNo(2))
EquB2 \(=2^{*}\) MLyReal(FinalPart-o(2)) \(-2^{*}\) MLyReal(FinalPartNo(3))
EquB3 \(=2 *\) MLyReal(FinalPart-o(3)) \(-2^{*}\) MLyReal(FinalPartNo(1))
EquC1 \(=\) 2*MLzReal(FinalPart-o(1)) \(^{*}\) 2*MLzReal(FinalPartNo(2))
EquC2 \(=\) 2*MLzReal \(^{*}\) (FinalPart-o(2)) - 2*MLzReal(FinalPartNo(3)) \(^{*}\) (Final
EquC3 \(=2 *\) MLzReal(FinalPart-o(3)) \(-2^{*}\) MLzReal(FinalPartNo(1))
Equd1 \(=\quad\left(\right.\) MLzReal \(\left(F i n a l P a r t N o(1-)^{* *} 2\right)\)
(MLzReal(FinalPartNo(2))**2) + (MLyReal(FinalPartNo(1))**2)
EquD1 \(=-\) Equd1 \(\quad\) (MLyReal(FinalPartNo(2))**2) + (MLxReal(FinalPartNo(1-)**2) - (MLxReal(FinalPartNo(2))**2)

EquD1 \(=-E q u D 1 \quad-\quad\left((M L r(\text { FinalPartNo(1) })+\text { RadT })^{* *} 2\right) \quad+\) ((MLr(FinalPartNo(2))+RadT)**2)

Equd2 \(\quad=\quad(M L z R e a l(F i n a l P a r t N o(2-) * * 2)\)
(MLzReal(FinalPartNo(3))**2) + (MLyReal(FinalPartNo(2))**2)
EquD2 \(=-\) Equd2 \(\quad\) (MLyReal(FinalPartNo(3))**2) + (MLxReal(FinalPartNo(2-)**2) - (MLxReal(FinalPartNo(3))**2)

EquD2 \(=-E q u D 2 \quad-\quad\left((M L r(F i n a l P a r t N o(2))+\text { RadT })^{* *} 2\right) \quad+\) ((MLr(FinalPartNo(3))+RadT)**2)

Equd3 \(=\quad\left(\mathrm{MLzReal}\left(F i n a l P a r t N o(3-)^{* *} 2\right)\right.\)
(MLzReal(FinalPartNo(1))**2) + (MLyReal(FinalPartNo(3))**2)
EquD3 =-Equd3 - (MLyReal(FinalPartNo(1))**2) + (MLxReal(FinalPartNo(3-)**2) - (MLxReal(FinalPartNo(1))**2)

EquD3 =-EquD3 - ((MLr(FinalPartNo(3))+RadT) \(\left.)^{* *} 2\right) \quad+\) ((MLr(FinalPartNo(1))+RadT)**2)
if (CuspFound .eqv. .TRUE. .and. EdgeCase .eqv. .FALSE.) then ! If in a cusp and not on an edge
\[
\begin{aligned}
& \text { EquValuesA }(1,1)=\text { EquA1 } \\
& \text { EquValuesA }(1,2)=\text { EquB1 } \\
& \text { EquValuesA }(1,3)=\text { EquC1 } \\
& \text { EquValuesB }(1)=\text { EquD1 } \\
& \text { EquValuesA }(2,1)=\text { EquA2 } \\
& \text { EquValuesA }(2,2)=\text { EquB2 } \\
& \text { EquValuesA }(2,3)=\text { EquC2 } \\
& \text { EquValuesB }(2)=\text { EquD2 } \\
& \text { EquValuesA( } 3,1)=\text { EquA3 }
\end{aligned}
\]
```

EquValuesA(3,2) = EquB3
EquValuesA(3,3) = EquC3
EquValuesB(3) = EquD3
stochDists(1) = FinalPartDist(1,2)
stochDists(2) = FinalPartDist(2,2)
stochDists(3) = FinalPartDist(3,2)
sumDist = stochDists(1) + stochDists(2) + stochDists(3) !

```

Starts stochastic optimisation to find the resting position
```

newCoords(1) = TempX
newCoords(2) = TempY
newCoords(3) = TempZ
dx(1) = 10 * RadLarge
dx(2) = 10 * RadLarge
dx(3) = 10 * RadLarge
do a = 1,10
do b=1,3
dx(b) = dx(b)/10
end do
do c = 1,500
do b = 1, 3
call random_number(RX)
stochxnew(b) = newCoords(b) +

```
\(d x(b)\) * \(\left(2^{*} R X-1\right)\)
end do
ibad \(=0\)
do \(b=1,3\)
                            stochDists(b) = ((PartCoords(b,1)-
stochxnew(1))**2)+((PartCoords(b,2)-stochxnew(2))**2)+((PartCoords(b,3)-
stochxnew(3))**2)
- RadT - MLr(FinalPartNo(b))
stochDists(3)
then
stochxnew(b)
```

                            stochDists(b) = sqrt(stochDis-s(b))
                            stochynew = stochDists(1) + stochDists(2) +
                                    if (stochynew < sumDist .and. ibad == 0)
                                    do b=1,3
                                    newCoords(b) =
                                    if (stochDists(b) < 0) then
                                    ibad = 1
                    end if
                            end do
                                    end do
                                    sumDist = stochynew
                                    end if
    end do
    end do

```
NewX = newCoords(1)
NewY = newCoords(2)
NewZ = newCoords(3)
do \(\mathrm{a}=1\), MolNo-1 ! Confirms that the particle is not overlapping with any others in its new position

Dist \(=((M L x R e a l(a)-N e w X) * * 2)+((\) MLyReal \((a)-\) NewY \(\left.)^{* *} 2\right)+\left(\left(\right.\right.\) MLzReal(a)-NewZ) \(\left.{ }^{* *} 2\right)\)

Dist \(=\) sqrt(Dist)
if (Dist < MLr(a)+RadT) then
OverDist = 0
OverlapCount \(=\) OverlapCount +1 if (OverlapCount > 2500) then GO TO 50
end if
do \(b=1,3\)
Dist \(=\quad((M L x R e a l(a)-\)
PartCoords(b,1))**2)+((MLyReal(a)-PartCoords(b,2))**2)+((MLzReal(a)-PartCoords(b,3))**2) Dist = sqrt(Dist)
if (Dist < OverDist .or. OverDist ==
0 ) then
OverDist \(=\) Dist
OverDistNo = b
end if
end do
FinalPartNo(OverDistNo) =a
FullCount \(=\) FullCount +1
if (OverDist \(==0\) ) then GO TO 50
else GO TO 60
end if
end if
end do
DistAB \(=\quad\) ((PartCoords(1,1)-
PartCoords(2,1))**2)+((PartCoords(1,3)-PartCoords(2,3))**2)
DistAB \(=\) sqrt(DistAB)
DistBC =
((PartCoords(2,1)-
PartCoords(3,1))**2)+((PartCoords(2,3)-PartCoords(3,3))**2)
DistBC \(=\operatorname{sqrt}(\) DistBC \()\)
DistCA =
((PartCoords(3,1)-
PartCoords(1,1))**2)+((PartCoords(3,3)-PartCoords(1,3))**2)
DistCA \(=\operatorname{sqrt}(\) DistCA \()\)
DistAN \(=((\) PartCoords(1,1)-NewX)**2)+((PartCoords(1,3)-
NewZ)**2)
DistAN \(=\operatorname{sqrt}(\) DistAN \()\)
DistBN \(=((\) PartCoords(2,1)-NewX)**2)+((PartCoords(2,3)-
NewZ)**2)
DistBN = sqrt(DistBN)
DistCN \(=\left((\text { PartCoords }(3,1)-\text { New } X)^{* *} 2\right)+((\) PartCoords \((3,3)-\)
NewZ)**2)
DistCN \(=\operatorname{sqrt}(\) DistCN \()\)
Sempi \(=(\) DistAB + DistBC + DistCA \() / 2\)
SetTri \(=\) Sempi * - Sempi - DistAB) * -Sempi - DistBC) * -
Sempi - DistCA)
SetTri \(=\operatorname{sqrt}(\) SetTri)
```

SempiA $=($ DistAB + DistAN + DistBN $) / 2$
TriA $=$ SempiA * $(- \text { empiA }- \text { DistAB })^{*}(-e m p i A-D i s t A N) ~ * ~(-$

```
empiA - DistBN)
TriA \(=\operatorname{sqrt}(\) TriA \()\)
SempiB \(=(\) DistBC + DistBN + DistCN \() / 2\)
TriB \(=\) SempiB * (-empiB - DistBC) * (-empiB - DistBN) * (-
empiB - DistCN)
TriB \(=\operatorname{sqrt}(\) TriB \()\)
SempiC \(=(\) DistCA + DistCN + DistAN \() / 2\)
TriC = SempiC * (-empiC - DistCA) * (-empiC - DistCN) * (-
empiC - DistAN)
TriC \(=\operatorname{sqrt}(\) TriC \()\)
if (TriA + TriB + TriC > SetTri + 2.5) then! Confirms the new
particle location is correctly resting on the three particles below it

CONTINUE
OverlapCount \(=0\)
if (FirstTri .eqv. .TRUE.) then do \(\mathrm{a}=1\), MolNo-1 Dist \(\quad=\quad((\) MLxReal \((\mathrm{a})-\)
NewX)**2)+((MLzReal(a)-NewZ)**2) Dist \(=\) sqrt(Dist) if (Dist \(<\) RadT \(+\quad\) MLr(a) \(\quad+\)
(RadT*8) .and. NewY-MLyReal(a) < RadT \(\left.+\operatorname{MLr}(\mathrm{a})+\left(\operatorname{RadT}^{*} 6\right)\right)\) then
TriCheckNo(TriCheckCount) = a

TriCheckCount + 1

TriCheckCount-1, 1, -1
then
(TriCount \(<=100000\) ) then
```

        TriCombi(TriCount,1) = TriCheckNo(a)
        TriCombi(TriCount,2) = TriCheckNo(b)
        TriCombi(TriCount,3) = TrilckNo(c)
        TriCount = TriCount + 1
        else
        exit aLoop
    ```
end if


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FinalDists(a) \(\quad=\quad((\) PartCoords \((a, 1)-\)
NewX)**2)+((PartCoords(a,2)-NewY)**2)+((PartCoords(a,3)-NewZ)*2 \()\)
FinalDists(a) = sqrt(FinalDists(a))
if (FinalDists(a) > RadT+MLr(FinalPartNo(a))+1)
then
FullCount \(=\) FullCount +1
GO TO 50
end if
end do
if (NewX < RadT .or. NewY < RadT .or. NewZ < RadT) then
FullCount = FullCount + 1
if (TempX >= GridSize-RadT-RadT .or. TempX <= RadT+RadT .or. TempZ >= GridSize-RadT-RadT .or. TempZ <= RadT+RadT) then
if (TempX <= RadT+RadT .and. TempZ <= RadT+RadT) then

EdgeSide \(=1\)
elseif (TempX >= GridSize-RadT-RadT
.and. TempZ >= GridSize-RadT-RadT) then
EdgeSide \(=4\)
elseif (TempX >= GridSize-RadT-RadT
.and. TempZ <= RadT+RadT) then
>= GridSize-RadT-RadT) then
EdgeSide \(=2\)
elseif (TempX <= RadT+RadT .and. TempZ
EdgeSide \(=3\)
elseif (TempX <= RadT+RadT) then
EdgeSide = 5
elseif (TempX >= GridSize-RadT-RadT)
then
EdgeSide \(=8\)
elseif (TempZ <= RadT+RadT) then
EdgeSide \(=6\)
elseif (TempZ >= GridSize-RadT-RadT)
then
EdgeSide \(=7\)
end if
EdgeCase = .TRUE.
GO TO 25
end if
GO TO 50
elseif (NewX > GridSize-RadT .or. New \(Y\) > GridSize-RadT
.or. NewZ > GridSize-RadT) then
FullCount = FullCount +1
if (TempX >= GridSize-RadT-RadT .or. TempX <=
RadT+RadT .or. TempZ >= GridSize-RadT-RadT .or. TempZ <= RadT+RadT) then
if (TempX <= RadT+RadT .and. TempZ <=
RadT+RadT) then
EdgeSide \(=1\)
elseif (TempX >= GridSize-RadT-RadT
.and. TempZ >= GridSize-RadT-RadT) then
.and. TempZ <= RadT+RadT) then
EdgeSide \(=4\)
elseif (TempX >= GridSize-RadT-RadT
EdgeSide \(=2\)
elseif (TempX <= RadT+RadT .and. TempZ
>= GridSize-RadT-RadT) then
```

    EdgeSide = 3
    elseif (TempX <= RadT+RadT) then
            EdgeSide = 5
                            elseif (TempX >= GridSize-RadT-RadT)
    then
then
seif (EdgeCase .eqv. .TRUE.) then ! Else if the particle has come to
rest upon an edge
if (EdgeSide < 5) then ! If the particle is resting in a corner, so needs a single particle contact
if (EdgeSide $==1$ ) then
NewX = RadT
NewZ = RadT
elseif (EdgeSide ==2) then
NewX = GridSize-RadT
NewZ = RadT
elseif (EdgeSide ==3) then
NewX = RadT
NewZ = GridSize-RadT
elseif (EdgeSide == 4) then
NewX = GridSize-RadT
NewZ = GridSize-RadT
end if
Dist $=$ RadT + MLr(FinalPartNo(1))
new
(MLxReal(FinalPartNo(1))**2)+(2*MLxReal(FinalPartNo(1))*NewX)(MLzReal(FinalPartNo(1))**2)
NewY
NewY+(2*MLzReal(FinalPartNo(1))*NewZ)+(Dist**2)-(NewX**2)-(NewZ**2) New $Y=\operatorname{sqrt}($ New $Y$ )
if (NewY /= NewY) then if (FirstEdge .eqv. .TRUE.) then
do $\mathrm{a}=1$, MolNo-1
dist $=((\operatorname{MLxReal}(\mathrm{a})-$
Dist $=$ sqrt(Dist)

```
(RadT*8)) then

> EdgeCombi(EdgeCount) = a

EdgeCount + 1

EdgeCombi(EdgeCount-EdgeAttempt)
EdgeCount =
end if
end do
end if

FirstEdge = .FALSE.
if (EdgeAttempt <= EdgeCount-1) then
FinalPartNo(1)
=

EdgeAttempt = EdgeAttempt + 1 GO TO 60
end if
FullCount \(=\) FullCount +1
GO TO 40
end if
-f (tempY - (MLyReal(FinalPartNo(1)) + NewY- <
tempY - (MLyReal(FinalP-rtNo(1)) - NewY)) then
NewY \(=\) MLyReal(FinalPartNo(1)) + New \(Y\)
else
NewY = MLyReal(FinalP-rtNo(1)) - NewY
end if
do \(\mathrm{a}=1\), MoINo- 1
dist
((MLxReal(a)-
Newx \(\left.)^{* * 2} 2\right)+\left((\text { MLyReal(a)-Newy })^{* *} 2\right)+((\) MLzReal(a)-NewZ)**2)
Dist \(=\) sqrt(Dist)
if (Dist < MLr(a)+RadT-1) then
OverlapCount \(=\) OverlapCount + 1
if (OverlapCount \(>2500\) ) then
GO TO 40
end if
FinalPartNo(1) = a
FullCount \(=\) FullCount +1
GO TO 60
end if
end do
else! On a regular edge so resting on two particles
NewXVal = .FALSE.
NewZVal = .FALSE.
if (EdgeSide \(==5\) ) then
stochxnew(1) = RadT
newCoords(3) = TempZ
NewXVal = .TRUE.
elseif (EdgeSide \(==6\) ) then
newCoords(1) = TempX
stochxnew(3) = RadT
NewZVal = .TRUE.
```

    elseif (EdgeSide == 7) then
    newCoords(1) = TempX
    stochxnew(3) =-GridSize - RadT
    NewZVal = .TRUE.
    elseif (EdgeSide == 8) then
stochxnew(1) =-GridSize - RadT
newCoords(3) = TempZ
NewXVal = .TRUE.
end if
stochDists(1) = FinalPartDist(1,2)
stochDists(2) = FinalPartDist(2,2)
sumDist = stochDists(1) + stochDists(2)
newCoords(2) = TempY
dx(1) = 10 * RadLarge
dx(2) = 10 * RadLarge
dx(3) = 10 * RadLarge
do a = 1, 10
do b = 1, 3
dx(b) = dx(b) / 10
end do
do c=1,500
call random_number(RX)
stochxnew(2) = newCoords(2) +
dx(2) * (2*RX-1)
if (NewXVal .eqv. .TRUE.) then
call random_number(RX)
stochxnew(3)
elseif (NewZVal .eqv. .TRUE.) then
call random_number(RX)
stochxnew(1)
end if
ibad = 0
do b = 1, 2
stochDists(b)
((PartCoords(b,1)-stochxnew(1))**2)+((PartCoords(b,2)-
stochxnew(2))**2)+((PartCoords(b,3)-stochxnew(3))**2)
ists(b-) - RadT - MLr(FinalPartNo(b))
stochDists(2)
== 0) then

```
stochxnew(b)
end do sumDist = stochynew
            end do
    end do
    NewX = newCoords(1)
    NewY = newCoords(2)
    NewZ = newCoords(3)
    do \(\mathrm{a}=1\), MolNo-1
                            dist \(\quad=\quad((M L x R e a l(a)-\)
Newx)**2)+((MLyReal(a)-Newy)**2)+((MLzReal(a)-NewZ)**2)
        Dist \(=\) sqrt(Dist)
        if (Dist < MLr(a) +RadT-1) then
                            OverDist = 0
                            OverlapCount \(=\) OverlapCount +1
                                    if (OverlapCount > 2500) then
                                    GO TO 30
                                    end if
                                    do \(b=1,2\)
                                    dist \(=((M L x R e a l(a)-\)
PartCoords(b,1))**2)+((MLyReal(a)-PartCoords(b,2))**2)+((MLzReal(a)-PartCoords(b,3))**2)
                                    Dist = sqrt(Dist)
                                    if (Dist < OverDist .or.
OverDist == 0) then
                                    OverDist = Dist
                                    OverDistNo = b
                                    end if
                                    end do
                                    FinalPartNo(OverDistNo) =a
                                    FullCount \(=\) FullCount +1
                                    if (OverDist \(==0\) ) then
                                    GO TO 30
            else
                    GO TO 60
                end if
        end if
            end do
            do \(a=1,2\)
                            FinalDists(a) \(\quad=\quad(\) PartCoords(a,1)-
NewX)*2 2\()+((\) PartCoords(a,2)-NewY)**2)+((PartCoords(a,3)-NewZ)*2 \()\)
                        FinalDists(a) = sqrt(FinalDists(a))
                        if (FinalDists(a)
RadT+MLr(FinalPartNo(a))+1) then
                                FullCount \(=\) FullCount +1
30
                                    CONTINUE
                                    if (FirstSide .eqv. .TRUE.) then
                                    do \(b=1\), MolNo-1
                                    dist
((MLxReal(b)-Newx)**2)+((MLzReal(b)-NewZ)**2)
                                    Dist \(=\operatorname{sqrt}(\) Dist \()\)
\(\left.\operatorname{MLr}(\mathrm{b})+\left(\operatorname{RadT}^{*} 8\right)\right)\) then
\[
\text { SideCheckNo(SideCheckCount) }=b
\]

SideCheckCount \(=\) SideCheckCount +1

SideCheckCount-1, 1, -1
SideCheckCount-1, 1, -1
then
if (Dist < RadT +

SideCombi(SideCount,1) = SideCheckNo(b)
SideCombi(SideCount,2) \(=\) SICheckNo(c)
SideCount \(=\) SideCount +1
else
exit bLoop
end if

SideCombi(b,1)
SideCombi(b,2)

RadT) then
if (NewX < RadT .or. NewY < RadT .or. NewZ <
FullCount \(=\) FullCount +1 GO TO 30
elseif (NewX > GridSize-RadT .or. New \(Y>\) GridSize-
RadT .or. NewZ > GridSize-RadT) then
FullCount \(=\) FullCount +1
GO TO 30
end if
if (NewX < RadT .or. NewY < RadT .or. NewZ < RadT) then FullCount = FullCount +1
GO TO 40
elseif (NewX > GridSize-RadT .or. NewY > GridSize-RadT
.or. NewZ > GridSize-RadT) then
FullCount \(=\) FullCount +1
GO TO 40
end if
MLxReal(MolNo) \(=\) New \(X\)
MLyReal(MolNo) \(=\) New \(Y\)
MLzReal(MolNo) \(=\) NewZ
else
MLxReal(MoINo) \(=\) TempX \(\quad\) ! Saves the particle location
MLyReal(MolNo) \(=\) TempY MLzReal(MolNo) = TempZ
end if

MLr(MolNo) = RadT
FullCount = 0
OverlapCount \(=0\)
Full = 0
MoINo \(=\) MolNo +1
else
MLxReal(MoINo) \(=x\)
MLyReal(MoINo) \(=y\)
MLzReal(MolNo) = z
MLr(MoINo) \(=\) RadT
FullCount \(=0\)
OverlapCount \(=0\)
Full = 0
\(\mathrm{MolNo}=\mathrm{MolNo}+1\)
end if
CONTINUE
else
Full = 1
CONTINUE
end if
end
subroutine PointSafe! Determines if the falling particle has impacted yet
use allSubs ! Loads the variables from the module
integer a, b, c
real Dist
character t
Hit = .FALSE.
FullCheck \(=\).FALSE.
! Checks the distance between the current falling particle location and previously placed partice to determine if it has impacted
cloop: do \(-=1\), MolNo-1
Dist \(=\left((\operatorname{MLxReal}(\mathrm{a})-\mathrm{x})^{* *} 2\right)+\left((\operatorname{MLyReal}(\mathrm{a})-\mathrm{y})^{* *} 2\right)+\left((\operatorname{MLzReal}(\mathrm{a})-\mathrm{z})^{* *} 2\right)\)
Dist \(=\) sqrt(Dist)
if (Dist <= ((RadT) \(+(\operatorname{Mlr}(\mathrm{a}))))\) then
Hit = .TRUE.
exit cloop
end if
end do cloop
! If the impact is above the top of the box, a counter is incremented to show the box may be full
if ((Hit .eqv. .TRUE.) .and. (y -= (GridSize - RadT) )) then
Hit = .FALSE.
FullCount \(=\) FullCount +1
RoofCount \(=\) RoofCount +1
end if
if (RoofCount >=500) then
FullCheck = .TRUE.
end if
end

\section*{Appendix 4: 2D Chain System Algorithm}

This appendix contains the algorithm used to create the 2D chain systems.
```

    module allSubs ! Initialises the variables used through all functions
    character, dimension (:,:), allocatable, public :: RA*4
    integer, dimension (:,:), allocatable, public :: RAMolClose
    integer MolNo, RadLarge, RadSmall, BoxSize, GridSize, Rads, count, SN, Full,
    FullCount, OneLegacyCount
integer MLx, MLy, MLr, Quad, QuadC, AllocateVal, Roofcount
real MLxReal, MLyReal
integer, dimension (:), allocatable, public :: OneLegacyCounterCount
integer, dimension (:,:), allocatable, public :: Ones
integer, dimension (:,:), allocatable, public:: ChainOnes
integer, dimension (:,:,:), allocatable, public:: OnesLegacy
integer, dimension (:,:), allocatable, public :: Contacts
dimension MLr(10000), Rads(10), MLxReal(10000), MLyReal(10000)
logical FullCheck, Hit, RoofHit, StartPlace
integer x, y, Long, Tall, RadT, ChainLength, OverFallCount, MinFallCount, LoopNo
end module allSubs
program packedbed
use allSubs ! Loads the variables from the module
! Initialises local variables
character t, FileName*15, FileID*3
integer m, n, check, PrintNo, ProgCount, PCld, iSeed, count3
dimension FileID(1000)
real RX, ScaleFac, ScaleVal
real Dist
real PartArea, VoidArea, VoidFrac, Pi
integer count2, RadTnew, TotLength
logical Finished, Cont, Impact
dimension iSeed(50)
! Variables initial values set
StartPlace = .TRUE.
OverFallCount =0
MinFallCount = 0
LoopNo = '
if ( }t== 'y') the
Rads(1) = 10
inputted 's Rads'x) = 'Radius'
SN =1 ! Sets the number of different radii in the system
RadLarge = 0
RadSmall = 0
ChainLength = 5 ! Sets the number of particles per chain
do count = 1, SN
if (RadLarge < Rads(count)) then
RadLarge = Rads(count)
end if
if (RadSmall > Rads(count) .or. RadSmall == 0) then

```
```

        RadSmall = Rads(count)
        end if
    end do
RadLarge = 10
RadSmall = 10
! Calculates the box size based on the largest radius present
BoxSize = (RadLarge*6) * (ChainLength/2)
GridSize = BoxSize*5
AllocateVal = ((BoxSize*3)**2)*2
! Allocates the arrays
allocate(RA(1:GridSize, 1:GridSize))
allocate(RAMolClose(1:GridSize, 1:GridSize))
allocate(Ones(1:AllocateVal,1:2))
allocate(ChainOnes(1:AllocateVal,1:2))
allocate(OnesLegacy(1:270,1:AllocateVal,1:2))
allocate(OneLegacyCounterCount(1:270))
do ProgCount = 1,50
write(FileID'Prog'ount), '(i0)') ProgCount
end do
! Se219nitialiables intial values
MLxreal = 0
MLyReal = 0
MLr = 0
PartArea = 0
VoidArea = 0
VoidFrac = 0
Pi=3.141596535
TotLength = 0
MolNo = 1
OneLegacyCount = 1
OverFallCount = 0
"FileName = "
Full = 0
check = 0
FullCount = 0
Finished = .FALSE.
Ones = 0
OnesLegacy = 0
OneLegacyCounterCount ",
RA = '0'
RAMolClose = 0
RoofCount = 0
RoofHit = .FALSE.
call random_seed()

```
do ProgCount \(=1,50!\) Starts the loop for the number of systems to be created

LayerLoop: do while (count < 10000000)
Impact \(=\). FALSE.
! Picks a random radius and \(x\) coordinate, and sets \(y\) to be on
the bottom of the box
call random_number(RX)
count2 \(=1+\) floor(SN*RX) RadT = Rads(count2)
call random_number(RX)
count2 \(=1+\) floor ((GridSize-(2*RadT) \() * R X)\)
x = count2+RadT
\(\mathrm{y}=\mathrm{RadT}\)
if \((\mathrm{MoINo}>1)\) then \(\quad\) ! Checks there is already at least
one particle in the system
hitloop: do count- = 1, MoINo-1
Dist =
((MLxReal(count3)-
\(\left.x)^{* *} 2\right)+((\) MLyReal(count3)-y)**2)
Dist \(=\) sqrt(Dist)
if (Dist \(<=((\) RadT* 2\()+(M l r(\) count 3\())))\) then
count = count + 1
Impact = .TRUE.
exit hitloop
end if
end do hitloop
if ((Impact .eqv. .FALSE.) .and. ( \(x<=\) GridSize-
(RadT*ChainLength))) then ! If the particle is not overlapping with any others and is inside the grid, its location is saved
```

MLxReal(MolNo) $=x$
MLyReal(MoINo) $=y$
MLr(MolNo) = RadT
$\mathrm{MolNo}=\mathrm{MolNo}+1$
do $m=1$, ChainLength -1
$x=x+\operatorname{RadT}$
if ( $\mathrm{x}<\mathrm{GridSize-RadT} \mathrm{)} \mathrm{then}$
Impact = .FALSE.
hitloop3: do count3 = 1,

```
MolNo - \((m+1)\)
\(\left((\text { MLxReal }(\text { count } 3)-x)^{* *} 2\right)+\left((\text { MLyReal }(\text { count3 })-y)^{* *} 2\right)\)
\(\left(\left(\operatorname{RadT}{ }^{*} 2\right)+(\operatorname{Mlr}(\right.\) count 3\(\left.\left.))\right)\right)\) then

Dist = Dist \(=\) sqrt(Dist) if (Dist <= count = Impact = exit
end if end do hitloop3

MoINo = MoINo -
(m)

Cycle LayerLoop end if else
\(\mathrm{MolNo}=\mathrm{MolNo}-(\mathrm{m})\) Cycle LayerLoop end if
end do
\[
\text { count }=0
\]
end if
else
MLxReal(MoINo) \(=x\)
MLyReal(MolNo) \(=y\)
\(\mathrm{MLr}(\mathrm{MolNo})=\) RadT
MolNo = MolNo + 1
do \(m=1\), ChainLength -1
\(x=x+\operatorname{Rad} T\)
if ( \(x<\) GridSize - RadT) then
MLxReal(MolNo) \(=x\)
\(\operatorname{MLyReal}(\mathrm{MolNo})=y\)
\(\mathrm{MLr}(\mathrm{MolNo})=\) RadT
MolNo = MolNo + 1
else
MolNo = MolNo - (m)
Cycle LayerLoop
end if
end do
end if
end do LayerLoop
! This loops through the base line to check that there is nowhere a small particle could fall through to the bottom of the box, and if so, places a particle there do \(m=\) RadSmall, GridSize-RadSmall RadT = RadSmall
Impact = .FALSE.
hitloop2: do count3 = 1, MoINo - 1
Dist \(=\left((\text { MLxReal }(\text { count } 3)-m)^{* *} 2\right)\)
Dist \(=\) sqrt(Dist)
if (Dist < ((RadSmall) \()+(\) MIr(count3) \())\) ) then
count \(=\) count +1
Impact = .TRUE. exit hitloop2
end if
```

    end do hitloop2
    if (Impact .eqv. .FALSE.) then
        count = 0
        MLxReal(MolNo)=m
        MLyReal(MolNo) = RadSmall
        MLr(MoINo) = RadSmall
        MolNo = MolNo + 1
        call AddChain
    end if
    end do
    StartPlace = .FALSE.
    do n=1,500 !Loops for each particle being added to the system,
    using the main function. At the end of each loop, it checks if the box is full and if so, leaves the
loop.
LoopNo = n
call molpos
if (Full == 1) then
exit
elseif (RoofHit .eqv. .TRUE.) then
exit
end if
end do
t = 'y'
if (t == 'y' .and. RoofHit .eqv. .TRUE.) then ! Saves the particle
locations to a file
FileName = "
FileName = trim(adjustl(FileID(ProgCount))) // '.csv'
open(1, file = FileName, status = 'new')
do y = 1,MolNo-1
write(1,*) MLxReal(y), ',' , MLyReal(y), ',' , MLr(y)
end do
close(1)
end if
end do
end if
end program
subroutine molpos
use allSubs ! Loads the variables from the module
! Sets up the local variables
integer count2, Spot, Height, DoubRad, RowRad, a,b,c, Radln, m, n, TempX, TempY
real MidWay, Dist
character t, FileName*15
integer SavIncremX, SavIncremY, SafeLocCount, LR, SavOneX, SavOneY,
SavOnePart, LRNo, OneCount, RealPos1, RealPos2
integer TempRealPos1, TempRealPos2, ChainOneCount
logical SafeLocFound, Go, ResetCheck
real TempXa, TempXb, TempYa, TempYb, DistAB, DistBC, DistAC, AngleA, AngleB,
AngleFin, GradFin, HelpDist
real FDistA, FDistB, FDistC, FDistD

```
real xDiff, yDiff, Pi, FinalSavX, FinalSavY, SavDist
integer FinalSavLong, FinalSavTall, checktime, Balanced
integer Balances, Touches
dimension Balances(10)
real DistFac, RadScale
integer NewPos, TRP1Swap, TRP2Swap
integer FinalPart, SideCount
dimension FinalPart(2,3)
real PartCoords, stochDists, sumDist, dx, stochxnew, newCoords, stochynew
integer ibad
dimension PartCoords(2,2), stochDists(2), newCoords(2), dx(2), stochxnew(2)
real RX, NewX, NewY
logical ChainAdd
real OverDist
integer OverDistNo
logical NotBal, FirstBal
dimension BalCheckNo(10000), BalCombi(100000,2)
integer BalCheckCount, BalCount, BalCheckNo, BalCombi, BalAttempt
integer OverlapCount
logical EdgeCase, FirstEdge
integer EdgeCombi, EdgeCount, EdgeAttempt
dimension EdgeCombi(10000)
integer ChainStartNo, ChainStartCont, d
real ChainGrad, EquC
logical ChainHitCheck, ChainEdgeHitCheck, ChainTopHitCheck
logical TopCase
integer OverTopCount, PartHit, MiddlePart, MiddlePartA, MiddlePartB, FallPoint,
ContPoint, ContPointB
real Dy, intC, CheckY, MiddlePoint, ContDist, ContSpot
logical Fell, Tilt, HMAdju
integer FallCount, AdjCount
real ContSpotTemp, ContSpotTempUy, ContSpotL, ContSpotR, ContSpotUy, ContSpotUx
integer ContSpotUn, NLCount
logical RoundTwo
real Valdx, ValDist, ValAng1,ValDist2, ValDist3, ValAng2a, ValAng2b, ValAng2, ValAng3
logical SideBal, Upwards, Downwards

Fell = .FALSE.
Tilt = .FALSE.
FallPoint \(=0\)
FallCount \(=0\)
AdjCount \(=0\)
40
CONTINUE
if (FullCount \(==2500000)\) then
Full = 1
end if
if (FallCount >20) then
OverFallCount \(=\) OverFallCount +1
if (OverFallCount >=100) then
Full = 1
end if
GO TO 10
end if
! Setting initial values of variables
Hit = .FALSE.
ResetCheck = .FALSE.
TopCase = .FALSE.
ChainTopHitCheck = .FALSE.
checktime \(=1\)
Balanced \(=0\)
Touches = 0
Balances = 0
NLCount \(=0\)
HMAdju = .FALSE.
ContSpotTemp = 0
ContSpotTempUy = 0
ContSpotL = 0
ContSpotR = 0
ContSpotUy \(=0\)
ContSpotUx = 0
ContSpotUn = 0
SideBal = .FALSE.
Upwards = .FALSE.
Downwards = .FALSE.
RoundTwo = .FALSE.
MiddlePart = 0
MiddlePartA \(=0\)
MiddlePartB \(=0\)
MiddlePoint \(=0\)
ContPoint \(=0\)
ContPointB = 0
ContSpot \(=0\)
ContDist \(=99999\)
Valdx \(=0\)
ValDist \(=0\)
ValAng1 = 0
ValDist2 \(=0\)
ValDist3 = 0
ValAng2a \(=0\)
ValAng2b \(=0\)
ValAng2 \(=0\)
ValAng3 = 0
Dy \(=0\)
intC \(=0\)
CheckY = 0
ChainStartNo \(=0\)
ChainStartCont =1
ChainGrad \(=0\)
EquC \(=0\)

EdgeAttempt \(=0\)
EdgeCount \(=0\)
EdgeCombi \(=0\)
EdgeCase = .FALSE.
FirstEdge = .TRUE
FinalPart \(=999999\)
OverDist = 0
OverDistNo \(=0\)
OverlapCount \(=0\)
OverTopCount \(=0\)
TRP1Swap \(=0\)
TRP2Swap = 0
ChainAdd \(=\). FALSE .
NotBal = .FALSE.
FirstBal = .TRUE.
BalCheckNo = 0
BalCombi \(=0\)
BalCheckCount \(=0\)
BalCount \(=0\)
BalCheckNo \(=0\)
BalCombi \(=0\)
BalAttempt \(=0\)
RadScale \(=0\)
TempRealPos1 = 0
TempRealPos2 \(=0\)
DistFac = 0
FDistA \(=0\)
FDistB \(=0\)
FDistC \(=0\)
FDistD \(=0\)
SavDist \(=0\)
SavOneX = 0
SavOneY = 0
TempXa = 0
TempXb \(=0\)
TempYa \(=0\)
TempYb = 0
DistAB \(=0\)
DistBC \(=0\)
DistAC \(=0\)
AngleA \(=0\)
AngleB \(=0\)
AngleFin \(=0\)
GradFin \(=0\)
\(x\) Diff \(=0\)
\(y\) Diff \(=0\)
\(\mathrm{Pi}=3.141596535\)
NewPos = 0
FinalDists \(=0\)
```

PartCoords = 0
stochDists = 0
sumDist $=0$
$\mathrm{dx}=0$
stochxnew = 0
newCoords = 0
stochynew $=0$
if (Fell .eqv. .TRUE.) then
Fell = .FALSE.
GO TO 66
end if
! Randomly chooses which radius will be used for this particle
call random_number(RX)
RadScale = RadLarge/RadSmall
RadScale $=$ RadScale +1
count2 $=1+$ floor ( $2^{*}$ RX $)$
if (count2 == 2) then
RadT = RadLarge
else
RadT = RadSmall
end if
wloop: do while (Hit .eqv. .FALSE.)
FallPoint = GridSize
! Randomly chooses the $x$ value
call random_number(RX)
Spot $=1+$ floor ((GridSize-(2*RadT))*RX)
x = Spot+RadT
CONTINUE
do $y=$ FallPoint, RadT, -1 ! Loops from the top of the box, and sends to the function to determine impact
Long $=(x /$ BoxSize $)+1$
Tall $=(y / B o x S i z e)+1$
call PointSafe
! If the box is full or an impact has occured, the loop is exited
if (Full $==1$ ) then exit wloop
end if
if (FullCheck .eqv. .TRUE.) then
RoofHit = .TRUE.
GO TO 10
end if
if (Hit .eqv. .TRUE.) then
exit wloop
end if
end do
end do wloop

```
if ((Hit .eqv. .TRUE.) .and. (Full /= 1)) then
if (MolNo > 1 ) then
RA = '0'
RAMolClose \(=0\)
! Sets up the variables to be used for particle placement
Ones \(=0\)
OneCount = 1
ChainOnes \(=0\)
ChainOneCount \(=1\)
do \(\mathrm{a}=1\), MoINo - \(1 \quad\) ! Loops through the particles for contour plot
placement
MLxCor \(=\) MLxReal(a)
MLyCor \(=\) MLyReal(a) ! Takes the radius, \(x\) and \(y\) coordinates
of the current particle in the loop
Radln \(=\operatorname{Mlr}(\mathrm{a})\)
DoubRad \(=(\) Radll \(n+\) RadT \()+1\)
do Height \(=0\), Radln ! Draws the particle onto the contour plot, "-"s marking blocked locations, "1"s being valid spots MidWay \(=\) Radln**2 - Heigh**2 RowRad = abs(sqrt(MidWay)) if((MLxCor+Height<=GridSize-
RadT).and.(MLyCor+RowRad<=GridSize-RadT).and.(MLyCor-
RowRad>=RadT).and.(MLxCor-Height>=RadT))then
RA(MLyCor+RowRad, MLxCor+Height) = '-'
RA(MLyCor-RowRad, MLxCor+Height) = '-'
RA(MLyCor+RowRad, MLxCor-Height) \(=\) '-'
RA(MLyCor-RowRad, MLxCor-Height) \(=\) ' - '
end if
do count2 \(=-\) RowRad,RowRad
if((MLxCor+Height<=GridSize-
RadT).and.(MLyCor+count2<=GridSize).and.(MLxCor-
Height>=RadT).and.(MLyCor+count2>=RadT))then

> RA(MLyCor+count2,

MLxCor+Height) = '-'
RA(MLyCor+count2, MLxCor-
Height) \(=\) ' - '
end if
end do
end do
do Height \(=0\), DoubRad ! Draws locations around the current particle that are too close for the new particle to be added due to overlap MidWay \(=\) DoubRad**2 - Height**2 \(^{*}\)
RowRad = abs(sqrt(Midway)) do count2 = -rowrad+1, rowrad-1
if
((MLyCor+count2<=GridSize).and.(MLxCor+Height<=GridSize-
RadT).and.(MLyCor+count2>=RadT).and.(MLxCor+Height>=RadT))then
RA(MLyCor+count2,
MLxCor+Height) = '-'
end if
((MLyCor+count2<=GridSize).and.(MLxCor-Height<=GridSize-
RadT).and.(MLyCor+count2>=RadT).and.(MLxCor-Height>=RadT))then
RA(MLyCor+count2, MLxCor-
Height) = '-'
end if
end do
end do
do Height = -Radln, Radln
do count2 = MlyCor-1, 1, -1
if
((count2<=GridSize).and.(MLxCor+Height<=GridSize-
RadT).and.(count2>=RadT).and.(MLxCor+Height>=RadT))then
RA(count2, MLxCor+Height) = '-'
end if
end do
end do
do Height \(=-\) DoubRad, \(0 \quad\) ! Adds the valid spots for the
resting particle to be placed
MidWay \(=\) DoubRad**2 - Height**2 \(^{*}\)
RowRad = abs(sqrt(Midway))
if
((MLyCor+RowRad<=GridSize).and.(MLxCor+height<=GridSize-
RadT).and.(MLxCor+height>=RadT).and.(MLyCor+RowRad>=RadT))then
if (RA(MLyCor+RowRad, MLxCor+Height)
/= '-') then
MLxCor+Height) = '1'
RA(MLyCor+RowRad,
RAMoIClose(MLyCor+RowRad,
MLxCor+Height) \(=\mathrm{a}\)
end if
end if
if ((MLyCor-
RowRad>=RadT).and.(MLxCor+height<=GridSize-
RadT).and.(MLxCor+height>=RadT).and.(MLyCor-RowRad<=GridSize)) then
if (RA(MLyCor-RowRad, MLxCor+Height) /=
'-') then
MLxCor+Height \()=' 1\) '
RA(MLyCor-RowRad,
RAMolClose(MLyCor-RowRad,
MLxCor+Height) \(=\mathrm{a}\)
end if
end if
if ((MLyCor+RowRad<=GridSize).and.(MLxCor-
Height<=GridSize-RadT).and.(MLxCor-Height>=RadT).and.(MLyCor+RowRad>=RadT))then if (RA(MLyCor+RowRad, MLxCor-Height) /=
'-') then

Height) = '1'
RA(MLyCor+RowRad, MLxCor-

MLxCor-Height) \(=\mathrm{a}\)
RAMoIClose(MLyCor+RowRad,
end if
end if

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if ((MLyCor-RowRad>=RadT).and.(MLxCor-height<=GridSize-RadT).and.(MLxCor-height>=RadT).and.(MLyCorRowRad<=GridSize))then
'-') then
Height) = '1'
MLxCor-Height) \(=\mathrm{a}\)
if (RA(MLyCor-RowRad, MLxCor-Height) /=
RA(MLyCor-RowRad, MLxCor-
RAMoIClose(MLyCor-RowRad,
end if
end if
do count2 = -RowRad, RowRad
if
((MLyCor+count2<=GridSize).and.(MLxCor+height<=GridSize-
RadT).and.(MLxCor+height>=RadT).and.(MLyCor+count2>=RadT))then
if (RA(MLyCor+count2,
MLxCor+Height) /= '-') then RA(MLyCor+count2,
MLxCor+Height) = '1'
RAMoIClose(MLyCor+count2, MLxCor+Height) \(=\mathrm{a}\)
end if
end if
if ((MLyCor-
count2>=RadT).and.(MLxCor+height<=GridSize-
RadT).and.(MLxCor+height>=RadT).and.(MLyCor-count2<=GridSize))then
if (RA(MLyCor-count2,
MLxCor+Height) /= '-') then

MLxCor+Height) = '1'
RA(MLyCor-count2,
RAMoIClose(MLyCor-
count2, MLxCor+Height) \(=\mathrm{a}\)
end if
end if
if ((MLyCor+count2>=RadT).and.(MLxCor-
height<=GridSize-RadT).and.(MLxCor-
height>=RadT).and.(MLyCor+count2<=GridSize))then
if (RA(MLyCor+count2, MLxCor-
Height) /= '-') then
RA(MLyCor+count2,
MLxCor-Height) = '1'
RAMoIClose(MLyCor+count2, MLxCor-Height) = a
end if
end if
if
((MLyCor-
count2<=GridSize).and.(MLxCor-height<=GridSize-RadT).and.(MLxCor-height>=RadT).and.(MLyCor-count2>=RadT))then

Height) /= '-') then
MLxCor-Height) \(=\) ' 1 '
count2, MLxCor-Height) \(=\mathrm{a}\)
if (RA(MLyCor-count2, MLxCor-RA(MLyCor-count2,

RAMoIClose(MLyCor-
end if
end if
end do
\[
\begin{aligned}
& \text { end do } \\
& \text { end do } \\
& \text { do } a=1 \text {, GridSize ! Finds the valid points and saves them to an array } \\
& \text { do } b=1 \text {, GridSize } \\
& \text { if (RA(b,a) }==1 \text { '1') then } \\
& \text { ReWLoop: do } c=1 \text {, OneCount } \\
& \text { if ((Ones }(c, 2)==a) \text { and. (Ones(c,1) } \\
& \text { Ones }(\mathrm{c}, 1)=\mathrm{b} \\
& \text { exit ReWLoop }
\end{aligned}
\]
<b)) then
then
                                    Ones(OneCount, 1) = b
                                    Ones(OneCount, 2) = a
                                    OneCount = OneCount + 1
                                    end if
            end if
    end do
end do
do \(a=1\), OneCount \(-1!\) Finds the closest of these points to the impact location and moves the particle to it
\[
\begin{aligned}
& \text { TempX }=\text { Ones }(\mathrm{a}, 2) \\
& \text { TempY }=\text { Ones }(\mathrm{a}, 1)
\end{aligned}
\]
if (TempY \(<=y+1\) ) then
Dist \(=\left((x-\text { TempX })^{* *} 2\right)+\left((y-\text { Temp } Y)^{* *} 2\right)\)
Dist \(=\) sqrt(Dist)
if ((Dist < SavDist) .or. (SavDist \(==0)\) ) then
SavDist \(=\) Dist
SavOneX = Ones(a,2)
SavOneY = Ones(a,1)
end if
end if
end do
TempX = SavOneX
TempY = SavOneY
if \(((\) TempX \(==0)\).and. \((\) TempY \(==0))\) then GO TO 10
end if

SavOnePart = RAMoIClose \((\) TempY, TempX \()\)
SafeLocCount \(=0\)
SavIncremX = SavOneX
SavIncremY = SavOneY
SafeLocFound = .FALSE.
FinalSavX \(=0\)
FinalSavY \(=0\)
\(\mathrm{LR}=0\)
RealPos1 \(=0\)
RealPos2 \(=0\)
if \((\) MLxReal(SavOnePart \()==\) TempX) then! Determines which way
the particle should roll
call random_number(RX)
LRNo = \(1+\) floor(2*RX)
if \((\mathrm{LRNo}==1)\) then
\(L R=-1\)
elseif (LRNo == 2) then
\(L R=1\)
end if
elseif (MLxReal(SavOnePart) < TempX) then
LR = 1
Upwards = .TRUE.
elseif \((\) MLxReal (SavOnePart) \(>\) TempX) then
LR = -1
Downwards = .TRUE.
end if
RMPInter \(=0\)
RMPPrev = SavOnePart
RealPos1 = SavOnePart
do \(\mathrm{a}=1\), OneCount-1
if (Ones(a,2) == TempX) then
SideCount = a
end if
end do
do while (SafeLocFound .eqv. .FALSE.) ! Iterates in that direction until the next position would be higher, or reaching the edge of the box
if ((Ones(SideCount+LR,1) > Ones(SideCount,1)) .or. (Ones(SideCount,2) == RadT) .or. (Ones(SideCount,2) == GridSize-RadT)) then SafeLocFound = .TRUE.
else
SideCount \(=\) SideCount + LR
end if
end do

19
CONTINUE
TempX = Ones(SideCount+AdjCount,2)
TempY = Ones(SideCount+AdjCount,1)
if (TempX > GridSize-RadT) then
TempX = GridSize-RadT
TempY = Ones(SideCount-AdjCount,1)
elseif (TempX < RadT) then
TempX = RadT
TempY = Ones(SideCount-AdjCount,1)
end if
do \(\mathrm{a}=1, \mathrm{MolNo}-1!\) Finds the particles closest to the low point for the new particle to be resting on
if (MLyReal(a) < TempY+RadT) then
Dist \(=((\) MLxReal(a)-TempX)**2) \(+((\) MLyReal \((a)-\)
TempY)**2)
Dist = sqrt(Dist) - RadT - MLr(a)
if (Dist <= FinalPart(1,2)) then
FinalPart( 2,1 ) \(=\) FinalPart \((1,1)\)
FinalPart(2,2) = FinalPart(1,2)
FinalPart(2,3) = FinalPart(1,3)
FinalPart \((1,1)=a\)
FinalPart \((1,2)=\) Dist
FinalPart(1,3) = Dist + RadT + MLr(a)
elseif (Dist <= FinalPart(2,2)) then
FinalPart \((2,1)=\mathrm{a}\)
FinalPart \((2,2)=\) Dist
FinalPart(2,3) = Dist + RadT + MLr(a)
end if
end if
end do

CONTINUE

PartCoords(1,1) \(=\) MLxReal(FinalPart(1,1))
PartCoords(1,2) \(=\) MLyReal(FinalPart(1,1))
PartCoords(2,1) = MLxReal(FinalPart(2,1))
PartCoords(2,2) \(=\) MLyReal(FinalPart(2,1))
if ((TempX == RadT) .or. (TempX == GridSize-RadT)) then EdgeCase = .TRUE.
end if
if (EdgeCase .eqv. .TRUE.) then ! If the particle is on an edge, it balances the new particle on the edge + one particle

NewX = TempX
Dist \(=\) RadT + MLr(FinalPart(1,1))
NewY
(MLxReal(FinalPart(1,1))**2)+(2*MLxReal(FinalPart(1,1))*NewX)
NewY = NewY \(+\left(\right.\) Dist**2 \(\left.^{*}\right)-\left(\right.\) New \(\left.{ }^{* *}{ }^{2}\right)\)
New \(Y=\operatorname{sqrt}(N e w Y)\)
if (NewY /= NewY) then
71
CONTINUE
if (FirstEdge .eqv. .TRUE.) then
do \(a=1\), MolNo-1
Dist = (MLxReal(a)-NewX)
if (Dist \(<\) RadT \(+\quad\) MLr(a) +
(RadT*8)) then
a
EdgeCombi(EdgeCount) =
EdgeCount = EdgeCount +
1
                        EdgeAttempt = EdgeAttempt +1
                                    GO TO 50
    end if
    FullCount \(=\) FullCount +1
    GO TO 10
    end if
    if ((TempY - (MLyReal(FinalPart(1,1)) + NewY)) < (TempY -
(MLyReal(FinalPart(1,1)) - NewY))) then
    \(\operatorname{New} Y=\operatorname{MLyReal}(\) FinalPart \((1,1))+\) New \(Y\)
    else
    New \(Y=\operatorname{MLyReal}(\) FinalPart(1,1)) - New \(Y\)
    end if
    do \(a=1\), MolNo-1 ! Confirming the new particle is not
overlapping with any other particles
    Dist \(=((\) MLxReal(a)-NewX)**2)+((MLyReal(a)-
NewY)**2)
    Dist \(=\) sqrt(Dist)
    if (Dist < MLr(a)+RadT-0.1) then
                            OverlapCount = OverlapCount + 1
                            if (OverlapCount > 2500) then
                                    GO TO 71
                end if
                FinalPart(1,1) =a
                FullCount \(=\) FullCount +1
                GO TO 50
            end if
end do
                            if ((NewX < RadT) .or. (NewY < RadT) .or. (NewX > GridSize-
RadT) .or. (NewY > GridSize-RadT)) then
                                    FullCount \(=\) FullCount +1
                                    GO TO 10
end if
else ! else if the particle is not on an edge it balances on two particles through stochastic optimisation
```

newCoords = 0
stochDists = 0
sumDist $=0$
$\mathrm{dx}=0$
stochxnew = 0
ibad $=0$
newCoords(1) $=$ TempX
newCoords(2) $=$ TempY
stochDists(1) = FinalPart(1,3)
stochDists(2) = FinalPart(2,3)
sumDist $=$ stochDists(1) + stochDists(2)

```
```

    \(\mathrm{dx}(1)=10\) * RadLarge
    \(d x(2)=10\) * RadLarge
    do \(a=1,10\)
        do \(b=1,2\)
        \(d x(b)=d x(b) / 10\)
    end do
    do \(c=1,500\)
                            call random_number(RX)
                            stochxnew(2) = newCoords(2) + (dx(2) *
    ((2*RX)-1))
call random_number(RX)
stochxnew(1) = newCoords(1) + (dx(1) *
((2*RX)-1))
ibad $=0$
do $b=1,2$
stochDists(b) $=(($ PartCoords $(\mathrm{b}, 1)-$
stochxnew(1))**2) + ((PartCoords(b,2)-stochxnew(2))**2)
stochDists(b) $=$ sqrt(stochDists(b)) -
RadT - MLr(FinalPart(b,1))
if (stochDists(b) < 0) then
ibad = 1
end if
end do
stochynew $=$ stochDists(1) + stochDists(2)
if ((stochynew < sumDist) .and. (ibad == 0))
then
stochxnew(b)

```
```

                                    end do
    ```
                                    end do
                                    sumDist = stochynew
                                    sumDist = stochynew
    end if
    end if
    end do
    end do
end do
end do
NewX = newCoords(1)
NewX = newCoords(1)
NewY = newCoords(2)
NewY = newCoords(2)
do \(\mathrm{a}=1\), MolNo- -1
do \(\mathrm{a}=1\), MolNo- -1
                            Dist \(=((\) MLxReal(a)-NewX \() * * 2)+((\) MLyReal \((a)-\)
                            Dist \(=((\) MLxReal(a)-NewX \() * * 2)+((\) MLyReal \((a)-\)
New \(Y\) )**2)
    Dist \(=\) sqrt(Dist)
    if (Dist < MLr(a)+RadT) then
        OverDist = 0
        OverlapCount \(=\) OverlapCount +1
        if (OverlapCount > 2500) then
                                    NotBal = .TRUE.
                                    GO TO 70
        end if
        do \(b=1,2\)
```


if (NotBal .eqv. .TRUE.) then ! If the particle is not correctly balancing then it looks for alternate particles to be resting on and moves to that location

> if (FirstBal .eqv. .TRUE.) then do $\mathrm{a}=1$, MolNo-1

Dist $=\left((\text { MLxReal }(a)-\text { New } X)^{* *} 2\right)$
Dist $=$ sqrt(Dist)
if ((Dist < RadT + MLr(a) + (RadT*8))
.and. (NewY-MlyReal(a) < RadT + MLr(a) + (RadT*6))) then
BalCheckNo(BalCheckCount) = a
BalCheckCount
BalCheckCount + 1
end if
end do
aLoop: do a = BalCheckCount-1, 1, -1
do $b=$ BalCheckCount-1, 1, -1
if (BalCheckNo(b) <
BalCheckNo(a)) then
if (BalCount <=
100000) then
if
(abs(MlxReal(BalCheckNo(a)) - MlxReal(BalCheckNo(b))) <= RadT*2 + MLr(BalCheckNo(a)) + MLr(BalCheckNo(b))) then

BalCombi(BalCount,1) = BalCheckNo(a)
BalCombi(BalCount,2) = BalCheckNo(b)
BalCount $=$ BalCount +1
end if
else
exit aLoop end if end if
end do
end do aLoop
end if
FirstBal = .FALSE .
if (BalAttempt <= BalCount-1) then
do while (BalCombi(BalCount-BalAttempt,1)
== 0 .or. BalCombi(BalCount-BalAttempt,2) == 0)
BalAttempt $=$ BalAttempt +1
end do
FinalPart(1,1) $=$ BalCombi(BalCount-
BalAttempt,1)
BalAttempt,2)

FinalPart $(2,1)=$ BalCombi(BalCount-
BalAttempt $=$ BalAttempt +1
if (BalAttempt <= 100000) then
GO TO 50
end if
end if
if (TempX >= GridSize-(RadT*5)) then
TempX = GridSize-RadT
EdgeCase = .TRUE.
GO TO 50
elseif (TempX <= RadT+(RadT*5)) then
TempX = RadT
EdgeCase = .TRUE.
GO TO 50
end if
if ((AdjCount < 75) .and. (AdjCount > -75)) then
AdjCount = AdjCount - LR
HMAdju = .TRUE.
GO TO 19
elseif (AdjCount < -75 .and. Downwards .eqv.
.TRUE.) then
Downwards = . FALSE.
AdjCount $=0$
LR = 1
GO TO 19
elseif (AdjCount > 75 .and. Upwards .eqv. .TRUE.)
then

$$
\begin{aligned}
& \text { Downwards = .TRUE. } \begin{array}{c}
\text { AdjCount }=0 \\
\text { LR }=-1 \\
\text { GO TO } 19
\end{array} \\
& \text { else } \quad \text { GO TO 10 } \\
& \text { end if } \\
& \text { GO TO } 10
\end{aligned}
$$ GridSize-RadT) .or. (NewY < RadT)) then

RAMolClose $=0$
else
MIxReal(MolNo) $=x$
MlyReal(MoINo) = y
MLr(MoINo) = RadT
FullCount $=0$
MoINo = MolNo + 1
end if
! The first particle in the chain placed, now moving onto placing the rest of the chain
$R A="$
OverlapCount $=0$
MlxCor $=$ MlxReal(MolNo-1)
MlyCor $=$ MlyReal(MoINo-1)
Radln $=$ MLr(MoINo-1)
DoubRad $=($ Radln + RadT $)+1$
do Height $=-$ Radln, $0!$ The contour plot is remade similar to the first time, however valid points are only placed attached to the particle just added to the system

MidWay = Radln**2 - Height**2
RowRad = abs(sqrt(Midway))
if ((MlyCor+RowRad<=GridSize).and.(MlxCor + Height $<=$ GridSize-
RadT).and.(MlxCor+Height>=RadT).and.(MlyCor+RowRad>=RadT))then if (MlyCor+RowRad>= MlyCor) then do $\mathrm{a}=1$, MoINo-2

Dist $=\left((\text { MlxReal }(\mathrm{a})-(\mathrm{MlxCor}+\text { Height }))^{\star *} 2\right) \quad+$
((MlyReal(a)-(MlyCor+RowRad))**2)
Dist $=$ sqrt(Dist)
if (Dist < Radln $+\mathrm{MLr}(\mathrm{a})$ ) then
GO TO 15
end if
end do
RA(MlyCor+RowRad, MlxCor+Height) = '1'
end if
end if
15
CONTINUE
if ((MlyCor-RowRad>=RadT).and.(MlxCor+Height<=GridSize-
RadT).and.(MlxCor+height>=RadT).and.(MlyCor-RowRad<=GridSize))then
if (MlyCor-RowRad>= MlyCor) then do $\mathrm{a}=1$, MolNo-2

Dist $\left.=((\text { MlxReal(a)-(MlxCor+Height }))^{* *} 2\right)+$
((MlyReal(a)-(MlyCor-RowRad))**2)
Dist $=$ sqrt(Dist)
if (Dist < Radln + MLr(a)) then
GO TO 16
end if
end do
RA(MlyCor-RowRad, MlxCor+Height) = ' 1 '
end if
end if
16

## CONTINUE

if ((MlyCor+RowRad<=GridSize).and.(MlxCor-Height<=GridSize-
RadT).and.(MlxCor-Height>=RadT).and.(MlyCor+RowRad>=RadT))then if (MlyCor+RowRad>= MlyCor) then

```
                            do a = 1, MolNo-2
                            Dist = ((MlxReal(a)-(MlxCor-Height))**2)
                                    +
((MlyReal(a)-(MlyCor+RowRad))**2)
    Dist = sqrt(Dist)
    if (Dist < Radln + MLr(a)) then
                                    GO TO 17
    end if
    end do
    RA(MlyCor+RowRad, MlxCor-Height) = '1'
    end if
    end if
1 7
                            CONTINUE
                            if ((MlyCor-RowRad>=RadT).and.(MlxCor-Height<=GridSize-
RadT).and.(MlxCor-height>=RadT).and.(MlyCor-RowRad<=GridSize))then
                        if (MlyCor-RowRad>= MlyCor) then
                        do a = 1, MolNo-2
                            Dist = ((MlxReal(a)-(MlxCor-Height))**2) +
((MlyReal(a)-(MlyCor-RowRad))**2)
                            Dist = sqrt(Dist)
                            if (Dist < Radln + MLr(a)) then
                                    GO TO 18
                            end if
                        end do
                        RA(MlyCor-RowRad, MlxCor-Height) = '1'
                        end if
                            end if
1 8
    end do
    ChainOneCount = 1
    do a = 1, GridSize
        do b=1,GridSize
                if (RA(b,a) == '1') then
                                    ChainOnes(ChainOneCount, 1) = b
                                    ChainOnes(ChainOneCount, 2) = a
                                    ChainOneCount = ChainOneCount + 1
            end if
    end do
    end do
    call random number(RX)
    LRNo = 1 + floor(2*RX)
    CONTINUE
    if (NLCount >= 250) then
    OverFallCount = OverFallCount +1
    MoINo = MoINo - 1
    if (OverFallCount >= 100) then
                Full = 1
    end if
    GO TO 10
    end if
    if (LRNo == 1) then ! Picks whether the chain should fall left or right
    TempX = ChainOnes(1,2)
    TempY = ChainOnes(1,1)
```

elseif (LRNo == 2) then
TempX = ChainOnes(ChainOneCount-1,2)
TempY = ChainOnes(ChainOneCount-1,1)
end if
if (MlxReal(MoINo-1) $==$ GridSize-RadT) then
TempX = ChainOnes $(1,2)$
TempY = ChainOnes(1,1)
elseif (MlxReal(MolNo-1) == RadT) then
TempX = ChainOnes(ChainOneCount-1,2)
TempY = ChainOnes(ChainOneCount-1,1)
end if
if (TempX == 0 .or. TempY ==0) then
TempX = MIxReal(MolNo-1)
TempY = MlyReal(MolNo-1)+MLr(MolNo-1)
end if
FinalPart = 99999
FinalPart $(1,1)=$ MolNo-1
Dist $=\left((\text { MlxReal }(\mathrm{a})-\text { TempX })^{* *} 2\right)+(($ MlyReal(a)-TempY $) * * 2)$
Dist $=$ sqrt(Dist) $-\operatorname{MLr}(\mathrm{a})$
FinalPart(1,2) = Dist
FinalPart(1,3) = Dist + MLr(a)
do $\mathrm{a}=1$, MolNo-2
if (MlyReal(a) < TempY+1) then
Dist $=(($ MlxReal(a)-TempX)**2)+((MlyReal(a)-TempY)**2)
Dist $=\operatorname{sqrt}($ Dist $)-$ RadT $-\operatorname{MLr}(\mathrm{a})$ if (Dist <= FinalPart(2,2)) then

FinalPart $(2,1)=\mathrm{a}$
FinalPart(2,2) = Dist
FinalPart( 2,3 ) $=$ Dist + RadT $+\operatorname{MLr}(\mathrm{a})$ end if
end if
end do
CONTINUE
PartCoords(1,1) $=$ MlxReal(FinalPart(1,1))
PartCoords(1,2) $=$ MlyReal(FinalPart(1,1))
PartCoords(2,1) $=$ MlxReal(FinalPart(2,1))
PartCoords(2,2) $=$ MlyReal(FinalPart(2,1))
EdgeCase = .FALSE.
TopCase = .FALSE.
if ((TempX <= RadT) .or. (TempX >= GridSize-RadT)) then
EdgeCase = .TRUE.
elseif (TempY >= GridSize-RadT) then
TopCase = .TRUE.
end if
if (EdgeCase .eqv. .TRUE.) then! Does the same as above but resting the particle against the edge attached to the first particle

NewX = TempX
Dist $=\operatorname{MLr}($ FinalPart $(1,1))$

New $Y$
(MlxReal(FinalPart( 1,1 ))**2)+(2*MlxReal(FinalPart( 1,1 ))*NewX)
NewY $=$ NewY $+($ Dist**2)-(NewX**2)
New $\mathrm{Y}=\operatorname{sqrt}($ New Y$)$
if (NewY /= NewY) then MoINo = MoINo - 1 GO TO 10
end if
if (TempY - (MlyReal(FinalPart(1,1)) + NewY) < TempY (MlyReal(FinalPart(1,1)) - NewY)) then

New $Y=\operatorname{MlyReal}($ FinalPart $(1,1))+$ New $Y$
else
NewY = MlyReal(FinalPart(1,1)) - NewY
end if
elseif (TopCase .eqv. .TRUE.) then
NewY = TempY
Dist $=\operatorname{MLr}($ FinalPart $(1,1))!$ Does the same as above but resting the particle against the roof of the box attached to the first particle

NewX =
(MlyReal(FinalPart(1,1))**2)+(2*MlyReal(FinalPart(1,1))*NewY)
NewX = NewX+(Dist**2)-(New $\left.{ }^{* *} 2\right)$
NewX $=\operatorname{sqrt}($ New $X)$
if (NewX /= NewX) then
MoINo $=$ MoINo -1
GO TO 10
end if
if (TempX - (MlxReal(FinalPart(1,1)) + NewX) < TempX -
(MlxReal(FinalPart(1,1)) - NewX)) then
NewX $=$ MlxReal(FinalPart(1,1)) + NewX
else
NewX $=$ MlxReal(FinalPart(1,1)) - NewX
end if
else! Does the same as above resting the particle against a particle while still being attached to the first particle

```
newCoords = 0
stochDists = 0
sumDist = 0
dx = 0
stochxnew = 0
ibad = 0
newCoords(1) = TempX
newCoords(2) = TempY
stochDists(1) = FinalPart(1,3)
stochDists(2) = FinalPart(2,3)
sumDist = stochDists(1) + stochDists(2)
```

```
    dx(1) = 10 * RadLarge
    dx(2) = 10 * RadLarge
    do a = 1, 10
        do b = 1, 2
            dx(b) = dx(b) / 10
        end do
        do c = 1,500
            call random_number(RX)
            stochxnew(\overline{2})= newCoords(2) + dx(2) * ((2*RX)-1)
            call random_number(RX)
            stochxnew(1) = newCoords(1) + dx(1) * ((2*RX)-1)
            ibad = 0
            stochDists(1) = ((PartCoords(1,1)-
stochxnew(1))**2)+((PartCoords(1,2)-stochxnew(2))**2)
                            stochDists(1) = sqrt(stochDists(1)) -
MLr(FinalPart(1,1))
    if (stochDists(1) < 0) then
                            ibad = 1
                            end if
                            stochDists(2) = ((PartCoords(2,1)-
stochxnew(1))**2)+((PartCoords(2,2)-stochxnew(2))**2)
                            stochDists(2) = sqrt(stochDists(2)) - RadT -
MLr(FinalPart(2,1))
                            if (stochDists(2) < 0) then
                            ibad = 1
                            end if
                            stochynew = stochDists(1) + stochDists(2)
                    if ((stochynew < sumDist) .and. (ibad== 0)) then
                                    do b=1, 2
                                    newCoords(b) = stochxnew(b)
            end do
                        sumDist = stochynew
                    end if
                        end do
            end do
                            ContPoint = FinalPart(2,1)
                            NewX = newCoords(1)
                            NewY = newCoords(2)
                            end if
                            if ((NewX > GridSize-RadT) .or. (NewX < RadT) .or. (NewY > GridSize-RadT)
.or. (NewY < RadT)) then
                            if (EdgeCase .eqv. .FALSE.) then
                        EdgeCase = .TRUE.
    end if
    MoINo = MolNo - 1
    GO TO 10
    end if
    do a = 1, MolNo-2
    Dist = ((MlxReal(a)-NewX)*2})+((\mathrm{ MlyReal(a)-NewY)**2)
```

.TRUE.) then

```
Dist \(=\) sqrt(Dist
if (Dist < MLr(a)+RadT) then
    OverlapCount \(=\) OverlapCount +1
    if (OverlapCount > 2500) then
        if (Tilt .eqv. .FALSE.) then
            OverlapCount \(=0\)
            if ( \(\mathrm{LRNo}==1\) ) then
                                    LRNo = 2
            else
                        LRNo = 1
                end if
                Tilt = .TRUE.
                GO TO 14
                end if
                MolNo = MolNo - 1
                if ((AdjCount < 75) .and. (AdjCount > -75)) then
                    AdjCount = AdjCount - LR
                    HMAdju = .TRUE
                    GO TO 19
                            elseif (AdjCount < -75 .and. Downwards .eqv.
                    Downwards = .FALSE.
                    AdjCount \(=0\)
                        LR = 1
                    GO TO 19
                elseif (AdjCount > 75 .and. Upwards .eqv. .TRUE.)
```

then
Downwards = .TRUE.
AdjCount $=0$
$L R=-1$
GO TO 19
else
GO TO 10
end if
GO TO 10
end if
FinalPart(2,1) = a
GO TO 60
FullCount $=$ FullCount +1
MoINo $=$ MoINo -1
GO TO 10
end if
end do

MlxReal(MolNo) $=$ NewX! Saves the second particle in the chain
MlyReal(MolNo) $=$ NewY
MLr(MolNo) $=$ RadT
FullCount = 0
MoINo = MolNo + 1
ChainStartNo $=$ MolNo-2 ! If the requested chain length is longer than 2 then the following code is done

ChainStartCont = MolNo-1
CSCy = MlyReal(ChainStartCont)
CSCx = NewX
do $\mathrm{a}=1$, ChainLength -2 ! Loops for the chain particles beyond the first two
OverlapCount $=0$
ChainGrad $=($ MlyReal(ChainStartCont) - MlyReal(ChainStartNo)) $/$ (MlxReal(ChainStartCont) - MIxReal(ChainStartNo))

EquC $=$ MlyReal(ChainStartCont) - (ChainGrad * MIxReal(ChainStartCont))
if (MlxReal(ChainStartCont) - MlxReal(ChainStartNo) $==0$ ) then! If particle is vertical then places the new one on top

NewX = MIxReal(ChainStartNo)
NewY = MlyReal(ChainStartNo+a) + RadT
else ! Otherwise works out the gradient and then angle of the 2 particle chain to add the following particles onto

NewX $=$ RadT $/\left(\operatorname{sqrt}\left(\left(\right.\right.\right.$ ChainGrad $\left.\left.\left.^{* *} 2\right)+1\right)\right)$
New $Y=($ ChainGrad * NewX)
if (MIxReal(ChainStartCont) < MIxReal(ChainStartNo)) then
if (MlyReal(ChainStartCont) >
MlyReal(ChainStartNo)) then

$$
\begin{aligned}
\text { New } X & =\text { MlxReal(MoINo-1) }- \text { NewX } \\
\text { NewY } & =\text { MlyReal(MolNo-1) }- \text { New } Y \\
\text { else } \quad \text { New } X & =\text { MlxReal(MoINo-1) }- \text { NewX } \\
\text { New } Y & =\text { MlyReal(MoINo-1) }- \text { New } Y
\end{aligned}
$$

else
end if
then
if (MlyReal(ChainStartCont) >
MlyReal(ChainStartNo)) then

CONTINUE
ChainHitCheck = .FALSE.
ChainEdgeHitCheck = .FALSE.
ChainTopHitCheck = .FALSE.
ChainHitLoop: do $b=1$, MoINo $-\mathrm{a}-2 \quad$ ! Checks if the new part of the chain is overlapping with anything

Dist $=\left((\text { MlxReal }(\mathrm{b})-\text { NewX })^{* *} 2\right)+\left((\right.$ MlyReal $(\mathrm{b})-$ NewY $\left.){ }^{* *} 2\right)$
Dist $=$ sqrt(Dist)
if (Dist < ((RadT) $+(\operatorname{Mlr}(\mathrm{b})))$ ) then
ChainHitCheck = .TRUE.
PartHit $=\mathrm{b}$
end if
end do ChainHitLoop

CONTINUE
if ((NewX > GridSize-RadT) .or. (NewX < RadT)) then! Checks if the new part of the chain is outside of the box

ChainEdgeHitCheck = .TRUE.
elseif (New $Y>$ GridSize-RadT) then
ChainTopHitCheck = .TRUE.
end if
if (ChainHitCheck .eqv. .TRUE.) then ! If overlapping then the particle moves to be resting upon the particle it is overlapping

```
if (OverlapCount > 2500) then
    MoINo = MoINo - a
    if (Tilt .eqv. .FALSE.) then
            OverlapCount = 0
            if (LRNo == 1) then
                LRNo = 2
            else
                LRNo = 1
            end if
                    Tilt = .TRUE.
                    GO TO 14
    end if
    MoINo = MolNo - 1
    if ((AdjCount < 75) .and. (AdjCount > -75)) then
            AdjCount = AdjCount - LR
            HMAdju = .TRUE.
            GO TO 19
    elseif (AdjCount < -75 .and. Downwards .eqv.
                                    Downwards = .FALSE.
                    AdjCount = 0
            LR = 1
            GO TO 19
    elseif (AdjCount > 75 .and. Upwards .eqv. .TRUE.)
```

then

```
                                    Downwards = .TRUE.
                                    AdjCount = 0
                                    LR = -1
                                    GO TO 19
            GO TO 10
```

    else
    end if
    GO TO 10
    end if
newCoords = 0
stochDists $=0$
sumDist $=0$
$\mathrm{dx}=0$
stochxnew $=0$
ibad $=0$
newCoords(1) = NewX
newCoords(2) $=$ New $Y$

```
stochDists(1) = Dist
stochDists(2) \(\quad=\quad((\) MlxReal \((\) MoINo-a-1 \()\) -
```

NewX)**2)+((MlyReal(MolNo-a-1)-NewY)**2)
stochDists(2) = sqrt(stochDists(2))
sumDist $=$ stochDists(1) + stochDists(2)
$\mathrm{dx}(1)=10$ * RadLarge
$\mathrm{dx}(2)=10$ * RadLarge
do $b=1,10$
do $\mathrm{c}=1,2$
dx © $=$ (C)(c) / 10
end do
do $c=1,500$
call random_number(RX)
stochxnew $(2)=$ newCoords(2) $+d x(2)$ *
((2*RX)-1)
call random_number(RX)
stochxnew(1) $=$ newCoords(1) $+d x(1)$ *
((2*RX)-1)
ibad $=0$
stochDists(1) $=\quad($ MLxReal(PartHit $)-$
stochxnew(1))**2)+((MLyReal(PartHit)-stochxnew(2))**2)
stochDists(1) = sqrt(stochDist-(1)) - (-adT) -
(MLr(PartHit))
if (stochDists $(1)<0)$ then
ibad = 1
end if
stochDists(2) $=((M L x R e a l(M o l N o-a-1)-$
stochxnew(1))**2)+((MLyReal(MoINo-a-1)-stochxnew(2))**2)
stochDists(2) = sqrt(stochDist-(2)) - ((a+1) *
RadT)
if (stochDists $(2)<0)$ then
ibad = 1
end if
stochynew $=$ stochDists(1) + stochDists(2)
if ((stochynew < sumDist) .and. (ibad == 0))
then
stochxnew(d)

```
                                    do \(d=1,2\)
                                    newCoords(d) =
                                    end do
                                    sumDist = stochynew
                                    end if
                            end do
                                    end do
                                    ContPoint \(=\) PartHit
                                    NewX = newCoords(1)
                                    NewY = newCoords(2)
                            if (NewY < MLyReal(PartHit)) then
```




```
                            GO TO 10
end if
if (NewX > GridSize-RadT) then
    NewX = GridSize-RadT
elseif (NewX < RadT) then
            NewX = RadT
end if
Dist \(=(a+1) *\) RadT
New \(Y=-\left(\right.\) MLxReal(MolNo-a-1)**2) \(+\left(2^{*}\right.\) MLxReal(MolNo-a-
NewY \(=\) NewY \(+\left(\right.\) Dist \(\left.^{* *} 2\right)-\left(\right.\) New \(\left.{ }^{* *}{ }^{*} 2\right)\)
New \(Y=\operatorname{sqrt}(\) New \(Y\) )
if (NewY /= NewY) then
    \(\mathrm{MolNo}=-\mathrm{olN}-\mathrm{-a}-1\)
    GO TO 10
end if
if (-empy - (MLyReal(MolNo-a-1) + NewY) < -empy -
            New \(Y=\) MLyReal(MolNo-a-1) + New \(Y\)
else
    NewY \(=\) MLyReal(MolNo-a-1) - New \(Y\)
end if
do \(b=1,-o \mid N o-a-2\)
    Dist \(=\left((\text { MLxReal(b)-NewX })^{* *} 2\right)+((\) MLyReal \((b)-\)
    Dist \(=\) sqrt(Dist)
    if (Dist < ((RadT) \(+(\operatorname{Mlr}(\mathrm{b})))\) ) then
        ChainHitCheck = .TRUE.
        PartHit = b
        OverlapCount \(=\) OverlapCount +1
        GO TO 99
    end if
end do
    ChainGrad \(=-\) New \(Y-\) MLyReal(ChainStartNo)) \(/-\) NewX -
EquC \(=-\) New - (ChainGrad *NewX)
CSCy = NewY
CSCx = NewX
```

(MLyReal(MolNo-a-1) - NewY)) then
NewY)**2)
MLxReal(ChainStartNo))
do $d=1$, $a!$ The previous particle in the chain are moved to be in line with the fixed location of the new particle

OverlapCount $=0$
if - NewX - MLxReal(ChainStartNo) $==0$ ) then MLxReal(MoINo-d) $=$ NewX CSCy =-CSCy - RadT MLyReal(MoINo-d) = CSCy
else
MLxReal(MolNo-d) $=$ RadT
(sqrt((ChainGrad**2) +1 ) $)$
MLyReal(MolNo-d) $=$ (ChainGrad
MLxReal(MolNo-d))

# if (NewX < MLxReal(ChainStartNo)) then CSCy = CScy + MLyReal(MoINo-d) CSCx = CScx + MLxReal(MoINo-d) MLxReal(MolNo-d) = CSCx MLyReal(MolNo-d) = CSCy <br> elseif (NewX > MLxReal(ChainStartNo)) 

then
CSCy =-CScy - MLyReal(MoINo-d)
CSCx =-CScx - MLxReal(MoINo-d)
MLxReal(MolNo-d) = CSCx
MLyReal(MolNo-d) = CSCy
end if
end if
end do
elseif (ChainTopHitCheck .eqv. .TRUE.) then! If the particle is over the top of the box it is moved to be resting against it

OverTopCount $=$ OverTopCount +1
if (OverlapCount $>2500$ ) then
MolNo $=-\mathrm{OIN}-\mathrm{a}-1$
GO TO 10
end if
if (OverTopCount > 2500) then
MoINo $=-\mathrm{OlN}-\mathrm{a}-1$
GO TO 10
end if
NewY = GridSize-RadT
Dist $=(a+1)^{*}$ RadT
NewX $=-($ MLyReal(MolNo-a-1)**2)+(2*MLyReal(MoINo-a-
1)*New Y )

NewX $=$ NewX $+\left(\right.$ Dist $\left.^{* *} 2\right)-\left(\right.$ New $^{* * * 2)}$
New $X=\operatorname{sqrt}($ New $X)$
if (NewX /= NewX) then
$\mathrm{MolNo}=-\mathrm{olN}-\mathrm{a}-1$
GO TO 10
end if
if (-empx - (MLxReal(MolNo-a-1) + NewX) < -empx -
(MLxReal(MolNo-a-1) - NewX)) then
NewX $=$ MLxReal(MolNo-a-1) + NewX
else
NewX = MLxReal(MolNo-a-1) - NewX
end if

```
do \(b=1,-o l N o-a-2\)
Dist \(=\left((\text { MLxReal(b)-NewX })^{* *} 2\right)+((\) MLyReal \((\mathrm{b})-\)
```

NewY)**2)
Dist $=$ sqrt(Dist)
if (Dist < ((RadT) $+(\operatorname{Mlr}(\mathrm{b})))$ ) then
ChainHitCheck = .TRUE.
PartHit = b
OverlapCount $=$ OverlapCount +1
GO TO 99
end if

elseif (AdjCount > 75 .and. Upwards .eqv.
.TRUE.) then

```
                        Downwards = .TRUE.
                        AdjCount = 0
        LR = -1
        GO TO 19
        else
        GO TO 10
        end if
        end if
        end do
    end do
    if (NewY > GridSize-RadT) then
        RoofCount = RoofCount +1
        MoINo =-olN--a-1
        GO TO 10
    elseif ((NewX > GridSize-RadT) .or. (NewX < RadT)) then
        MoINo = -olN-- a-1
        GO TO 10
    end if
```

    MLxReal(MolNo) \(=\) NewX! Saves the particle location and loops to
    the next particle in the chain to be added if there are any left
MLyReal(MoINo) $=$ New $Y$
MLr(MoINo) = RadT
FullCount = 0
MoINo $=$ MoINo +1
end do
if ((MLxReal(MolNo-1) <= RadT+0.2) .or. (MLxReal(MoINo-1) >= GridSize-

RadT-0.2)) then
GO TO 10
end if
if $(\operatorname{MOD}($ ChainLength,2 $)==0)$ then ! Determines the centre point of the chain for determining balance

MiddlePartA = -olNo - ((ChainLength/2)+1)
MiddlePartB = -olNo - ((ChainLength/2))
MiddlePoint $=(($ MLxReal $($ MiddleP-rta $)-$ MLxReal $($ MiddlePartB $)) / 2)+$
MLxReal(MiddlePartB)
elseif (MOD(ChainLength,2) $==1$ ) then
MiddlePart = olNo - ((ChainLength/2)+1)
MiddlePoint $=$ MLxReal(MiddlePart)
end if
do $m=$ MolNo-ChainLength, MolNo-1! Determines furthest point of contact along the chain Dist $=\left((\operatorname{MLxReal}(\mathrm{m})-\mathrm{MLxReal}(\text { ContPoint }))^{* *} 2\right)+(($ MLyReal $(\mathrm{m})-$ MLyReal(ContPoint))**2)

Dist $=$ sqrt(Dist)
if (Dist $<=(\operatorname{MLr}(\mathrm{m})+\mathrm{MLr}($ ContPoint $)+0.1))$ then
ContDist $=$ Dist
ContPointB $=\mathrm{m}$
end if
end do

```
    ContSpot = 0
    OuterCPLoopA: do m = MoINo-1, MolNo-ChainLength, -1
        do n = 1, -olN- - a - 2
            Dist = ((MLxReal(m)-MLxReal(n))**2)+((MLyReal(m)-
MLyReal(n))**2)
    Dist = sqrt(Dist)
        if (Dist < MLr(m)+MLr(n)+0.1) then
    if (MLxReal(MolNo-1) > MLxReal(ChainStartNo))
then
                                ContSpotTemp = ((MLxRe-I(n)
MLxReal(m))/2) + MLxReal(m)
ContSpot)) then
                                if ((ContSpot == 0) .or. (ContSpotTemp >
                                    ContSpot = ContSpotTemp
                                    ContPoint = n
                                    ContPointB = m
        end if
    else
        ContSpotTemp = ((MLxRe-l(n)
MLxReal(m))/2) + MLxReal(m)
ContSpot)) then
                                if ((ContSpot == 0) .or. (ContSpotTemp <
                                    ContSpot = ContSpotTemp
                                    ContPoint = n
                                    ContPointB = m
                                    end if
                                    end if
                end if
            end do
        end do OuterCPLoopA
    ContSpot = ((MLxReal(ContP-int) - MLxReal(ContPointB))/2) +
MLxReal(ContPointB)
if ((MLxReal(MolNo-1) > MLxReal(ChainStartNo)) .and. (MiddlePoint > ContSpot)) then! Checks that contact points on the chain are in the correct positions for chain balance

\section*{CONTINUE}
```

x = MLxReal(MolNo-1)

```
x = MLxReal(MolNo-1)
FallPoint = MLyReal(MolNo-1)
FallPoint = MLyReal(MolNo-1)
MolNo = -olNo - ChainLength
MolNo = -olNo - ChainLength
Fell = .TRUE.
Fell = .TRUE.
if (FallCount < 10) then
if (FallCount < 10) then
    FallCount = FallCount +1
    FallCount = FallCount +1
    GO TO 40
    GO TO 40
else
else
                            if ((AdjCount < 75) .and. (AdjCount > -75)) then
                            if ((AdjCount < 75) .and. (AdjCount > -75)) then
                            AdjCount = Adj-ount - LR
                            AdjCount = Adj-ount - LR
                    HMAdju = .TRUE.
                    HMAdju = .TRUE.
                    GO TO 19
                    GO TO 19
                    elseif (AdjCount < -75 .and. Downwards .eqv. .TRUE.) then
                    elseif (AdjCount < -75 .and. Downwards .eqv. .TRUE.) then
                    Downwards = .FALSE.
                    Downwards = .FALSE.
                    AdjCount = 0
                    AdjCount = 0
                    LR = 1
                    LR = 1
                            GO TO 19
                            GO TO 19
                            elseif (AdjCount > 75 .and. Upwards .eqv. .TRUE.) then
```

                            elseif (AdjCount > 75 .and. Upwards .eqv. .TRUE.) then
    ```

Downwards = .TRUE.
AdjCount \(=0\)
LR = -1
GO TO 19
else
GO TO 10
end if
end if
elseif ((MLxReal(MolNo-1) < MLxReal(ChainStartNo)) .and. (MiddlePoint < ContSpot)) then

\section*{CONTINUE}
x = MLxReal(MolNo-1)
FallPoint \(=\) MLyReal(MoINo-1)
MolNo = -olNo - ChainLength
Fell = .TRUE .
if (FallCount < 10) then
FallCount \(=\) FallCount +1
GO TO 40
else
if ((AdjCount < 75) .and. (AdjCount > -75)) then
AdjCount = Adj-ount - LR
HMAdju = .TRUE .
GO TO 19
elseif (AdjCount <-75 .and. Downwards .eqv. .TRUE.) then Downwards = .FALSE.
AdjCount \(=0\)
LR = 1
GO TO 19
elseif (AdjCount > 75 .and. Upwards .eqv. .TRUE.) then Downwards = .TRUE.
AdjCount \(=0\)
LR = -1
GO TO 19
else
GO TO 10
end if
end if
end if
ContSpotL \(=0\)
ContSpotR = 0
ContSpotUy \(=0\)
ContSpotUx = 0
ContSpotUn = 0
do \(m=\) MolNo-1, MoINo-ChainLength, -1
do \(\mathrm{n}=1\), \(-\mathrm{olN}-\mathrm{-a}-2\)
Dist \(=\left((\operatorname{MLxReal}(m)-M L x R e a l(n))^{* *} 2\right)+((\operatorname{MLyReal}(m)-\)
MLyReal(n)) \({ }^{* *} 2\) )
Dist \(=\) sqrt(Dist)
if (Dist \(<\operatorname{MLr}(\mathrm{m})+\mathrm{MLr}(\mathrm{n})+0.1)\) then
ContPoint \(=\mathrm{n}\)
ContSpotTemp \(=\quad((\) MLxReal \((\) ContP-int \()\)
\(\operatorname{MLxReal}(m)) / 2)+\operatorname{MLxReal}(m)\)
ContSpotL)) then

ContSpotR)) then

MLyReal(m))/2) + MLyReal(m)
> ContSpotUy)) then
end if
if ((ContSpotR \(==0)\).or. (ContSpotTemp > ContSpotR = ContSpotTemp
end if
ContSpotTempUy \(=\) ((MLyReal(ContP-int) -
if ( \(\mathrm{m} /=-\mathrm{olNo}\) - ChainLength) then if ((ContSpotUy ==0) .or. (ContSpotTempUy
end if end if
end if end do end do
do \(m=\) MolNo-1, MolNo-ChainLength+1, -1 do \(\mathrm{n}=1\), \(-\mathrm{olN}-\mathrm{-a}-2\)

Dist \(=\left((\operatorname{MLxReal}(\mathrm{m})-\mathrm{MLxReal}(\mathrm{n}))^{* *} 2\right)+((\operatorname{MLyReal}(\mathrm{m})-\)
MLyReal(n))**2)
Dist \(=\) sqrt(Dist)
if (Dist \(<\operatorname{MLr}(\mathrm{m})+\mathrm{MLr}(\mathrm{n})+0.1\) ) then
ContSpotTemp \(=((\operatorname{MLxRe}-I(n)-\operatorname{MLxReal}(m)) / 2)+\)
MLxReal(m)
if ((MLxReal(MoINo-1) > MLxReal(MoINo-
ChainLength)) .and. (ContSpotTemp > MLxReal(m))) then
elseif ((MLxReal(MolNo-1) < MLxReal(MolNoChainLength)) .and. (ContSpotTemp < MLxReal(m))) then

SideBal = .TRUE.
end if
end if
end do
end do
if (MLxReal(MoINo-1) > MLxReal(MolNo-ChainLength)) then! If the particle is not balancing correctly, the algorithm goes back to the beginning, however the initial falling point is moved to the end of this chain
if ((ContSpotL > MLxReal(MoINo-ChainLength)) .or. (SideBal .eqv.
.FALSE.)) then
if
((MLxReal(MolNo-ChainLength).GT.MLr(MoINo-
ChainLength)+0.2).and.(MLyReal(MolNo-ChainLength)/=MLyReal(MolNo-1))) then
NLCount = NLCount + 1
OverlapCount \(=0\)
if ( \(\mathrm{LRNo}==1\) ) then
LRNo = 2
else
\(\mathrm{LRNo}=1\)
end if
Tilt = .TRUE.
MolNo = MolNo-a
GO TO 14
end if
end if
elseif (MLxReal(MolNo-1) < MLxReal(MolNo-ChainLength)) then if ((ContSpotR < MLxReal(MolNo-ChainLength)) .or. (SideBal .eqv.
.FALSE.)) then
if ((MLxReal(MolNo-ChainLength)/=GridSize-MLr(MoINo-
ChainLength)).and.(MLyReal(MoINo-ChainLength)/=MLyReal(MoINo-1))) then
NLCount = NLCount + 1
OverlapCount \(=0\)
if ( \(\mathrm{LRNo}==1\) ) then
LRNo = 2
else
LRNo \(=1\)
end if
Tilt = .TRUE. MolNo = MolNo - a GO TO 14
end if
end if
end if
if \((\) MLyReal(MoINo-ChainLength \()>\) MLyReal(MolNo-1)) then
if (MLxReal(MoINo-1) > MLxReal(MoINo-ChainLength)) then
GO TO 21
elseif (MLxReal(MolNo-1) < MLxReal(MoINo-ChainLength)) then GO TO 22
end if
end if
CONTINUE
if ((MinFallCount > FallCount) .or. (MinFallCount == 0)) then
MinFallCount = FallCount
end if
else
Full = 1
end if
end
subroutine PointSafe! Determines if the falling particle has impacted yet
use allSubs ! Loads the variables from the module
integer a, b, CoordX, CoordY
real Dist
character t

Hit = .FALSE.
FullCheck \(=\).FALSE.
! Checks the distance between the current falling particle location and previously placed partice to determine if it has impacted
```

cloop: do a = 1, MolNo - 1
Dist = ((MLxReal(a)-x)**2)+((MLyReal(a)-y)**2)
Dist = sqrt(Dist)
if (Dist <= ((RadT)+(Mlr(a)))) then

```

Hit = .TRUE.
exit cloop
end if
end do cloop
! If the impact is above the top of the box, a counter is incremented to show the box may be full
if ((Hit .eqv. .TRUE.) .and. ( \(y>=(\) GridSize - RadT \()\) )) then
Hit = .FALSE.
FullCount \(=\) FullCount +1
RoofCount \(=\) RoofCount +1
end if
if (RoofCount >=1000) then
FullCheck = .TRUE.
end if
if (FullCount \(==2500000\) ) then
Full = 1
end if
end
subroutine AddChain()! This subroutine performs the exact same function as the main particle chain adding code, however is used for the chains placed along the base layer use allsubs
integer count2, Spot, Height, DoubRad, RowRad, a,b,c, Radln, m, n, TempX, TempY real MidWay, Dist
character t, FileName*15
integer SavIncremX, SavIncremY, SafeLocCount, LR, SavOneX, SavOneY, SavDist, SavOnePart, LRNo, OneCount, RealPos1, RealPos2
integer TempRealPos1, TempRealPos2, ChainOneCount
logical SafeLocFound, Go, ResetCheck
real TempXa, TempXb, TempYa, TempYb, DistAB, DistBC, DistAC, AngleA, AngleB, AngleFin, GradFin, HelpDist
real FDistA, FDistB, FDistC, FDistD
real xDiff, yDiff, Pi, FinalSavX, FinalSavY
integer FinalSavLong, FinalSavTall, checktime, Balanced
integer Balances, Touches
dimension Balances(10)
real DistFac, RadScale
integer NewPos, TRP1Swap, TRP2Swap
integer FinalPart, SideCount
dimension FinalPart( 2,3 )
real PartCoords, stochDists, sumDist, dx, stochxnew, newCoords, stochynew
integer ibad
dimension PartCoords(2,2), stochDists(2), newCoords(2), dx(2), stochxnew(2)
real RX, NewX, NewY
logical ChainAdd
real OverDist
integer OverDistNo
logical NotBal, FirstBal
dimension BalCheckNo(10000), BalCombi(100000,2)
integer BalCheckCount, BalCount, BalCheckNo, BalCombi, BalAttempt
integer OverlapCount
```

integer ChainStartNo, ChainStartCont, d
real ChainGrad, EquC
logical ChainHitCheck, ChainEdgeHitCheck, ChainTopHitCheck
logical TopCase
integer OverTopCount, PartHit
Hit = .FALSE.
ResetCheck = .FALSE.
checktime = 1
Balanced $=0$
Touches = 0
Balances = 0
FinalPart $=999999$
OverDist = 0
OverDistNo = 0
OverlapCount $=0$
TRP1Swap = 0
TRP2Swap = 0
ChainAdd = .FALSE.
ChainOneCount = 1
NotBal = .FALSE.
FirstBal = .TRUE.
BalCheckNo = 0
BalCombi = 0
BaICheckCount $=0$
BalCount = 0
BalCheckNo = 0
BalCombi = 0
BalAttempt $=0$
RadScale = 0
TempRealPos1 $=0$
TempRealPos2 $=0$
DistFac = 0
FDistA = 0
FDistB $=0$
FDistC $=0$
FDistD = 0
SavDist = 0
SavOneX = 0
SavOneY = 0
TempXa = 0
TempXb = 0
TempYa $=0$
TempYb = 0
DistAB = 0
DistBC $=0$
DistAC $=0$
AngleA $=0$
AngleB $=0$
AngleFin $=0$
GradFin $=0$

```
```

$x$ Diff $=0$
$y$ Diff $=0$
$\mathrm{Pi}=3.141596535$
NewPos = 0
FinalDists $=0$
PartCoords = 0
stochDists $=0$
sumDist $=0$
$\mathrm{dx}=0$
stochxnew = 0
newCoords $=0$
stochynew $=0$
RA = "
OverlapCount $=0$
do $\mathrm{a}=1$, MolNo -1
MLxCor $=$ MLxReal(a)
MLyCor $=$ MLyReal(a)
Radln = MLr(a)
DoubRad $=($ Radln + RadT $)+1$
if ( $\mathrm{a} /=\mathrm{MolNo}$-1) then
do Height $=0$, DoubRad
MidWay $=$ DoubRad**2 - Height**2
RowRad = abs(sqrt(Midway))
do count2 $=-$ rowrad +1 , rowrad-1
if

```
((MLyCor+count2<=GridSize).and.(MLxCor+Height<=GridSize-
RadT).and.(MLyCor+count2>=RadT).and.(MLxCor+Height>=RadT))then
                                    RA(MLyCor+count2, MLxCor+Height) = '-'
                                    end if
                                    if ((MLyCor+count2<=GridSize).and.(MLxCor-
Height<=GridSize-RadT).and.(MLyCor+count2>=RadT).and.(MLxCor-Height>=RadT))then
                                    RA(MLyCor+count2, MLxCor-Height) \(=\) ' - '
                                    end if
        end do
    end do
    do Height \(=-\) RadIn, RadIn
        do count2 \(=\) MlyCor-1, 1, -1
        if
((count2<=GridSize).and.(MLxCor+Height<=GridSize-
RadT).and.(count2>=RadT).and.(MLxCor+Height>=RadT))then
                                    RA(count2, MLxCor+Height) = '-'
                                    end if
        end do
        end do
    end if
    if ( \(\mathrm{a}==\) MolNo-1) then
        do Height \(=-\) Radln, 0
            MidWay = Radln**2 - Height**2
            RowRad = abs(sqrt(Midway))
if
((MLyCor+RowRad<=GridSize).and.(MLxCor+height<=GridSize-
RadT).and.(MLxCor+height>=RadT).and.(MLyCor+RowRad>=RadT))then
if (RA(MLyCor+RowRad, MLxCor+Height) /= '-') then
RA(MLyCor+RowRad, MLxCor+Height) = ' 1 '
end if
end if
if ((MLyCor-
RowRad>=RadT).and.(MLxCor+height<=GridSize-
RadT).and.(MLxCor+height>=RadT).and.(MLyCor-RowRad<=GridSize))then if (RA(MLyCor-RowRad, MLxCor+Height) /= '-') then RA(MLyCor-RowRad, MLxCor+Height) = '1' end if
end if
if ((MLyCor+RowRad<=GridSize).and.(MLxCor-
Height<=GridSize-RadT).and.(MLxCor-Height>=RadT).and.(MLyCor+RowRad>=RadT))then if (RA(MLyCor+RowRad, MLxCor-Height) /= '-') then

RA(MLyCor+RowRad, MLxCor-Height) = '1' end if
end if
if ((MLyCor-RowRad>=RadT).and.(MLxCor-height<=GridSize-RadT).and.(MLxCor-height>=RadT).and.(MLyCor-
RowRad<=GridSize))then
if (RA(MLyCor-RowRad, MLxCor-Height) /= '-') then
RA(MLyCor-RowRad, MLxCor-Height) = '1'
end if
end if end do
end if
end do
do \(\mathrm{a}=1\), GridSize
do \(b=1\), GridSize
if (RA(b,a) == ' 1 ') then
ChainOnes(ChainOneCount, 1) \(=b\)
ChainOnes(ChainOneCount, 2) \(=\mathrm{a}\)
ChainOneCount \(=\) ChainOneCount +1
end if
end do
end do
call random_number(RX)
LRNo \(=1+\) floor (2*RX)
if \((\mathrm{LRNo}==1)\) then
TempX = ChainOnes \((1,2)\)
TempY = ChainOnes(1,1)
elseif (LRNo == 2) then
TempX = ChainOnes(ChainOneCount-1,2)
TempY = ChainOnes(ChainOneCount-1,1)
end if
FinalPart = 99999
FinalPart \((1,1)=\) MolNo-1
Dist \(=\left((\text { MLxReal }(a)-\text { TempX })^{* *} 2\right)+((\) MLyReal \((a)-T e m p Y) * * 2)\)
Dist \(=\) sqrt(Dist) \(-\operatorname{MLr}(\mathrm{a})\)
FinalPart(1,2) = Dist
FinalPart \((1,3)=\) Dist \(+\operatorname{MLr}(\mathrm{a})\)
do \(\mathrm{a}=1\), MoINo-2
if (MLyReal(a) < TempY+1) then
Dist \(=((\) MLxReal(a)-TempX)**2)+((MLyReal(a)-TempY)**2) Dist = sqrt(Dist) - RadT - MLr(a) if (Dist <= FinalPart(2,2)) then
\[
\text { FinalPart }(2,1)=\mathrm{a}
\]

FinalPart(2,2) = Dist
FinalPart( 2,3 ) \(=\) Dist + RadT \(+\operatorname{MLr}(\mathrm{a})\)
end if
end if
end do
60
CONTINUE
PartCoords \((1,1)=\) MLxReal(FinalPart(1,1))
PartCoords \((1,2)=\) MLyReal(FinalPart(1,1))
PartCoords \((2,1)=\) MLxReal(FinalPart(2,1))
PartCoords(2,2) \(=\) MLyReal(FinalPart(2,1))
if \(((\) TempX \(==\) RadT). or. (TempX \(==\) GridSize-RadT) \()\) then
NewX = TempX
Dist \(=\operatorname{MLr}(\) FinalPart \((1,1))\)
New \(Y=-\left(\right.\) MLxReal(FinalPart(1,1))**2) \(+\left(2^{*}\right.\) MLxReal(FinalPart(1,1))*NewX)
New \(Y=\) New \(Y+\left(\right.\) Dist**2)-(New \(\left.{ }^{* *} 2\right)\)
New \(Y=\operatorname{sqrt}(\) New \(Y\) )
if (NewY /=NewY) then MolNo = MolNo-1 GO TO 10
end if
if (TempY - (MLyReal(FinalPart(1,1)) + NewY) < TempY
(MLyReal(FinalPart(1,1)) - NewY)) then New \(Y=\operatorname{MLyReal}(\) FinalPart \((1,1))+\) New \(Y\)
else
New \(Y=\operatorname{MLyReal}(\) FinalPart(1,1)) \(-\operatorname{New} Y\)
end if
else
newCoords(1) \(=\) TempX
newCoords(2) \(=\) TempY
stochDists(1) \(=\) FinalPart \((1,3)\)
stochDists(2) \(=\) FinalPart \((2,3)\)
sumDist \(=\) stochDists(1) + stochDists(2)
\(\mathrm{dx}(1)=10\) * RadLarge
\(d x(2)=10\) * RadLarge
do \(a=1,10\)
do \(b=1,2\)
\(d x(b)=d x(b) / 10\)
end do
do \(c=1,500\)
```

    call random_number(RX)
    stochxnew(2) = newCoords(2) + dx(2) * (2*RX-1)
    call random_number(RX)
    stochxnew(1) = newCoords(1) + dx(1) * (2*RX-1)
    ibad = 0
    stochDists(1) = ((PartCoords(1,1)-
    stochxnew(1))**2)+((PartCoords(1,2)-stochxnew(2))**2)
stochDists(1) = sqrt(stochDists(1)) - MLr(FinalPart(1,1))
if (stochDists(1) < 0) then
ibad = 1
end if
stochDists(2) = ((PartCoords(2,1)-
stochxnew(1))**2)+((PartCoords(2,2)-stochxnew(2))**2)
stochDists(2) = sqrt(stochDists(2)) - RadT
MLr(FinalPart(2,1))
if (stochDists(2) < 0) then
ibad = 1
end if
stochynew = stochDists(1) + stochDists(2)
if ((stochynew < sumDist) .and. (ibad == 0)) then
do b=1, 2
newCoords(b) = stochxnew(b)
end do
sumDist = stochynew
end if
end do
end do
NewX = newCoords(1)
NewY = newCoords(2)
end if
if ((NewX > GridSize-RadT) .or. (NewX < RadT) .or. (NewY > GridSize-RadT) .or.
(NewY < RadT)) then
MolNo = MolNo-1
GO TO 10
end if
do a = 1, MolNo-2
Dist = ((MLxReal(a)-NewX)**2)+((MLyReal(a)-NewY)**2)
Dist = sqrt(Dist)
if (Dist < MLr(a)+RadT) then
OverlapCount = OverlapCount + 1
if (OverlapCount > 2500) then
MoINo = MoINo-1
GO TO 10
end if
FinalPart(2,1) = a
GO TO 60
FullCount = FullCount +1
MolNo = MolNo-1

```

GO TO 10
end if
end do
MLxReal(MoINo) \(=\) New \(X\)
\(\operatorname{MLyReal}(\mathrm{MolNo})=\) New \(Y\)
MLr(MolNo) = RadT
FullCount = 0
MoINo \(=\) MoINo +1
ChainStartNo = MoINo-2
ChainStartCont \(=\) MoINo-1
CSCy = MLyReal(ChainStartCont)
do \(\mathrm{a}=1\), ChainLength -2
OverlapCount \(=0\)
ChainGrad \(=(\) MLyReal(ChainStartCont) - MLyReal(ChainStartNo)) /
(MLxReal(ChainStartCont) - MLxReal(ChainStartNo))
EquC = MLyReal(ChainStartCont) - (ChainGrad * MLxReal(ChainStartCont))
if (MLxReal(ChainStartCont) - MLxReal(ChainStartNo) \(==0\) ) then
NewX = MLxReal(ChainStartCont)
CSCy = CSCy + RadT
NewY = CSCy
else
NewX \(=\) RadT \(/\left(\operatorname{sqrt}\left(\left(\right.\right.\right.\) ChainGrad**2 \(\left.\left.\left.^{*}\right)+1\right)\right)\)
NewY = (ChainGrad * NewX)
if (MLxReal(ChainStartCont) < MLxReal(ChainStartNo)) then
NewX = MLxReal(MolNo-1) - NewX
NewY = MLyReal(MolNo-1) - NewY
elseif (MLxReal(ChainStartCont) > MLxReal(ChainStartNo)) then New \(X=\) MLxReal(MoINo-1) + New \(X\)
New \(Y=\) MLyReal(MoINo-1) + New \(Y\)
end if
end if
ChainHitCheck = .FALSE.
ChainEdgeHitCheck = .FALSE.
ChainTopHitCheck = .FALSE.
ChainHitLoop: do \(b=1\), MoINo \(-\mathrm{a}-2\)
Dist \(=\left((\text { MLxReal }(b)-\text { NewX })^{* *} 2\right)+((\) MLyReal \((b)-N e w Y) * * 2)\)
Dist \(=\) sqrt(Dist)
if (Dist < ((RadT) \(+(\operatorname{Mlr}(\mathrm{b})))\) ) then
ChainHitCheck = .TRUE.
PartHit = b
end if
end do ChainHitLoop
CONTINUE
if ((NewX > GridSize-RadT) .or. (NewX < RadT)) then
ChainEdgeHitCheck = .TRUE.
elseif (NewY > GridSize-RadT) then
ChainTopHitCheck = .TRUE.
end if
```

            if (ChainHitCheck .eqv. .TRUE.) then
            if (OverlapCount > 2500) then
                MoINo = MolNo - a-1
                GO TO 10
    end if
    newCoords(1) = NewX
    newCoords(2) = NewY
    stochDists(1) = Dist
    stochDists(2) =
                                    ((MLxReal(MolNo-a-1)-
    NewX)**2)+((MLyReal(MoINo-a-1)-NewY)**2)
stochDists(2) = sqrt(stochDists(2))
sumDist = stochDists(1) + stochDists(2)
dx(1) = 10 * RadLarge
dx(2) = 10 * RadLarge
do b=1,10
do c=1,2
dx(c) = dx(c) / 10
end do
do c=1,500
call random_number(RX)
stochxnew(2) = newCoords(2) + dx(2) * (2*RX-1)
call random_number(RX)
stochxnew(1) = newCoords(1) + dx(1) * (2*RX-1)
ibad = 0
stochDists(1) = ((MLxReal(PartHit)-
stochxnew(1))**2)+((MLyReal(PartHit)-stochxnew(2))**2)
stochDists(1) = sqrt(stochDists(1)) - RadT -
MLr(PartHit)
if (stochDists(1) < 0) then
ibad = 1
end if
stochDists(2) = ((MLxReal(MolNo-a-1)-
stochxnew(1))**2)+((MLyReal(MoINo-a-1)-stochxnew(2))**2)
stochDists(2) = sqrt(stochDists(2)) - ((a+1) * RadT)
if (stochDists(2) < 0) then
ibad = 1
end if
stochynew = stochDists(1) + stochDists(2)
if ((stochynew < sumDist) .and. (ibad == 0)) then
do d=1,2
newCoords(d) = stochxnew(d)
end do
sumDist = stochynew
end if
end do
end do
NewX = newCoords(1)

```
```

NewY = newCoords(2)
if (NewY < RadT) then
NewY = RadT
NewX = MLxReal(MolNo-1) + RadT
end if
do b = MolNo - a-2, 1, -1
Dist = ((MLxReal(b)-NewX)**2)+((MLyReal(b)-NewY)**2)
Dist = sqrt(Dist)
if (Dist < ((RadT)+(Mlr(b)))) then
ChainHitCheck = .TRUE.
PartHit = b
OverlapCount = OverlapCount +1
GO TO 99
end if
end do
if ((NewX < RadT) .or. (NewX > GridSize - RadT)) then
ChainHitCheck = .FALSE.
ChainEdgeHitCheck = .TRUE.
GO TO 99
end if
if (NewY > GridSize - RadT) then
ChainHitCheck = .FALSE.
ChainTopHitCheck = .TRUE.
GO TO 99
end if
ChainGrad = (NewY - MLyReal(ChainStartNo)) / (NewX -
MLxReal(ChainStartNo))
EquC = NewY - (ChainGrad *NewX)
CSCy = NewY
CSCx = NewX
do d=1,a
OverlapCount = 0
if (NewX - MLxReal(ChainStartNo) == 0) then
MLxReal(MolNo-d) = NewX
MLyReal(MoINo-d) = NewY-RadT
else
MLxReal(MolNo-d) = RadT / (sqrt((ChainGrad**2) +
1))
MLyReal(MolNo-d) = (ChainGrad * MLxReal(MoINo-
d))
if (NewX < MLxReal(ChainStartNo)) then
CSCy = CSCy + MLyReal(MolNo-d)
CSCx = CSCx + MLxReal(MoINo-d)
MLxReal(MoINo-d) = CSCx
MLyReal(MolNo-d) = CSCy
elseif (NewX > MLxReal(ChainStartNo)) then
CSCy = CSCy - MLyReal(MolNo-d)
CSCx = CSCx - MLxReal(MolNo-d)
MLxReal(MoINo-d) = CSCx
MLyReal(MolNo-d) = CSCy

```
```

                end if
                    end if
    end do
    end if
if (ChainEdgeHitCheck .eqv. .TRUE.) then
if (OverlapCount > 2500) then
MolNo = MolNo-a-1
GO TO 10
end if
if (NewX > GridSize-RadT) then
NewX = GridSize-RadT
elseif (NewX < RadT) then
NewX = RadT
end if
Dist = (a+1)*RadT
NewY = -(MLxReal(MoINo-a-1)**2)+(2*MLxReal(MoINo-a-1)*NewX)
NewY = NewY+(Dist**2)-(NewX**2)
NewY = sqrt(NewY)
if (NewY /= NewY) then
MoINo = MolNo-a-1
GO TO 10
end if
if (TempY - (MLyReal(MoINo-a-1) + NewY) < TempY -
(MLyReal(MoINo-a-1) - NewY)) then
NewY = MLyReal(MolNo-a-1) + NewY
else
NewY = MLyReal(MolNo-a-1) - NewY
end if
do b=1,MolNo - a-2
Dist = ((MLxReal(b)-NewX)**2)+((MLyReal(b)-NewY)**2)
Dist = sqrt(Dist)
if (Dist < ((RadT)+(Mlr(b)))) then
ChainHitCheck = .TRUE.
PartHit = b
OverlapCount = OverlapCount +1
GO TO 99
end if
end do
ChainGrad = (NewY - MLyReal(ChainStartNo)) / (NewX -
MLxReal(ChainStartNo))
EquC = NewY - (ChainGrad * NewX)
CSCy = NewY
CSCx = NewX
do d = 1, a
OverlapCount = 0
if (NewX - MLxReal(ChainStartNo) == 0) then
MLxReal(MolNo-d) = NewX
MLyReal(MoINo-d) = NewY-RadT

```
else
MLxReal(MoINo-d) \(=\) RadT \(/(\operatorname{sqrt}((\) ChainGrad** 2\()+\)
d))

MLyReal(MolNo-d) \(=(\) ChainGrad * MLxReal(MoINo-

> if (NewX < MLxReal(ChainStartNo)) then CSCy \(=\) CSCy + MLyReal(MoINo-d) CSCx \(=\) CSCx + MLxReal(MoINo-d) MLxReal(MoINo-d) \(=\) CSCx MLyReal(MoINo-d) \(=\) CSCy
> elseif \((\) NewX \(>\) MLxReal(ChainStartNo) \()\) then
> CSCy \(=\) CSCy - MLyReal(MoINo-d)
> CSCx \(=\) CSCx - MLxReal(MoINo-d)
> 
> 
> MLxReal(MoINo-d) \(=\) CSCx
> end if \(\quad\) MLyReal(MoINo-d) \(=\) CSCy
end do
elseif (ChainTopHitCheck .eqv. .TRUE.) then
OverTopCount = OverTopCount + 1
if (OverlapCount > 2500) then
MolNo = MolNo-a-1
GO TO 10
end if
if (OverTopCount > 2500) then
MoINo = MoINo-2
GO TO 10
end if
NewY = GridSize-RadT
Dist \(=(a+1)^{*}\) RadT
NewX \(=-(\) MLyReal(MoINo-a-1)**2)+(2*MLyReal(MoINo-a-1)*NewY)
NewX = NewX+(Dist**2)-(NewY**2)
NewX \(=\operatorname{sqrt}(\) New \(X)\)
if (NewX /= NewX) then
MoINo = MolNo-a-1
GO TO 10
end if
if (TempX - (MLxReal(MoINo-a-1) + NewX) < TempX -
(MLxReal(MoINo-a-1) - NewX)) then
NewX \(=\) MLxReal(MolNo-a-1) + NewX
else
NewX = MLxReal(MolNo-a-1) - NewX
end if
do \(\mathrm{b}=1\), MolNo \(-\mathrm{a}-2\)
Dist \(=\left((\text { MLxReal }(\mathrm{b})-\text { NewX })^{* *} 2\right)+\left((\mathrm{MLyReal}(\mathrm{b})-\text { NewY })^{* *} 2\right)\)
Dist \(=\) sqrt(Dist)
if (Dist < ((RadT) \(+(\operatorname{Mlr}(\mathrm{b})))\) ) then
ChainHitCheck = .TRUE.
PartHit = b
OverlapCount \(=\) OverlapCount +1
end if
end do
ChainGrad \(=(\) New \(Y\) - MLyReal(ChainStartNo)) / (NewX MLxReal(ChainStartNo))

EquC \(=\) New \(Y\) - (ChainGrad *NewX)
CSCy = NewY
do \(d=1\), \(a\)
OverlapCount = 0
OverTopCount \(=0\)
if (NewX - MLxReal(ChainStartNo) \(==0\) ) then
MLxReal(MolNo-d) = NewX
CSCy = CSCy - RadT
MLyReal(MoINo-d) = CSCy
else
MLxReal(MolNo-d) \(=\) RadT \(/(\operatorname{sqrt}((\) ChainGrad**2) +
1))

MLyReal(MolNo-d) \(=(\) ChainGrad * MLxReal(MoINo-
d))
if (NewX < MLxReal(ChainStartNo)) then
CSCy = CSCy + MLyReal(MolNo-d)
CSCx = CSCx + MLxReal(MoINo-d)
MLxReal(MolNo-d) = CSCx
MLyReal(MolNo-d) = CSCy
elseif (NewX > MLxReal(ChainStartNo)) then
CSCy = CSCy - MLyReal(MolNo-d)
CSCx = CSCx - MLxReal(MolNo-d)
MLxReal(MolNo-d) = CSCx
MLyReal(MoINo-d) = CSCy
end if
end if
end do
end if
MLxReal(MolNo) \(=\) New \(X\)
MLyReal(MolNo) \(=\) New \(Y\)
MLr(MolNo) = RadT
FullCount = 0
MoINo \(=\) MoINo +1
end do

CONTINUE
end

\section*{Appendix 5: RSA Algorithm}

This appendix contains the algorithm used to create the random sequential adsorption image used in Figure 4.3.
```

program packedbed
! Sets up initial variables
integer MoINo, RadLarge, RadSmall, BoxSize, GridSize, Rads, count, SN,
integer MLr
real MLxReal, MLyReal
dimension MLr(10000), Rads(10), MLxReal(10000), MLyReal(10000)
integer x, y, RadT
character t, FileName*15, FileID*3
integer ProgCount, PCId, count3
dimension FileID(1000)
real Dist
integer count2
logical Impact
t = 'y'
if (t == 'y') then
Rads(1) = 10 ! Inputs the radius to be present in the system
SN = 1
RadLarge = 0
RadSmall = 0
do count = 1,SN
if (RadLarge < Rads(count)) then
RadLarge = Rads(count)
end if
if (RadSmall > Rads(count) .or. RadSmall == 0) then
RadSmall = Rads(count)
end if
end do
RadLarge = 10 ! Determines the largest and smallest radius of the entered radii
RadSmall = 10
BoxSize = (RadLarge*6)
GridSize = BoxSize*5
do ProgCount = 1,50
write(FileID(ProgCount), '(i0)') ProgCount
end do
do ProgCount = 1,50 !Loops for the number of systems to be created
MLxReal = 0
MLyReal = 0
MLr = 0

```

MolNo = 1
FileName = "
call random_seed()
do while (count < 10000000)
Impact \(=\). FALSE.
! Finds a random \(x\) and \(y\) coordinate and radius
call random_number(RX)
count2 = 1 + floor(SN*RX)
RadT = Rads(count2)
call random_number(RX)
count2 \(=1+\) floor ((GridSize-(2*RadT))*RX)
x = count2+RadT
call random_number(RX)
count2 \(=1+\) floor ((GridSize-(2*RadT))*RX)
\(y=\) count2+RadT
! Confirms that the chosen location does not overlap with a previously
placed particle
if (MolNo > 1 ) then
hitloop: do count3 \(=1\), MoINo -1
Dist \(=\left((\text { MLxReal }(\text { count } 3)-x)^{* *} 2\right)+((\) MLyReal \((\) count3 \()-\)
\(y)^{* *} 2\) )
Dist \(=\operatorname{sqrt}(\) Dist \()\)
if (Dist \(<=(\) RadT + Mlr(count3))) then count = count + 1 Impact = .TRUE. exit hitloop
end if
end do hitloop
if (Impact .eqv. .FALSE.) then ! If there is no overlap, the location is saved, if there is an overlap the location is not saved and ignored.
count \(=0\)
MLxReal(MolNo) \(=x\)
MLyReal(MoINo) \(=y\)
\(\mathrm{MLr}(\mathrm{MolNo})=\) RadT
\(\mathrm{MoINo}=\mathrm{MoINo}+1\)
end if
else
MLxReal(MolNo) \(=x\)
MLyReal(MolNo) \(=y\)
MLr(MoINo) \(=\) RadT
MoINo = MolNo + 1
end if
end do
\(t=\) ' \(y\) '
if ( \(t==\) ' \(y\) ') then ! The particle locations are saved to a file, and the next system is started

FileName = "
FileName = trim(adjustl(FileID(ProgCount))) // '.csv'
open(1, file = FileName, status = 'new')

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```

            do y=1,MolNo-1
                write(1,*) MLxReal(y), ',', MLyReal(y), ',' , MLr(y)
                    end do
                    close(1)
                end if
    end do
    end if
end program

```

\section*{Appendix 6: MatLab Code Used}

This appendix contains the code used, to obtain data and visualise created systems, within MatLab.

\section*{Visualising 2D System Beds}
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted if isfile([num2str(x) '.csv']) \% Confirms the file exists in the expected folder load ([num2str(x) '.csv']) \% Loading the respective file box on \% Turns on an outline so the edges of the box are in the image output th \(=0: \mathrm{pi} / 50: 2^{*} \mathrm{pi} ; \%\) Gives the variable th values in the range 0 to \(2 \pi\) \(L=\) length(evalin('base',sprintf('X\%d',x))) \% Sets \(L\) to the number of particles in the system
figure \((x)\) \% Creates a figure for system \(x\)
for \(q=1: L \%\) Loops through each particle within the system xunit \(=\) evalin('base',sprintf('X\%d(q,3)',x)) * \(\cos (\) th \(\quad+\)
evalin('base',sprintf('X\%d(q,1)',x)); \% Calculates the x positions on the particle circumference yunit \(=\) evalin('base',sprintf('X\%d(q,3)',x)) * \(\sin (t h) \quad+\)
evalin('base',sprintf('X\%d(q,2)',x)); \% Calculates the y positions on the particle circumference \(\mathrm{h}=\operatorname{plot}(x u n i t\), yunit, ' \(k\) '); \% Plots those positions onto the figure hold on \% Keeps the old figure when adding a new particle to it xlim([0 600]); \% Sets the x-axis limits ylim([0600]); \% Sets the y-axis limits
end
else
I = x \% Outputs the file number if the file does not exist for error checking end
end

\section*{Determining 2D Packing Fractions}

PartFrac \(=0 \%\) Stores the packing fractions for all the systems
PartSum \(=0 \%\) Stores the total of all of the packing fractions for calculating the average
PartAvg \(=0 \%\) Stores the average of the packing fractions across all the systems
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted
PartTot \(=0\); \% Stores the total area of Particles within the currently analysed system
if isfile([num2str(x) '.csv']) \% Confirms the file exists in the expected folder
load ([num2str(x) '.csv']) \% Loading the respective file
\(\mathrm{L}=\) length(evalin('base',sprintf('X\%d',x))); \% Sets \(L\) to the number of particles
in the system
for \(q=1: L \%\) Loops through each particle within the system
PartTot = ((evalin('base',sprintf('X\%d(q,3)',x)) ^ 2) * pi) + PartTot; \%
Calculates the area of the particle and adds it to the current total area
end
PartFrac \((x)=\) PartTot \(/\left(300^{\wedge} 2\right)\); \% Calculates the packing fraction of the
current system
PartSum = PartSum + PartFrac(x); \% Adds the packing fraction of the current
system to the total to be averaged
end
end
PartAvg = PartSum / 50 \% Calculates the packing fraction average of the systems

\section*{Determining 2D Number of Contacts}

\section*{William Eales}
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted if isfile(['contacts' num2str(x) '.csv']) \% Confirms the file exists in the expected folder load (['contacts' num2str(x) '.csv']) \% Loading the respective contacts file load ([num2str(x) '.csv']) \% Loading the respective particle locations file \(\mathrm{L}=\) length(evalin('base',sprintf('contacts\%d',x))); \% Sets \(L\) to the number of particles in the system for \(q=1: L\)

SmolContNo = 0; \% Stores the number of contacts for small
particles
LorgContNo \(=0\); \% Stores the number of contacts for large particles
\(f=1\); \% The counter for looping through the arrays
while evalin('base',sprintf('contacts\%d(q,f)',x)) ~= 0 \% Checks the particle has more than zero contacts
if evalin('base',sprintf('X\%d(q,3)',x)) == 10 \% Determines if
the particle is of radius 10 (small) or not (large)
SmolContNo = SmolContNo + 1; \% Increments the
number of contacts for a small particle
\(f=f+1 ; \%\) Increments the array counter
else
number of contacts for a large particle
LorgContNo \(=\) LorgContNo \(+1 ; \%\) Increments the
\(f=f+1 ; \%\) Increments the array counter
end
end
SmolContCount(x,q) = SmolContNo; \% Stores the number of contacts for each small particle across all systems

LorgContCount(x,q) = LorgContNo; \% Stores the number of contacts for each large particle across all systems
end end
end

Determining the Percentage of 2D Systems That Contain a Percolation Chain
PercCount \(=0 \%\) Stores the number of systems that contain a percolation chain TotalCount \(=0 \%\) Stores the total number of systems
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted if isfile(['shapes' num2str(x) '.csv']) \% Confirms the file exists in the expected folder load (['shapes' num2str(x) '.csv']) \% Loading the respective particle shapes
file
the file
CurShape = evalin('base',sprintf('shapes\%d',x)); \% Retrieves the chains from
file
[numRows,numCols] = size(CurShape); \% Determines the size of the array
TotalCount = TotalCount + 1; \% Adds one to the total number of systems if numRows \(==1 \%\) Determines if the system has no percolation chains PercCount \(=\) PercCount +1 ; \% If so adds one to this counter end end
end
PercFracs = 100-((PercCount/TotalCount) * 100) \% Determines the percentage of systems that contain a percolation chain

\section*{Determining the Number of Percolation Chains in 2D Systems}

AvgCount \(=0 \%\) Stores the average number of percolation chains across all systems MaxCount \(=0 \%\) Stores the maximum number of percolation chain in a system

MinCount \(=999 \%\) Stores the minimum number of percolation chain in a system
RowCount \(=0 \%\) Stores the number of percolation chains in each system
TotalCount \(=0 \%\) Stores the sum of how many percolation chains across all systems
TotAmount \(=0 \%\) Stores the number of systems
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted if isfile(['shapes' num2str(x) '.csv']) \% Confirms the file exists in the expected folder load (['shapes' num2str(x) '.csv']) \% Loading the respective particle shapes
file CurShape = evalin('base',sprintf('shapes\%d',x)); \% Retrieves the chains from
the file
[numRows,numCols] = size(CurShape); \% Determines the size of the array
TotalCount = TotalCount + (numRows-1); \% Adds the number of percolation
chains in the current system to the total
TotAmount \(=\) TotAmount +1 ; \(\%\) Adds one to the total number of systems RowCount(x) = numRows-1; \% Saves number of percolation chain to the
array
if numRows- \(1>\) MaxCount \(\%\) If it is more than the current highest
MaxCount = numRows - 1; \% It is overwritten
end
if numRows- 1 < MinCount \% If it is less than the current lowest
MinCount = numRows - 1; \% It is overwritten
end
end
end
AvgCount \(=\) TotalCount/TotAmount \% Calculates the average number of percolation chains per system

\section*{Determining the Shortest Percolation Chain in 2D Systems}

SmallShapes \(=0 \%\) Stores all smallest percolation chain lengths from all systems
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted
SmolShap = 0; \% Stores the current shortest percolation chain length
if isfile(['shapes' num2str(x) '.csv']) \% Confirms the file exists in the expected folder load (['shapes' num2str(x) '.csv']) \% Loading the respective particle chains file CurShape = evalin('base',sprintf('shapes\%d',x)); \% Retrieves the chains from
the file
[numRows,numCols] = size(CurShape); \% Determines the size of the array if numRows \(\sim=1 \%\) Confirms there is at least one chain in the system for \(y=1\) :numRows- \(1 \%\) Loops through all the chains in the system ShapLength \(=0\); \% Stores current chain length for \(z=1\) :numCols \(\%\) Loops through the columns
if CurShape \((y, z)=0 \%\) Checks if the chain is still
going
if ShapLength < SmolShap | SmolShap == 0
\% Checks if the current chain is shorter than the previously shortest chain SmolShap = ShapLength; \% If so it
replaces it
end
end
ShapLength \(=\) ShapLength +1 ; Increments the
chain length counter end end
end
end
SmallShapes(x) = SmolShap; \% Stores the smallest chain from this system
End

\section*{Determining the Longest Percolation Chain in 2D Systems}
LargeShapes = 0 \% Stores all largest percolation chain lengths from all systems
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted LorgShap \(=0 ; \%\) Stores the current longest percolation chain length if isfile(['shapes' num2str(x) '.csv']) \% Confirms the file exists in the expected folder load (['shapes' num2str(x) '.csv']) \% Loading the respective particle chain file CurShape = evalin('base',sprintf('shapes\%d',x)); )); \% Retrieves the chain from the file
[numRows,numCols] = size(CurShape); \% Determines the size of the array if numRows \(\sim=1 \%\) Confirms there is at least one chain in the system
for \(y=1\) :numRows- \(1 \%\) Loops through all the chains in the system
ShapLength \(=0\); \% Stores current chain length for \(z=1\) :numCols \% Loops through the columns
if CurShape \((y, z)==0 \%\) Checks if the chain is still
going
if ShapLength > LorgShap | LorgShap == 0
\% Checks if the current chain is longer than the previously longest chain
LorgShap = ShapLength; \% If so it replaces it
end
end
ShapLength = ShapLength +1 ; \% Increments the
chain length counter end
end
end
end
LargeShapes(x) = LorgShap; \% Stores the largest chain from this system
end

\section*{Determining the Average Percolation Chain Length in 2D Systems}
Shapes = \(0 \%\) Stores the sum of all chain lengths across all systems
ShapeCount \(=0 \%\) Stores the number of chains
AvgLength \(=0 \%\) Stores the average length of chain
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted if isfile(['shapes' num2str(x) '.csv']) \% Confirms the file exists in the expected folder load (['shapes' num2str(x) '.csv']) \% Loading the respective particle chain file CurShape = evalin('base',sprintf('shapes\%d',x)); \% Retrieves the chain from the file
[numRows,numCols] = size(CurShape); \% Determines the size of the array if numRows \(\sim=1 \%\) Confirms there is at least one chain in the system
for \(\mathrm{y}=1\) :numRows-1 \% Loops through all the chain in the system
ShapLength \(=0\); \% Stores current chain length
for \(z=1\) :numCols \% Loops through the columns
if CurShape \((y, z)==0 \%\) Checks if the chain is still
going
Shapes = Shapes + ShapLength; \% Adds
the chain length to the total of all shape lengths
ShapeCount \(=\) ShapeCount +1 ; \(\%\) Increments the number of chains counter
end
ShapLength = ShapLength +1 ; \% Increments the chain length counter end
end
end
end
end
AvgLength = Shapes/ShapeCount \% Calculates the average percolation chain length

\section*{Visualising 3D System Beds}
for \(\mathrm{a}=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted if isfile([num2str(a) '.csv']) \% Confirms the file exists in the expected folder load ([num2str(a) '.csv']) \% Loading the respective particle locations file CurPart = evalin('base',sprintf('X\%d',a))'; [ \(\mathrm{x} y \mathrm{z}\) ] = sphere; \% Sets up \(x, y\) and \(z\), as the coordinates of the sphere particle box on \% Turns on an outline so the edges of the box are in the image output \(\mathrm{L}=\) length(CurPart) \% Sets \(L\) to the number of particles in the system figure(a) Creates a figure for system a for \(q=1: L \%\) Loops through each particle within the system \(s(q)=\operatorname{surf}\left(x^{*} \operatorname{CurPart}(4, q)+\operatorname{CurPart}(1, q), y^{*} \operatorname{CurPart}(4, q)+\operatorname{CurPart}(3, q)\right.\), \(\left.z^{*} \operatorname{CurPart}(4, q)+\operatorname{CurPart}(2, q)\right)\); \% Draws the sphere particle onto the figure hold on \% Keeps the old figure when adding a new particle to it end
end
end

\section*{Determining 3D Packing Fractions}

PartFrac \(=0\) \% Stores the packing fractions for all the systems
PartFracAvg = 0 \% Stores the average of the packing fractions across all the systems
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted
PartTot \(=0\); \% Stores the total area of Particles within the currently analysed system
if isfile([num2str(x) '.csv']) \% Confirms the file exists in the expected folder
load ([num2str(x) '.csv']) \% Loading the respective particle locations file
\(\mathrm{L}=\) length(evalin('base',sprintf('X\%d',x))); \% Sets \(L\) to the number of particles
in the system
for \(q=1: L \%\) Loops through each particle within the system
PartTot \(=((\) evalin('base',sprintf('X\%d(q,4)',x)) ^ 3) * (4/3) * pi) +
PartTot \% Calculates the volume of the particle and adds it to the current total volume
end
PartFrac \((x)=\) PartTot / (240^3); \% Calculates the packing fraction of the
current system
PartFracAvg = PartFracAvg + PartFrac(x); \% Adds the packing fraction of the
current system to the total to be averaged
end
end
PartFracAvg = PartFracAvg / \(50 \%\) Calculates the packing fraction average of the systems

\section*{Determining 3D Number of Contacts}
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted if isfile(['contacts' num2str(x) '.csv']) \% Confirms the file exists in the expected folder load (['contacts' num2str(x) '.csv']) \% Loading the respective particle contacts
file
load ([num2str(x) '.csv']) \% Loading the respective particle locations file \(\mathrm{L}=\) length(evalin('base',sprintf('contacts\%d',x))); \% Sets \(L\) to the number of particles in the system
for \(q=1: L\) \% Loops through each particle within the system

SmolContNo = 0; \% Stores the number of contacts for small
particles
LorgContNo \(=0\); \% Stores the number of contacts for large particles
\(f=1\); \% The counter for looping through the arrays
while evalin('base',sprintf('contacts\%d(q,f)',x)) \(\sim 0 \%\) Checks the particle has more than zero contacts
if evalin('base',sprintf('X\%d(q,4)',x)) == 10 \% Determines if the particle is of radius 10 (small) or not (large)

SmolContNo \(=\) SmolContNo \(+1 ; \%\) Increments the
number of contacts for a small particle
\(f=f+1 ; \%\) Increments the array counter
else
LorgContNo \(=\) LorgContNo +1 ; \% Increments the
number of contacts for a large particle
\(f=f+1 ; \%\) Increments the array counter end
end
SmolContCount(x,q) = SmolContNo; \% Stores the number of contacts for each small particle across all systems

LorgContCount( \(\mathrm{x}, \mathrm{q}\) ) \(=\) LorgContNo; \% Stores the number of contacts for each large particle across all systems end
end
end

\section*{Determining Chain Angles in Single Chain Type System (Currently set at \(\mathbf{n}_{\mathrm{p}}=\mathbf{2}\) )}
\(y=1 \%\) Stores the number of chains
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted if isfile([num2str(x) '.csv']) \% Confirms the file exists in the expected folder load ([num2str(x) '.csv']) \% Loading the respective particle locations file \(L=\) length(evalin('base',sprintf('X\%d',x))) \% Sets \(L\) to the number of particles
in the system
for \(q=1: 2: L \%\) Loops through each particle within the system skipping middle of chain particles
\(v 1 \quad=\quad\) evalin('base',sprintf('X\%d(q+1,1)',x))
evalin('base',sprintf('X\%d(q,1)',x)); \% Calculates the dx between the current particle and the next particle it is attached to
v2 \(\quad=\quad\) evalin('base',sprintf('X\%d(q+1,2)',x)) evalin('base',sprintf('X\%d(q,2)',x)); \% Calculates the dy between the current particle and the next particle it is attached to
\(\mathrm{v} 3=\mathrm{v} 1 / \mathrm{v} 2\); \% Calculates the gradient of the chain
\(\mathrm{v} 4(\mathrm{x}, \mathrm{y})=\) atand \((\mathrm{v} 3)\); \% Calculates the angle of the chain
\(y=y+1 ; \%\) Increments the number of chains counter
end
end
end

\section*{Determining Chain Angles and Packing Fractions in Chain Systems (Based on Particle Size)}
ys \(=1 \%\) Stores the counter for shorter chain angle array
\(\mathrm{yc}=1 \%\) Stores the counter for longer chain angle array
PartTotC \(=0\); \% Stores the area covered by larger chains
PartTotS \(=0 ; \%\) Stores the area covered by smaller chains
PartFrac \(=0 ; \%\) Stores all the systems packing fractions

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PartSum = 0; \% Stores the sum of all systems packing fractions
PartAvg = 0; \% Stores the average of all systems packing fractions
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted if isfile([num2str(x) '.csv']) \% Confirms the file exists in the expected folder scount \(=1 ; \%\) Stores the number of smaller chains or single particles ccount \(=1\); \% Stores the number of larger chains load ([num2str(x) '.csv']) \% Loading the respective particle locations file \(L=\) length(evalin('base',sprintf('X\%d',x))) \% Sets \(L\) to the number of particles
in the system
for \(q=1: L \%\) Loops through each particle within the system
if evalin('base',sprintf('X\%d(q,3)',x)) == \(5 \%\) Determines of the radius
of the particle is 5 (small chain or single) or not (long chain)
singles(scount,1) = evalin('base',sprintf('X\%d(q,1)',x)); \% If
small, saves the \(x\) coordinate here
singles(scount,2) = evalin('base',sprintf('X\%d(q,2)',x)); \%
And the y coordinate here
scount \(=\) scount \(+1 ; \%\) Then adds one to the counter
else
chains(ccount,1) = evalin('base',sprintf('X\%d(q,1)',x)); \% If large, saves the x coordinate here
chains(ccount,2) = evalin('base',sprintf('X\%d(q,2)',x)); \% And
the y coordinate here
ccount \(=\) ccount \(+1 ; \%\) Then adds one to the counter
end
end
for \(q=1: 5: c c o u n t-4 \%\) Loops through the large chains (currently set for \(n_{p}=\)
5)
\(\mathrm{v} 1=\) chains \((\mathrm{q}+1,1)\) - chains \((\mathrm{q}, 1)\); \% Calculates the dx between the current particle and the next particle it is attached to
\(\mathrm{v} 2=\) chains \((\mathrm{q}+1,2)-\) chains \((\mathrm{q}, 2)\); \% Calculates the dy between the current particle and the next particle it is attached to
\(\mathrm{v} 3=\mathrm{v} 1 / \mathrm{v} 2\); \% Calculates the gradient of the chain
\(\mathrm{cv} 4(\mathrm{yc})=\) atand \((\mathrm{v} 3)\); \% Calculates the angle of the chain and saves it \(y c=y c+1 ; \%\) Increments the array counter
end
for \(q=1: 5\) :scount \(-4 \%\) Loops through the small chains (currently set for \(n_{p}=\) 5)
\(v 1=\) singles \((q+1,1)-\) singles \((q, 1)\); \% Calculates the \(d x\) between the current particle and the next particle it is attached to
\(\mathrm{v} 2=\) singles \((\mathrm{q}+1,2)-\) singles \((\mathrm{q}, 2)\); \% Calculates the dy between the current particle and the next particle it is attached to
\(\mathrm{v} 3=\mathrm{v} 1 / \mathrm{v} 2\); \% Calculates the gradient of the chain
sv4(ys) = atand(v3); \% Calculates the angle of the chain and saves it
ys = ys \(+1 ; \%\) Increments the array counter
end
PartTotC \(\left.=\left(\left(\left(10{ }^{\wedge} 2\right){ }^{*} \mathrm{pi}\right)-\left(\left(\left(10^{\wedge} 2\right)^{*}\left(\left(\left(2^{*} \mathrm{pi}\right) / 3\right)-((\operatorname{sqrt}(3)) / 2)\right)\right)\right)^{*}(0.8)\right)\right)^{*}\) (ccount); \% Calculates the area covered by larger chains

PartTotS \(=\left(\left(\left(5^{\wedge} 2\right){ }^{*} \text { pi }\right)-\left(\left(\left(5^{\wedge} 2\right)^{*}\left(\left(\left(2^{*} \mathrm{pi}\right) / 3\right)-((\operatorname{sqrt}(3)) / 2)\right)\right)^{*}(0.8)\right)\right)^{*}(\) scount \() ;\) \% Calculates the area covered by smaller chains

PartFrac \((x)=(\) PartTotS + PartTotC \() /\left(600^{\wedge} 2\right) ; \%\) Calculates the systems packing fraction

PartSum = PartSum + PartFrac(x); \% Adds the packing fraction to the total for calculating the average
else
\(I=x \%\) Outputs the file number if the file does not exist for error checking
end
end
PartAvg = PartSum / 50 \% Calculates the packing fraction average of the systems

\section*{Determining Chain Angles and Packing Fractions in Chain Systems (Based on Particle Overlap)}
ys \(=1 \%\) Stores the counter for shorter chain angle array
\(\mathrm{yc}=1 \%\) Stores the counter for longer chain angle array
PartTotC \(=0 ; \%\) Stores the area covered by larger chains
PartTotS \(=0 ; \%\) Stores the area covered by smaller chains
PartFrac \(=0 ; \%\) Stores all the systems packing fractions
PartSum = 0; \% Stores the sum of all systems packing fractions
PartAvg \(=0 ; \%\) Stores the average of all systems packing fractions
for \(x=1: 50 \%\) This line starts the loop that will iterate for the number of systems inputted if isfile([num2str(x) '.csv']) \% Confirms the file exists in the expected folder scount \(=1 ; \%\) Stores the number of smaller chains or single particles ccount \(=1 ; \%\) Stores the number of larger chains load ([num2str(x) '.csv']) \% Loading the respective particle locations file \(L=\) length(evalin('base',sprintf('X\%d',x))) \% Sets \(L\) to the number of particles
in the system

> for \(q=1: L \%\) Loops through each particle within the system
> \(\quad\) overlap = \(0 ; \%\) Value for if there is an overlap (1) or not (0)
if \(q \sim=L \%\) Determining if the loop is not on the last iteration \(m=q+1 ; \%\) Used to denote the particle placed after the
current particle
dist \(\quad=\quad((\) evalin('base',sprintf('X\%d(q,1)',x)) -
evalin('base',sprintf('X\%d(m,1)',x)))^2) \(+\quad((\) evalin('base',sprintf('X\%d(q,2)',x)) evalin('base',sprintf('X\%d(m,2)',x)))^2);
dist = sqrt(dist); \% Determining the distance between particle
\(q\) and \(m\)
if dist < ((evalin('base',sprintf('X\%d(q,3)',x)) + evalin('base',sprintf('X\%d(m,3)',x))) - 5) \% Determining if they are overlapping overlap \(=1 ; \%\) If so setting variable to 'yes'
end
end
if \(q \sim=1 \%\) Does the same as above however checks the particle
placed prior
\[
\mathrm{n}=\mathrm{q}-1
\]
\(\begin{array}{rlll}\text { dist } & = & ((\text { evalin('base',sprintf('X\%d(q,1)', } \mathrm{x})) & - \\ \left.\text { evalin('base', sprintf('X\%d(n,1)',x)) })^{\wedge} 2\right) & + & ((\text { evalin('base',sprintf('X\%d(q,2)',x)) } & -\end{array}\) evalin('base',sprintf('X\%d(n,2)',x)))^^2);
dist \(=\) sqrt(dist);
if dist \(<\quad((\) evalin('base',sprintf('X\%d(q, 3)', x)) +
evalin('base',sprintf('X\%d(n,3)',x)))-5) overlap =1;
end \(\quad\) end
if overlap \(==1 \%\) If an overlap is found then the particle is part of a
chain

Saves the x coordinate here

Saves the y coordinate here
chains(ccount,1) = evalin('base',sprintf('X\%d(q,1)',x)); \% chains(ccount,2) = evalin('base',sprintf('X\%d(q,2)',x)); \% ccount \(=\) ccount +1 ; \% Increments the array counter
else \% If no overlap then particle is a single singles(scount,1) = evalin('base',sprintf('X\%d(q,1)',x)); \%
Saves the x coordinate here singles(scount,2) = evalin('base',sprintf('X\%d(q,2)',x)); \% scount \(=\) scount +1 ; \% Increments the array counter end end
for \(q=1: 5:\) ccount-4
\(\mathrm{v} 1=\) chains \((\mathrm{q}+1,1)\) - chains \((\mathrm{q}, 1)\);
\(\mathrm{v} 2=\) chains \((\mathrm{q}+1,2)\) - chains \((\mathrm{q}, 2)\);
\(\mathrm{v} 3=\mathrm{v} 1 / \mathrm{v} 2\);
cv4(yc) = atand(v3);
yc = yc + 1;
end

PartTotC = (((10 ^ 2) * pi) - (((10^2)* (((2*pi)/3) - ((sqrt(3))/2))) * (0.8))) * (ccount); \% Calculates the area covered by chains

PartTotS = ((10 ^ 2) * pi) * (scount); \% Calculates the area covered by singles PartFrac \((x)=\left(\right.\) PartTotS + PartTotC) \(/\left(600^{\wedge} 2\right) ; \%\) Calculates the systems
packing fraction
PartSum = PartSum + PartFrac(x); \% Adds the packing fraction to the total for calculating the average
else
I = x \% Outputs the file number if the file does not exist for error checking
end
end
PartAvg = PartSum / 50 \% Calculates the packing fraction average of the systems```

